## TRAFFIC IMPACT AND ACCESS STUDY

## PROPOSED RESIDENTIAL DEVELOPMENT

4 Hillside Avenue<br>Newburyport, Massachusetts

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MDM Transportation Consultants, Inc. (MDM) has prepared this Traffic Impact and Access Study (TIAS) for a proposed residential development to be located at 4 Hillside Avenue in Newburyport, Massachusetts. This report documents existing operational and safety-related characteristics of roadways serving the development site, estimates future year operating characteristics of these roadways independent of the development, estimates developmentrelated trip generation, and identifies incremental impacts of site-related traffic.

This TIAS has been prepared in accordance with requirements and standards for the preparation of traffic studies as jointly issued by the Commonwealth of Massachusetts Executive Office of Energy \& Environmental Affairs/Massachusetts Department of Transportation (EEA/MassDOT).

## E. 1 PROIECT DESCRIPTION

The Site comprises approximately 4.55 acres located at 4 Hillside Avenue and 12-14 Cottage Court in Newburyport, Massachusetts. The Site includes a duplex home and an undeveloped parcel adjacent to the Highland Cemetery and single family homes on Cottage Court and Hillside Avenue. Access/egress to the Site is currently provided via Cottage Court and Hillside Avenue.

Under the proposed plan, the property will developed to include 58 new residential apartment units (48 apartments and the long range build-out of a 10 room residence for the YWCA) and an existing duplex home for a total of 60 on-site rental apartment units. Access/egress to the Site under proposed conditions will be provided via a right-in/right-out unsignalized driveway along Newburyport Turnpike (Route 1) and via roadway extensions of Cottage Court and Hillside Avenue.

## E. 2 STUDY AREA

This TIAS evaluates transportation characteristics of roadways and intersections that provide a primary means of access to the Site, and that are likely to sustain a measurable level of traffic impact from the development. The study area includes the following intersections:

- Route 1 at Low Street/ Pond Street (Signalized)
- Route 1 at Proposed Site Driveway (Unsignalized)
- Pond Street/Cottage Court/Auburn Street (Unsignalized)
- Pond Street/Hillside Avenue (Unsignalized)


## E. 3 SUMMARY OF ANALYSIS AND FINDINGS

Capacity analyses were conducted for each study area intersection to quantify existing and future year traffic operations with and without the development for the weekday morning and weekday evening peak hours. These time periods represent the highest activity periods of the proposed project and the adjacent roadway system.

Under existing and future No-Build conditions:
$\square$ The signalized intersection of Route 1 and Low Street/ Pond Street will operate below capacity at an overall level of service LOS D or better during the peak hours.
$\square$ The intersections of Cottage Court and Hillside Avenue with Pond Street will operate below capacity at LOS $B$ or better during the peak hours with minimal delay.

The analyses presented in this TIAS are based on industry-standard trip rates published by the Institute of Transportation Engineers (ITE). On this basis, the proposed apartment development is estimated to generate approximately 30 vehicle-trips during the weekday morning peak hour and 36 vehicle-trips during the weekday evening peak hour. On a daily basis, the development is estimated to generate approximately 386 vehicle trips on a weekday.

Under Build Conditions, the incremental changes in traffic at the study intersections due to the proposed development do not result in any significant change in intersection operations at the study intersections compared to No-Build conditions. Under Build conditions, the site driveway intersection with Route 1 and nearby signalized intersection will continue to operate under capacity during the peak hours with no material change in delay.

## E. 4 RECOMMENDATIONS

MDM finds that travel conditions in the site vicinity along Route 1 and Pond are generally unconstrained. Trip generation for the development is estimated at approximately 30 vehicletrips during the weekday morning peak hour and 36 vehicle-trips during the weekday evening peak hour. Traffic impacts associated with the proposed apartment development are not expected to notably affect travel or safety conditions in the site vicinity. MDM recommends the following access-related improvements:

## Route 1 at Proposed Site Driveway

MDM recommends the following access-related improvements which are subject to MassDOT permitting and approval, as shown in Figure 8:

- A "STOP" sign (R1-1) and STOP line pavement marking are recommended on the driveway approach to Route 1. A "no left turn" sign (R3-2) should be installed opposite the Site in the median of Route 1 to enhance the right turn only restriction. The signs and pavement markings shall be compliant with the Manual on Uniform Traffic Control Devices (MUTCD).
- The existing "traffic signal ahead" sign (W3-3) will need to be relocated given the conflict with the location of the proposed site driveway.
$\square$ The driveway alignment, widths and curb radii should been designed to achieve approximate perpendicular orientation with Route 1 . The final curb radii should also be designed to accommodate the largest anticipated design vehicle.
- The driveway has been designed to restrict vehicle movements to right-in/right-out only operation. To enhance the turn restriction, the driveway will incorporate pavement unarkings, a raised channelized right turn island and MUTCD compliant signage.

ㅁ Plantings (shrubs, bushes) and structures (walls, fences, etc.) shall be maintained at a height of 2 feet or less within the sight lines in vicinity of the Site driveways to provide unobstructed sight lines. Furthermore, the existing vegetation and structures within the sight lines shall be selectively cleared when the Site driveway is constructed and the terrain shall be graded as required to ensure minimum recommended sight line requirements are met or exceeded.

- A "STOP" sign (R1-1) is recommended on the Cottage Court approach to Pond Street. The sign shall be compliant with the MUTCD.
$\square$ The existing dead-end sign (W14-1) should be removed when the Cottage Court is extended through the Site to Route 1.
- Given the close proximity (less than 100 feet) to the traffic signal control at the Route 1/Pond Street intersection, a "Do Not Block Intersection" sign and markings are recommended at the Pond Street/Auburn Street/Cottage Court intersection to enhance operations for left-turn movements at the intersection. All signs and marking shall be in conformance with the MUTCD.

Pond Street at Hillside Avenue

- A "STOP" sign (R1-1) is recommended on the Hillside Avenue approach to Pond Street. The sign shall be compliant with the MUTCD.


## E. 5 CONCLUSIONS

While the project will increase traffic in the immediate study area, adequate capacity is available under future Build conditions along Route 1, Pond Street, Low Street and at the study intersections to accommodate the trip increases associated with the proposed apartment development. The project is not projected to significantly change any reported operating levels compared to future No-Build conditions, thus no off-site mitigation is recommended. Proposed access improvements will provide ample capacity to accommodate site-generated traffic while also enhancing safety and capacity. In addition, proposed access/egress will be designed to enhance vehicular connections to the site and to ensure that adequate sight lines are provided in accordance with AASHTO criteria based on ambient travel speeds.

### 1.0 INTRODUCTION

This report presents a transportation impact and access evaluation for a proposed residential development to be located at 4 Hillside Avenue in Newburyport, Massachusetts. This report documents existing operational and safety-related characteristics of roadways serving the development site, estimates future year operating characteristics of these roadways independent of the development, estimates development-related trip generation, and identifies incremental impacts of site-related traffic.

This TIAS has been prepared in accordance with requirements and standards for the preparation of traffic studies as jointly issued by the Commonwealth of Massachusetts Executive Office of Energy \& Environmental Affairs/Massachusetts Department of Transportation (EEA/MassDOT).

### 1.1 PROPOSED DEVELOPMENT

The Site comprises approximately 4.55 acres located at 4 Hillside Avenue and 12-14 Cottage Court in Newburyport, Massachusetts. The Site includes a duplex home and an undeveloped parcel adjacent to the Highland Cemetery and single family homes on Cottage Court and Hillside Avenue. Access/egress to the Site is currently provided via Cottage Court and Hillside Avenue. The proximity of the site in relation to the regional transportation system is shown in Figure 1.

Under the proposed plan, the property will developed to include 58 new residential apartment units (48 apartments and the long range build-out of a 10 room residence for the YWCA) and an existing duplex home for a total of 60 on-site rental apartment units. Access/egress to the Site under proposed conditions will be provided via a right-in/right-out unsignalized driveway along Newburyport Turnpike (Route 1) and via roadway extensions of Cottage Court and Hillside Avenue. The preliminary Site layout sketch plan prepared by Westcott Site Services is presented in Figure 2.

## Traffic Impact \& Access Study

Newburyport, Massachusetts



### 1.2 STUDY METHODOLOGY

This transportation impact and access evaluation is conducted in accordance with EEA/MassDOT guidelines, and consists of several steps. The first step documents existing conditions in the transportation study area including an inventory of roadway geometry, observed traffic volumes, public transportation, and safety characteristics. Next, future year traffic conditions are forecast that account for other planned area developments, normal area growth, and development-related traffic increases. The third step quantifies operating characteristics of the study intersection. Specific attention is given to the incremental impacts of the proposed development. Finally, improvements are identified to address specific development-related requirements as needed.

### 1.3 STUDY AREA

This TIAS evaluates transportation characteristics of roadways and intersections that provide a primary means of access to the Site, and that are likely to sustain a measurable level of traffic impact from the development. The study area includes the following intersections:

- Route 1 at Low Street/ Pond Street (Signalized)
- Route 1 at Proposed Site Driveway (Unsignalized)
- Pond Street/Cottage Court/Auburn Street (Unsignalized)
- Pond Street/Hillside Avenue (Unsignalized)


### 2.0 EXISTING CONDITIONS

In order to provide a basis for quantifying the transportation impacts of the development, the existing roadway system and the existing traffic operations of study area roadways were reviewed. This section describes the existing traffic characteristics and operations of roadways and intersection within the study area. Specifically, this section presents an overview of the traffic data collection program, existing traffic volumes, safety issues and public transportation systems serving the area.

### 2.1 STUDY AREA ROADWAY NETWORK

The study area roadways and intersection are described briefly in this section. A general description of the physical roadway and intersection features is provided. The study area includes roadways under State and local jurisdiction. The study area and intersection are depicted in Figure 1.

### 2.1.1 Roadways

## Route 1

Route 1 is classified by the MassDOT as an urban other principal arterial roadway in the area which generally runs in a north - south direction and is under MassDOT jurisdiction. In the area, Route 1 generally runs parallel to I-95 and provides a connection to several major roadways including Route 1 A , Route 110 , Route 113 , and Route 133 . Within the study area, Route 1 provides two travel lanes in each travel direction separated by a median and additional travel lanes are provided at its major intersections. Pavement markings include single yellow edge lines, white lane line and marked white edge lines. The posted speed limit in the project vicinity ranges between 40 and 45 miles per hour. Land uses along Route 1 in the immediate project area primarily consist of residential uses with several industrial and commercial establishments.

## Pond Street

Pond Street is classified by the MassDOT as an Urban Minor Arterial under the City of Newburyport jurisdiction. Pond Street is an east-west roadway in the project area which connects Route 1/ Low Street to the west and High Street (Route 1A) to the east. The roadway generally provides one lane of travel in each direction with a total pavement width varying between 24 to 28 feet in the study area. A sidewalk is provided along both sides of the roadway within the study area and appears to have been recently enhanced with new wheelchair ramps and crosswalk markings. The posted speed limit along Pond Street in the study area is 30 miles per hour. Land use along Pond Street is generally residential with the exception of the Old Hill Burying Ground located along the northerly side of Pond Street.

## Cottage Court

Cottage Court is classified by the MassDOT as a Local roadway under the City of Newburyport jurisdiction. Cottage Court is approximately 450 feet in length and terminates at the Site. The roadway currently provides access to six homes and ranges is approximately 20 feet wide with no sidewalks. Streetlights are provided along Cottage Court.

## Hillside Avenue

Hillside Avenue is classified by the MassDOT as a Local roadway under the City of Newburyport jurisdiction. Hillside Avenue is approximately 275 feet in length and terminates at the Site. The roadway currently provides access to five homes and is approximately 20 feet wide with a sidewalk provided along the eastern side. Streetlights are provided along Hillside Avenue.

### 2.1.2 Intersections

## Route 1 at Low Street/ Pond Street

Route 1 meets Low Street/ Pond Street to form a four-way, signakized intersection. The northbound and southbound Route 1 approaches both provide a protected left-turn lane, a through travel lane and a shared through/ right turn lane. The Low Street eastbound approach provides a shared left/ through travel lane and an excusive right turn lane. The Pond Street westbound approach provides a single left/ through/ right turn lane. Traffic signal operation provides protected left turns from Route 1 with overlapping right turns from Low Street as well as split phasing between Low Street and Pond Street movements and an exclusive pedestrian crossing phase. Land uses at the intersection include several residential homes and a commercial property.

### 2.2 EXISTING TRAFFIC VOLUMES

Traffic-volume data used in this study were obtained by mechanical and manual methods im October 2014 and August 2015. Automatic traffic recorder counts (ATRs) were conducted along Route 1 while manual turning movement counts (TMCs) were conducted at the study intersections. Traffic data were collected during the weekday morning (7:00 to 9:00 AM) and weekday evening (4:00 to 6:00 PM) peak periods. These hours represent the combination of busiest activity periods of the Site and adjacent roadway network. The traffic count data is included in the Appendix.

### 2.2.1 Daily Traffic

Daily traffic volumes along Route 1 in the site vicinity were obtained by mechanical methods using an automatic traffic recorder. The results of the counts are summarized in Table 1, and are discussed below.

TABLE 1
EXISTING TRAFFIC VOLUME SUMMARY ROUTE 1 NORTH OF HILL STREET

|  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Time Period |  |  |  |

${ }^{3}$ Two-way daily traffic expressed in vehicles per day without seasonal adjustment.
${ }^{2}$ The percent of daily traffic that occurs during the peak hour.
${ }^{3}$ Two-way peak-hour volume expressed in vehicles per hour.
${ }^{4} \mathrm{NB}=$ Northbound, $\mathrm{SB}=$ Southbound

As summarized in Table 1, the weekday daily traffic volume on Route 1 in the site vicinity is approximately 11,660 vehicles per day (vpd) on a weekday. Peak hour traffic flow on Route 1 ranges from approximately 933 vehicles per hour (vph) during the morning peak hour to $1,090 \mathrm{vph}$ during the evening peak hour representing 8 to 9 percent of daily traffic flow. Vehicle flow is skewed towards the southbound direction during the weekday morning peak hour and in the northbound direction during the weekday evening peak hour.

### 2.2.2 Peak-Hour Traffic

Manual turning movement counts (TMCs) were conducted during the weekday morning (7:00 AM - 9:00 AM) and weekday evening (4:00 PM - 6:00 PM) peak periods. Traffic data used in this evaluation was collected in August 2015. These data reflect above-average traffic conditions based on review of MassDOT permanent count station data for the area. In order to provide a conservative analysis, no seasonal adjustment (reduction) of the data was made to the August traffic volume counts. Permanent count station data is provided in the Appendix. The resulting existing weekday morning and weekday evening peak hour traffic volumes for study intersections are depicted in Figure 3.

### 2.3 MEASURED TRAVEL SPEEDS

Vehicle speeds were obtained for the Route 1 northbound travel direction by timing vehicles over a known distance and then converting the travel times to speeds. Table 2 summarizes the average and $85^{\text {th }}$ percentile speeds for Route 1 adjacent to the Site. These speed data provide a basis for determining appropriate sight lines for the proposed driveway along Route 1. Field data are provided in the Appendix.

TABLE 2
SPEED STUDY RESULTS - ROUTE 1

|  | Travel Speeds |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Travel <br> Direction | Posted |  | Mean $^{1}$ | $8^{85^{\text {th }}}$ <br> Percentile |
|  |  |  | 45 | 48 |

${ }^{1}$ Advisory/ Posted Speed (mph)
${ }^{2}$ Arithmetic mean (mph)
${ }^{2}$ The speed at or below which 85 percent of the vehicles are traveling
As summarized in Table 2, the mean (average) travel speed on Route 1 traveling northbound is 42 mph and the $85^{\text {th }}$ percentile travel speed is 48 mph . The observed average and $85^{\text {th }}$ percentile travel speeds are highly consistent with the regulatory speed limit on Route 1 in the northbound direction.


### 2.4 SAFETY

In order to identify crash trends and safety characteristics for study area intersections, crash data were obtained from MassDOT for the City of Newburyport for the three-year period covering 2011 through 2013 (the most recent data currently available). A summary of the crash data with crash rates for each study area intersection is detailed in Table 3 with detailed data provided in the Appendix.

Crash rates were determined for each study area intersection. These rates quantify the number of crashes per million entering vehicles. MassDOT has determined the crash rates within the District 4 area (which includes the City of Newburyport) to be 0.58 for unsignalized intersections and 0.77 for signalized intersections. These rates represent MassDOT's "average" crash experience for District 4 communities and serves as a basis for comparing reported crash rates for study area intersections which are located within the district.

TABLE 3
INTERSECTION CRASH SUMMARY 2011 THROUGH $2013{ }^{1}$

|  | INTERSECTION |
| :---: | :---: |
|  | Route 1 at |
|  | Low Street/ |
| Data Category | Pond Street |
| Traffic Control | Signalized |
| Crash Rate ${ }^{2}$ | 0.19 |
| MHD District 4 Avg. ${ }^{3}$ | 0.77 |
| Year: |  |
| 2011 | 2 |
| 2012 | 1 |
| 2013 | 1 |
| Total | 4 |
| Type: |  |
| Angle | 2 |
| Rear-End | 1 |
| Head-On | 0 |
| Sideswipe | 1 |
| Single Vehicle | 0 |
| Unknown/Other | 0 |
| Severity: |  |
| P. Damage Only | 1 |
| Personal Injury | 3 |
| Fatality | 0 |
| Unknown | 0 |
| Conditions: |  |
| Dry | 3 |
| Wet | 1 |
| Snow | 0 |
| Other/Unknown | 0 |
| Time: |  |
| 7:00 to 9:00 AM | 0 |
| 4:00 to 6:00 PM | 0 |
| Rest of Day | 4 |

${ }^{1}$ Source: MassDOT Crash Database.
${ }^{2}$ Crashes per million entering vehicles (MEV)
${ }^{3}$ District 4 Average Crash Rate

- Route 1 at Low Street/ Pond Street: A total of four (4) crashes were reported for the Route 1 and Low Street signalized intersection - approximately 1 per year - resulting in a crash rate of 0.19 which is well below the District 4 average. The majority of reported crashes at the intersection included angle/ sideswipe type collisions ( $75 \%$ ). All of the crashes occurred outside the normal peak commuter traffic periods and seventy-five percent ( $75 \%$ ) of the crashes were personal injury type crashes. There were no pedestrian-related incidents or fatalities reported at the intersection during the 3 -year study period.
- Pond Street at Cottage Court/Auburn Street: There were no reported crashes at this intersection during the three year study period.
- Pond Street at Hillside Avenue: There were no reported crashes at this intersection during the three year study period.

In summary, the study intersections all experienced crash rates well below the District 4 average and no immediate safety countermeasures are warranted based on the crash history at the study intersections.

### 2.5 PUBLIC TRANSPORTATION FACILITIES

The Massachusetts Bay Transit Authority operates the Newburyport commuter rail service in the study area which is located less than 1 mile away on Parker Street. The Merrimack Valley Regional Transit Authority provides bus service immediately adjacent to the Site along Pond Street. Specifically, Bus Route 54 provides service for destinations in Amesbury, Newburyport and Salisbury including the Newburyport Commuter Rail Station. Bus Route 53 (Newburyport Summer Shuttle) also runs immediately adjacent to the Site along Pond Street and generally operates between June and September with service destinations including the Newburyport Commuter Rail Station and Plum Island. Specific route and schedule information is provided in the Appendix.

### 2.6 SIGHT LINE ANALYSIS

An evaluation of sight lines was conducted at the proposed site egress driveway location along Route 1 to ensure that minimum recommended sight lines will be available at the proposed site driveway intersection with Route 1. The evaluation documents sight lines under proposed conditions for vehicles as they relate to Route 1 with comparison to recommended guidelines.

The American Association of State Highway and Transportation Officials' (AASHTO) standards ${ }^{1}$ reference two types of sight distance which are relevant at the proposed site egress driveway intersection along Route 1: stopping sight distance (SSD) and intersection sight distance (ISD). Sight lines for critical vehicle movements at the proposed site driveway intersection with Route 1 were compared to minimum SSD and ISD recommendations for the regulatory speed limit posted in the area as well as ambient travel speeds recorded along Route 1 northbound near the site.

## Stopping Sight Distance

Sight distance is the length of roadway visible to the motorist to a fixed object. The minimum sight distance available on a roadway should be sufficiently long enough to enable a belowaverage operator, traveling at or near the design speed, to stop safely before reaching a stationary object in its path, in this case, a vehicle exiting onto Route 1. The SSD criteria are defined by AASHTO based on design and operating speeds, anticipated driver behavior and vehicle performance, as well as physical roadway conditions. SSD includes the length of roadway traveled during the perception and reaction time of a driver to an object, and the distance traveled during brake application on wet level pavement. Adjustment factors are applied to account for roadway grades when applicable.

SSD was estimated in the field using AASHTO standards for driver's eye ( 3.5 feet) and object height equivalent to the taillight height of a passenger car ( 2.0 feet) for the northbound Route 1 approach to the proposed site driveway. Table 4 presents a summary of the available SSD as they relate to Route 1 and AASHTO's recommended SSD based on posted and observed ambient travel speeds along Route 1. Speed study data is provided in the Attachments.

TABLE 4
STOPPING SIGHT DISTANCE SUMMARY ROUTE 1 NB APPROACH TO PROPOSED SITE DRIVEWAY

|  |  | AASHTO Recommended ${ }^{1}$ |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Approach/ |  | Posted |  |  |
| Travel | Available | Speed | Average | 85 ${ }^{\text {th }}$ Percentile |
| Direction | SSD | (45 mph) | Observed Speed ${ }^{2}$ | Observed Speed ${ }^{3}$ |
| Northbound | $430 \pm$ Feet | 360 Feet | 325 Feet | 400 Feet |

${ }^{1}$ Recommended sight distance based on AASHTO, A Policy on Geometric Design of Highways and Streets based on driver height of eye of 3.5 feet to object height of 2 feet
${ }^{2}$ Average travel speed of 42 MPH northbound
${ }^{3} 85^{\text {th }}$ percentile travel speed of 48 MPH northbound

[^0]As summarized in Table 4, the existing available sight lines exceed AASHTO's recommended SSD criteria for the regulatory speed limit as well as for the higher observed $85^{\text {th }}$ percentile travel speed along Route 1. Stopping sight distance calculations are provided in the Attachments.

## Intersection Sight Distance

Clear sight lines provide sufficient sight distance for a stopped driver on a minor-road approach to depart from the intersection and enter or cross the major road. AASHTO's ISD criteria are defined into several "cases". In this case, the proposed site egress driveway approach to the intersection is proposed to be under STOP signal control and the ISD in question relates to the ability to turn right onto Route 1.

Available ISD was estimated in the field using AASHTO standards for driver's eye ( 3.5 feet), object height ( 3.5 feet) for the northbound direction along Route 1 . Table 5 presents a summary of the available ISD for the departure from the proposed site driveway and AASHTO's ideal ISD.

TABLE 5
INTERSECTION SIGHT DISTANCE SUMMARY PROPOSED SITE DRIVEWAY DEPARTURE TO ROUTE 1 NB

|  |  | AASHTO Minimum ${ }^{\text { }}$ |  | AASHTO Ideal ${ }^{1}$ |
| :---: | :---: | :---: | :---: | :---: |
| Approach/ Travel Direction | Available ISD $^{2}$ | Posted Speed Limit ( 45 mph ) | 85 ${ }^{\text {th }}$ Percentile Observed Speed ${ }^{2}$ | Posted Speed Limit ( 45 mph ) |
| Looking South | $430 \pm$ Feet $^{\text {3 }}$ | 360 Feet | 400 Feet | 430 Feet |

${ }^{1}$ Recommended sight distance based on AASHTO, A Policy on Geometric Design of Highways and Streets. Based on driver height of eye of 3.5 feet and an object height of 3.5 feet and adjustments for roadway grade if required. Minimum value as noted represents SSD per AASHTO guidance.
${ }^{285}{ }^{\text {th }}$ percentile travel speed of 48 MPH northbound
${ }^{3}$ Assumes selective clearing of existing on-site vegetation and obstructions (i.e., retaining wall) and on-site re-grading.
The results of the ISD analysis presented in Table 4 indicate that minimum ISD criteria would be exceeded from the proposed site egress driveway looking south onto Route 1 and ideal ISD criteria would be met or nearly met. The results assume selective clearing of existing on-site vegetation and obstructions (i.e., retaining wall) along the site frontage and on-site re-grading conducted during driveway construction. The specific limits of on-site regrading should be further reviewed as the site design progresses.

### 3.0 FUTURE CONDITIONS

Evaluation of the proposed development impacts requires the establishment of a future baseline analysis condition. This section estimates future roadway and traffic conditions with and without the proposed development. To be consistent with EEA/MassDOT guidelines, a seven year planning horizon was selected.

To determine the impact of site-generated traffic volumes on the roadway network under future conditions, baselime traffic volumes in the study area were projected to a future year condition. Traffic volumes on the roadway network at that time, in the absence of the development (that is, the No-Build condition), would include existing traffic, new traffic due to general background traffic growth, and traffic related to specific development by others that is currently under review at the local and/or state level. Consideration of these factors resulted in the development of No-Build traffic volumes. Anticipated site-generated traffic volumes were then superimposed upon these No-Build traffic-flow networks to develop future Build conditions.

The following sections provide an overview of future No-Build traffic volumes and projected Build traffic volumes.

### 3.1 BACKGROUND TRAFFIC GROWTH

Background traffic includes demand generated by other planned developments in the area as well as demand increases caused by external factors. External factors are general increases in traffic not attributable to a specific development and are determined using historical data.

### 3.1.1 Historical Area Growth

Nearby permanent count station data published by MassDOT indicates a 0.4 percent annual growth rate. For planning purposes, a 0.5 percent annual growth rate is used. This correlated to an approximate 3.6 percent increase over a 7-year horizon. This growth rate is slightly higher than historic rates, and, as such, is also expected to account for any small fluctuation in hourly traffic as may occur from time to time in the study area and small background developments or vacancies in the area. MassDOT permanent count station data and background growth calculations are provided in the Appendix.

### 3.1.2 Background Development-Related Growth

Development of future No-Build traffic volumes considers traffic generated through the study area from other specific area developments. Review of Massachusetts Environmental Policy Act (MEPA) files and a review of the project area indicate that there is one planned development project in the area:

- Residential Development: The development is an approximate 1.5-acre tract of land located along Newburyport Turnpike (Route 1) north of Hill Street in Newburyport, Massachusetts. Under the proposed development plan, eight residential townhouse/condominium units will be constructed. Information provided in the Traffic Impact Assessment ${ }^{2}$ for the development indicates that the projected would generate 5 peak hour trips; a level that is accounted for in the general background traffic growth rate. The site-specific trip tracings are provided in the Appendix.


### 3.2 NO-BUILD TRAFFIC VOLUMES

To account for future traffic growth in the study area, the half (0.5) percent annual growth rate was applied to the existing (baseline) traffic volumes compounded annually over 7 years. Future No-Build traffic volumes are displayed in Figure 4.

[^1]

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### 3.3 SITE-GENERATED TRAFFIC-ITE BASIS

Future Build condition traffic volumes were developed by estimating the number of peak-hour trips expected to be generated by the proposed development, and distributing this additional traffic onto the local roadway network. These future development-related trips were added to future No-Build traffic volumes to evaluate future traffic operations with the proposed residential development in place. The methodology utilized to estimate the future tripgeneration characteristics of the proposed development are summarized below. In accordance with EEA/MassDOT guidelines, the traffic generated by the proposed development was estimated using trip rates published in ITE's Trip Generation for the Land Use Code (LUC) based on trip rates for Apartments (LUC 220). The trip generation calculation worksheet is provided in the Appendix.

Table 6 presents the trip-generation estimates for the proposed development (including the long range build-out of the 10 bedroom YWCA building) based on ITE methodology and EEA/MassDOT guidelines.

TABLE 6
TRIP-GENERATION SUMMARY

| Peak Hour/Direction | Apartments (58 Units) ${ }^{2}$ |
| :---: | :---: |
| Weekday Morning Peak Hour: |  |
| Entering | 6 |
| Exiting | $\underline{24}$ |
| Total | 30 |
| Weekday Evening Peak Hour: |  |
| Entering | 23 |
| Exiting | 13 |
| Total | 36 |
| Weekday Daily: | 386 |

ITE LUC 220 - Apartment applied to 58 units.
As summarized in Table 6, based on industry-standard trip rates, the proposed development is estimated to generate approximately 30 vehicle trips during the weekday morning peak hour ( 6 entering and 24 exiting) and 36 vehicle trips during the weekday evening peak hour (23 entering and 13 exiting). On a daily basis, the development is estimated to generate approximately 386 vehicle trips on a weekday.

### 3.4 TRIP DISTRIBUUTION AND ASSIGNMENT

The distribution for projected traffic for the proposed residential development is based primarily on Journey to Work data published by the US Census and the efficiency of the roadways serving the site. The resulting trip distribution for new trips is presented in Figure 5. Trip distribution calculations are provided in the Appendix.

Development-related trips for the Site were assigned to the roadway network using the ITE trip-generation estimates shown in Table 6 and the distribution patterns presented in Figure 5. New development-related trips at each intersection during the peak hours are quantified in Figure 6.

### 3.5 BUILD TRAFFIC VOLUMES

Future Build condition traffic volumes were arrived at by adding development-specific traffic volumes to the 2022 No-Build conditions. The 2022 Build condition traffic-volume networks for the peak hours are displayed in Figure 7.

Scale: Not to Scale

## MDM Planners \& Engineers

[^2]Newburyport, Massachusetts


Figure 6


Figure 7

Intersection capacity analyses are presented in this section for the Existing, No-Build, and Build traffic-volume conditions. Capacity analyses, conducted in accordance with EEA/MassDOT guidelines, provide an index of how well the roadway facilities serve the traffic demands placed upon them. The operational results provide the basis for recommended access and roadway improvements in the following section.

### 4.1 CAPACITY ANALYSIS PROCEDURES

Capacity analysis of intersections is developed using the Synchro ${ }^{\circledR}$ computer software, which implements the methods of the 2010 Highway Capacity Manual (HCM). The resulting analysis presents a level-of-service (LOS) designation for individual intersection movements. The LOS is a letter designation that provides a qualitative measure of operating conditions based on several factors including roadway geometry, speeds, ambient traffic volumes, traffic controls, and driver characteristics. Since the LOS of a traffic facility is a function of the traffic flows placed upon it, such a facility may operate at a wide range of LOS, depending on the time of day, day of week, or period of year. A range of six levels of service are defined on the basis of average delay, ranging from LOS A (the least delay) to LOS F (delays greater than 50 seconds for unsignalized movements and 80 seconds for signalized movements). The specific control delays and associated LOS designations are presented in the Appendix.

## 4. 2 INTERSECTION CAPACITY ANALYSIS RESULTS

Capacity analysis results for the weekday morning and weekday evening peak hour capacity analysis results for the unsignalized and signalized study intersections are described below, with detailed analysis results presented in the Appendix.

### 4.2.1 Level of Service Analysis

The capacity analysis results for the intersections in the study area are summarized in Table 7 and Table 8 for the weekday morning and weekday evening peak hours, respectively. Detailed analysis results are presented in the Appendix.

TABLE 7
INTERSECTION CAPACITY ANALYSIS RESULTS - WEEKDAY MORNING PEAK HOUR

| Intersection | Approach | 2015 Existing |  |  | 2022 No-Build |  |  | 2022 Build |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{v} / \mathrm{c}^{1}$ | Delay ${ }^{2}$ | $L^{\text {LOS }}{ }^{3}$ | $\mathrm{v} / \mathrm{c}$ | Delay | LOS | $\mathrm{v} / \mathrm{c}$ | Delay | LOS |
| Route 1 at | Eastbound | 0.74 | 36 | D | 0.76 | 37 | D | 0.78 | 38 | D |
| Low Street/ | Westbound | 0.50 | 41 | D | 0.52 | 42 | D | 0.54 | 42 | D |
| Pond Street | Northbound | 0.58 | 30 | C | 0.60 | 31 | C | 0.63 | 32 | C |
|  | Southbound | 0.62 | $\underline{33}$ | C | $\underline{0.64}$ | 33 | C | $\underline{0.64}$ | $\underline{34}$ | C |
|  | Overall | 0.74 | 34 | C | 0.76 | 34 | C | 0.78 | 35 | D |
| Pond Street at | Eastbound | 0.02 | $<5$ | A | 0.02 | $<5$ | A | 0.02 | $<5$ | A |
| Cottage Court/ | Westbound | 0.01 | $<5$ | A | 0.01 | $<5$ | A | 0.01 | $<5$ | A |
| Auburn Street | NB Exit | 0.00 | 10 | A | 0.00 | 10 | A | 0.00 | 10 | A |
|  | SB Exit | 0.02 | 9 | A | 0.02 | 9 | A | 0.02 | 9 | A |
| Pond Street at | Eastbound | 0.00 | $<5$ | A | 0.00 | $<5$ | A | 0.00 | $<5$ | A |
| Hillside Avenue | Westbound | 0.00 | $<5$ | A | 0.00 | $<5$ | A | 0.00 | <5 | A |
|  | NB Exit | 0.00 | $<5$ | A | 0.00 | $<5$ | A | 0.01 | 10 | A |
| Route 1 at | WB R Exit | $n / a^{4}$ | n/a | n/a | n/a | n/a | $n / \mathbf{a}$ | 0.00 | 9 | A |
| Proposed | Northbound | n/a | n/a | n/a | n/a | n/a | n/a | 0.02 | $<5$ | A |
| Site Driveway |  |  |  |  |  |  |  |  |  |  |

${ }^{1}$ Volume-to-capacity ratio
${ }^{2}$ Average control delay per vehicle (in seconds)
${ }^{3}$ Level of service
${ }^{4}$ Not Applicable

TABLE 8
INTERSECTION CAPACITY ANALYSIS RESULTS - WEEKDAY EVENING PEAK HOUR

| Intersection | Approach | 2015 Existing |  |  | 2022 No-Build |  |  | 2022 Build |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{v} / \mathrm{c}^{1}$ | Delay ${ }^{2}$ | $\mathrm{LOS}^{3}$ | $\mathrm{v} / \mathrm{c}$ | Delay | LOS | $\mathrm{v} / \mathrm{c}$ | Delay | LOS |
| Route 1 at | Eastbound | 0.81 | 39 | D | 0.85 | 43 | D | 0.88 | 46 | D |
| Low Street/ | Westbound | 0.51 | 39 | D | 0.53 | 40 | D | 0.53 | 40 | D |
| Pond Street | Northbound | 0.62 | 30 | C | 0.63 | 30 | C | 0.65 | 30 | C |
|  | Southbound | 0.57 | 33 | C | 0.58 | 34 | C | 0.58 | 34 | C |
|  | Overall | 0.81 | 34 | C | 0.85 | 35 | D | 0.88 | 37 | D |
| Pond Street at | Eastbound | 0.02 | $<5$ | A | 0.02 | $<5$ | A | 0.02 | $<5$ | A |
| Cottage Court/ | Westbound | 0.00 | $<5$ | A | 0.00 | $<5$ | A | 0.00 | $<5$ | A |
| Auburn Street | NB Exit | 0.03 | 12 | B | 0.03 | 12 | B | 0.03 | 12 | B |
|  | SB Exit | 0.02 | 9 | A | 0.03 | 9 | A | 0.03 | 10 | A |
| Pond Street at | Eastbound | 0.00 | $<5$ | A | 0.00 | $<5$ | A | 0.00 | $<5$ | A |
| Hillside Avenue | Westbound | 0.00 | $<$ | A | 0.00 | $<5$ | A | 0.00 | $<5$ | A |
|  | NB Exit | 0.00 | 10 | A | 0.00 | 10 | A | 0.01 | 10 | A |
| Route 1 at | WB R Exit | $n / \mathrm{a}^{4}$ | n/a | n/a | n/a | n/a | n/a | 0.00 | 10 | A |
| Proposed | Northbound | n/a | n/a | r/a | n/a | n/a | n/a | 0.01 | $<5$ | A |
| Site Driveway |  |  |  |  |  |  |  |  |  |  |

[^3]- Route 1 at Low Street/ Pond Street: Under existing and future No-Build conditions, the signalized intersection of Route 1 and Low Street will operate at an overall level of service (LOS) D or better during the peak hours. With the addition of the project, the intersection will continue to operate at an overall LOS D or better with no material increases in delay.
- Pond Street at Cottage Court/Auburn Street: Under Build conditions, the minor street approaches to the intersection will continue operate at LOS B or better during the peak hours with no material increases in delay compared to No-Build conditions.
- Pond Street at Hillside Avenue: Under Build conditions, the minor street approaches to the intersection will continue operate at LOS A during the peak hours with no material increases in delay compared to No-Build conditions.
- Route 1 at Proposed Site Driveway: Under future Build conditions with the proposed development in place, the Route 1 intersection with the right-in/right-out proposed site driveway will operate well under capacity at LOS A with minimal delay during the peak hours.

In summary, the incremental changes in traffic at the study intersections due to the proposed development do not result in any significant change in intersection operations at the study intersections compared to No-Build conditions. Under Build conditions, the site driveway intersection with Route 1 and nearby signalized intersection will continue to operate under capacity during the peak hours with no material change in delay.

### 4.2.3 Vehicle Queue Analysis

Vehicle queue results are presented for the signalized study intersection. These vehicle queues are compared to available storage lengths, which are defined as lengths of exclusive turn lanes or the distance to the nearest major intersection for through lanes. Vehicle queue results from the capacity analysis are summarized in Table 9 for the signalized study intersection of Route 1 at Low Street/Pond Street. Detailed worksheets of the queuing analysis are provided in the Appendix.

TABLE 9
VEHICLE QUEUE ANALYSIS SUMMARY
ROUTE 1 AT LOW STREET/ POND STREET

| Approach | Storage <br> Length (feet) | 2022 No-Build |  | 2022 Build |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Average Queue Length | 95* Percentile <br> Queue <br> Length | Average Queue Length | 95 ${ }^{\text {H }}$ Percentile <br> Queue <br> Length |
| Weekday Morning Peak Hour |  |  |  |  |  |
| Eastbound L/T | $>1000$ | 149 | 318 | 156 | 325 |
| Eastbound R | 150 $\pm$ | 33 | 68 | 33 | 68 |
| Westbound L/T/R | >1000 | 89 | 164 | 93 | 168 |
| Northbound L | $165 \pm$ | 86 | 160 | 95 | 173 |
| Northbound T, T/R | $>1500$ | 47 | 79 | 49 | 81 |
| Southbound L | $165 \pm$ | 19 | 52 | 20 | 53 |
| Southbound T, T/R | >1500 | 158 | 283 | 161 | 283 |
| Weekday Evening Peak Hour |  |  |  |  |  |
| Eastbound L/T | >1000 | 179 | 422 | 189 | 445 |
| Eastbound R | $150 \pm$ | 26 | 59 | 26 | 59 |
| Westbound L/T/R | $>1000$ | 88 | 174 | 89 | 175 |
| Northbound L | 165士 | 93 | 184 | 97 | 190 |
| Northbound T, T/R | $>1500$ | 98 | 160 | 100 | 162 |
| Southbound L | $165 \pm$ | 31 | 78 | 34 | 83 |
| Southbound T, T/R | $>1500$ | 133 | 214 | 134 | 214 |

${ }^{1}$ Average and $95^{\text {th }}$ percentile queue lengths are reported in feet per lane.
As presented in Table 9, average and $95^{\text {th }}$ percentile vehicle queues at the signalized study intersections are generally contained within available storage areas during the peak hours. Incremental impacts due to the proposed project are minor, generally representing an increase of one additional vehicle queue length or less for impacted movements and in many cases no increase at all.

### 5.0 RECOMMENDATIONS AND CONCLUSIONS

### 5.1 RECOMMENDATIONS

MDM finds that travel conditions in the site vicinity along Route 1 and Pond Street are generally unconstrained. Trip generation for the development is estimated at approximately 30 vehicle-trips during the weekday morning peak hour and 36 vehicle-trips during the weekday evening peak hour. Traffic impacts associated with the proposed apartment development are not expected to notably affect travel or safety conditions in the site vicinity. MDM recommends the following access-related improvements:

## Route 1 at Proposed Site Driveway

MDM recommends the following access-related improvements which are subject to MassDOT permitting and approval, as shown in Figure 8:

- A "STOP" sign (R1-1) and STOP line pavement marking are recommended on the driveway approach to Route 1. A "no left turn" sign (R3-2) should be installed opposite the Site in the median of Route 1 to enhance the right turn only restriction. The signs and pavement markings shall be compliant with the Manual on Uniform Traffic Control Devices (MUTCD).
- The existing "traffic signal ahead" sign (W3-3) will need to be relocated given the conflict with the location of the proposed site driveway.
- The driveway alignment, widths and curb radii should been designed to achieve approximate perpendicular orientation with Route 1 . The final curb radii should also be designed to accommodate the largest anticipated design vehicle.

- The driveway has been designed restrict the driveway movements to right-in/right-out movements. To enhance the turn restriction, the driveway will incorporate pavement markings, a raised channelized right turn island and MUTCD compliant signage.
- Plantings (shrubs, bushes) and structures (walls, fences, etc.) shall be maintained at a height of 2 feet or less within the sight lines in vicinity of the Site driveways to provide unobstructed sight lines. Furthermore, the existing vegetation and structures within the sight lines shall be selectively cleared when the Site driveway is constructed and the terrain shall be graded as required to ensure minimum recommended sight line requirements are met or exceeded.

Pond Street at Cottage Court
ㅁ A "STOP" sign (R1-1) is recommended on the Cottage Court approach to Pond Street. The sign shall be compliant with the MUTCD.

ㅁ The existing dead-end sign (W14-1) should be removed when the Cottage Court is extended through the Site to Route 1.
$\square$ Given the close proximity (less than 100 feet) to the traffic signal control at the Route 1/Pond Street intersection, a "Do Not Block Intersection" sign and markings are recommended at the Pond Street/Auburn Street/Cottage Court intersection to enhance operations for left-turn movements at the intersection. All signs and marking shall be in conformance with the MUTCD.

Pond Street at Hillside Avenue

ㅁ A "STOP" sign (R1-1) is recommended on the Hillside Avenue approach to Pond Street. The sign shall be compliant with the MUTCD.

### 5.2 CONCLUSIONS

While the project will increase traffic in the immediate study area, adequate capacity is available under future Build conditions along Route 1, Pond Street, Low Street and at the study intersections to accommodate the trip increases associated with the proposed apartment development. The project is not projected to significantly change any reported operating levels compared to future No-Build conditions, thus no off-site mitigation is recommended. Proposed access improvements will provide ample capacity to accommodate site-generated traffic while also enhancing safety and capacity. In addition, proposed access/egress will be designed to enhance vehicular connections to the site and to ensure that adequate sight lines are provided in accordance with AASHTO criteria based on ambient travel speeds.

## APPENDIX

- Traffic Volume Data
$\square$ Seasonal/ Yearly Growth Data
- Speed Data
- Crash Data
$\square$ Public Transportation
$\square$ Sight Distance Calculations
- Background Growth
- Trip Generation Calculations
$\square$ Trip Distribution Calculations
- Capacity Analyses
- Traffic Volume Data


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Marlborough, MA 01752
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N/S: Rte. 1
/W: Pond St./Low St. . lewburyport, MA

File Name : Rte 1 at Pond 7-9
Site Code : 00234001
Start Date : 8/5/2015
Page No : 2

| + | Rte. 1 From North |  |  |  |  | Pond Street From East |  |  |  |  | Rte. 1 From South |  |  |  |  | Low Street From West |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Stant Time | Right | Thru | Left | Peds | App. To | Right | Thru | Left | Peds | App. To | Right | Thru | Left | Peds | App Total | Right | Thru | Left | Peds | App. 1 | mit Total |

Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1
Deak Hour for Entire Intersection Begins at 08:00 AM

| 08:00 AM | 42 | 103 | 6 | 1 | 152 | 3 | 19 | $\ddagger$ | 0 | 23 | 2 | 44 | 33 | 0 | 79 | 35 | 23 | 24 | 0 | 82 | 336 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 08:15 AM | 30 | 85 | 3 | 0 | 118 | 0 | 32 | 2 | 0 | 34 | 1 | 44 | 32 | 1 | 78 | 22 | 19 | 31 | 0 | 72 | 302 |
| 08:30 AM | 35 | 80 | 10 | 0 | 125 | 5 | 34 | 0 | 0 | 39 | 0 | 39 | 32 | 0 | 71 | 29 | 35 | 25 | 0 | 89 | 324 |
| 08:45 AM | 40 | 86 | 10 | 2 | 138 | 3 | 40 | 3 | 0 | 46 | 8 | 56 | 35 | 0 | 99 | 43 | 35 | 43 | 0 | 121 | 404 |
| Fotal Volume | 147 | 354 | 29 | 3 | 533 | 11 | 125 | 6 | 0 | 142 | 11 | 183 | 132 | 1 | 327 | 129 | 112 | 123 | 0 | 364 | 1366 |
| \% App. Total | 27.6 | 66.4 | 5.4 | 0.6 |  | 7.7 | 88 | 4.2 | 0 |  | 3.4 | 56 | 40.4 | 0.3 |  | 35.4 | 30.8 | 33.8 | 0 |  |  |
| PHF | . 875 | . 859 | 725 | . 375 | 877 | 550 | . 781 | 500 | 000 | . 772 | . 344 | . 817 | 943 | . 250 | . 826 | . 750 | 800 | . 715 | 000 | . 752 | 845 |
| Passenger Venicies | 143 | 333 | 28 | 2 | 506 | 11 | 119 | ${ }^{6}$ | 0 | ;36 | ${ }^{17}$ | 173 | ${ }^{128}$ | - | 312 | 123 | 111 | 118 | 0 | 352 | 1305 |
| Passenger Venickes Heavy Vehicle5 | 4 | 21 | 1 | 1 | 27 | 0 | 6 | 0 | 0 | 6 | 0 | 10 | 4 | 1 | 15 | 6 | 1 | 5 | 0 | 12 | 60 |
| fr Heavy Vehicles | 2.7 | 5.9 | 3.4 | 33.3 | 5.1 | 0 | 4.8 | 0 | 0 | 4.2 | 0 | 5.5 | 3.0 | 100 | 4.6 | 4.7 | 0.9 | 4.1 | 0 | 3.3 | 4.4 |



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28 Lord Road, Suite 280
Marlborough, MA 01752
www mdmitrans.com

N/S: Rte. 1
ENW: Pond St./Low St.
. Newburyport, MA

File Name : Rte 1 at Pond 7-9
Site Code : 00234001
Start Date : 8/5/2015
Page No : 1

Groups Printed- Bicycles

|  | Rte. 1 From North |  |  |  |  | Pond Street From East |  |  |  |  | Rte. 1 From South |  |  |  |  | Low Street From West |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | App. Tolal | Right | Thru | Left | Peds | App Total | Right | Thru | Left | Peds ! | APp Totz | Right | Thru | Left | Peds | App. Toxt | int Totai |
| * BREAK *** |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Apprch \% Total \% | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  |  |

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28 Lord Road, Suite 280
Mariborough, MA

I/S:Auburn St/Cottage Ct.
$=/ \mathrm{W}$ : Pond Street
ewburyport, MA

File Name : Pond at Cottage 7-9
Site Code : 00235001
Start Date : 8/5/2015
Page No : 1

Groups Printed- Passenger Vehicles

| , | Auburn Street From North |  |  |  |  | Pond Street From East |  |  |  |  | Cottage Court From South |  |  |  |  | Pond Street From West |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Stant Time | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Totai | Right | Thru | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Torat | int. Total |
| 07:00 AM | 1 | 0 | 0 | 0 | 1 | 1 | 0 | 6 | 0 | 7 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 6 | 0 | 7 | 16 |
| 07:15 AM | 3 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 2 | 5 |
| 07:30 AM | 2 | 0 | 0 | 3 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 4 | 0 | 5 | 10 |
| 07:45 AM | 6 | 0 | 0 | 2 | 8 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 7 | 0 | 7 | 16 |
| Total | 12 | 0 | 0 | 5 | 17 | 1 | 0 | 6 | 0 | 7 | 1 | 0 | 1 | 0 | 2 | 3 | 0 | 18 | 0 | 21 | 47 |


| 08:00 AM | 1 | 0 | 1 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 5 | 0 | 5 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 08:15 AM | 3 | 0 | 0 | 2 | 5 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 4 | 0 | 4 | 10 |
| 08:30 AM | 3 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 6 | 0 | 6 | 10 |
| 08:45 AM | 9 | 1 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 8 | 18 |
| Total | 16 | 1 | 1 | 3 | 21 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 3 | 0 | 0 | 23 | 0 | 23 | 47 |


| Grand Total | 28 | 1 | 1 | 8 | 38 | 1 | 0 | 6 | 0 | 7 | 3 | 0 | 2 | 0 | 5 | 3 | 0 | 41 | 0 | 44 | 94 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Apprch \% | 73.7 | 2.6 | 2.6 | 21.1 |  | 14.3 | 0 | 85.7 | 0 |  | 60 | 0 | 40 | 0 |  | 6.8 | 0 | 93.2 | 0 |  |  |
| Total \% | 29.8 | 1.1 | 1.1 | 8.5 | 40.4 | 1.1 | 0 | 6.4 | 0 | 7.4 | 3.2 | 0 | 2.1 | 0 | 5.3 | 3.2 | 0 | 43.6 | 0 | 46.8 |  |

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28 Lord Road, Suite 280
Marlborough, MA 01752
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N/S: Hillside Ave
W: Pond Street ivewburyport, MA

File Name : Pond at Hillside 7-9
Site Code : 00235001
Start Date : 8/5/2015
Page No : 1

Groups Printed- Passenger Vehicles

| Groups Printed-Passenger Vehicles |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Pond Street From East |  |  |  | Hilliside Avenue From South |  |  |  | Pond Street From West |  |  |  |  |
| Start Time | Thru | Left | Peds | App. Total | Right | Left | Peds | App Total | Right $\mid$ | Thru | Peds | App. Total | Int. Total |
| BREAK *** |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Grand Total Apprch \% Total \% | 0 0 | 0 0 | 0 | 0 | 0 0 | 0 | 0 0 | 0 | 0 0 | 0 0 | 0 0 | 0 | 0 |

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28 Lord Road, Suite 280
Marlborough, MA 01752
www.mdmtrans.com
N/S: Rte. 1
W: Pond St./Low St. , Newburyport, MA

File Name : Rte 1 at Pond 4-6
Site Code : 00234002
Start Date : 8/5/2015
Page No : 1

Groups Printed- Passengeer Vehicles - Heavy Vehicles

|  | Rte. 1 <br> From North |  |  |  |  | Pond Street From East |  |  |  |  | Rte. 1 <br> From South |  |  |  |  | Low Street From West |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | A0p Totea | Right | Thul | Left | Peds | App. Total | Right | Thru | Left | Peds | App Total | Right | Thru | Left | Peds | App. Toral | Int Total |
| 04:00 PM | 23 | 94 | 15 | 1 | 133 | 1 | 27 | 5 | 0 | 33 | 3 | 87 | 46 | 0 | 136 | 32 | 24 | 44 | 0 | 100 | 402 |
| 04:15 PM | 31 | 89 | 14 | 0 | 134 | 3 | 31 | , | 0 | 37 | 3 | 102 | 36 | 0 | 141 | 35 | 30 | 46 | 0 | 111 | 423 |
| 04:30 PM | 34 | 87 | 14 | 3 | 138 | 4 | 29 | 1 | 0 | 34 | 1 | 86 | 47 | 0 | 134 | 24 | 38 | 33 | 0 | 95 | 401 |
| 04:45 PM | 15 | 78 | 11 | 0 | 104 | 4 | 30 | 5 | 0 | 39 | 5 | 100 | 42 | 0 | 147 | 25 | 31 | 40 | 0 | 96 | 386 |
| Total | 103 | 348 | 54 | 4 | 509 | 12 | 117 | 14 | 0 | 143 | 12 | 375 | 171 | 0 | 558 | 116 | 123 | 163 | 0 | 402 | 1612 |


| 05:00 PM | 48 | 84 | 14 | 1 | 147 | 6 | 26 | 4 | 0 | 36 | 1 | 102 | 40 | 0 | 143 | 41 | 25 | 50 | 0 | 116 | 442 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 05:15 PM | 36 | 107 | 14 | 4 | 161 | 2 | 37 | 3 | 0 | 42 | 1 | 97 | 44 | 0 | 142 | 28 | 37 | 45 | 0 | 110 | 455 |
| 05:30 PM | 25 | 88 | 14 | 1 | 128 | 7 | 34 | 4 | 0 | 45 | 6 | 99 | 38 | 1 | 144 | 33 | 31 | 51 | 0 | 115 | 432 |
| ${ }^{3} 05: 45 \mathrm{PM}$ | 26 | 87 | 9 | 1 | 123 | 0 | 18 | 3 | 0 | 21 | 2 | 50 | 30 | 1 | 83 | 19 | 31 | 33 | 0 | 83 | 310 |
| Total | 135 | 366 | 51 | 7 | 559 | 15 | 115 | 14 | 0 | 144 | 10 | 348 | 152 | 2 | 512 | 121 | 124 | 179 | 0 | 424 | 1639 |
| Grand Total | 238 | 714 | 105 | 11 | 1068 | 27 | 232 | 28 | 0 | 287 | 22 | 723 | 323 | 2 | 1070 | 237 | 247 | 342 | 0 | 826 | 3251 |
| Apprch \% | 22.3 | 66.9 | 9.8 | 1 |  | 9.4 | 80.8 | 9.8 | 0 |  | 2.1 | 67.6 | 30.2 | 0.2 |  | 28.7 | 29.9 | 41.4 | 0 |  |  |
| Total \% | 7.3 | 22 | 3.2 | 0.3 | 32.9 | 0.8 | 7.1 | 0.9 | 0 | 8.8 | 0.7 | 22.2 | 9.9 | 0.1 | 32.9 | 7.3 | 7.6 | 10.5 | 0 | 25.4 |  |
| Essengeer vetictes | 229 | 694 | 104 | 7 | 1034 | 26 | 227 | 25 | 0 | 278 | 22 | 713 | 320 | 1 | 1056 | 236 | 243 | 338 | 0 | 817 | 3185 |
| Mr Possorgan vaictes | 96.2 | 97.2 | 99 | 63.6 | 96.8 | 96.3 | 97.8 | 89.3 | 0 | 96.9 | 100 | 98.6 | 99.1 | 50 | 98.7 | 99.6 | 98.4 | 98.8 | 0 | 98.9 | 98 |
| Heavy Vehicies | 9 | 20 | 1 | 4 | 34 | 1 | 5 | 3 | 0 | 9 | 0 | 10 | 3 | 1 | 14 | 1 | 4 | 4 | 0 | 9 | 66 |
| \%\% Heany Vericles | 3.8 | 2.8 | 1 | 36.4 | 3.2 | 3.7 | 2.2 | 10.7 | 0 | 3.1 | 0 | 1.4 | 0.9 | 50 | 1.3 | 0.4 | 1.6 | 1.2 | 0 | 1.1 | 2 |

# MDM Transportation Consultants, Inc. 

28 Lord Road, Suite 280 Mariborough, MA 01752
www.mdmtrans.com
N/S: Cottage Ct./Auburn St.
/W: Pond St
sewburyport,MA
Then Click the Comments Tab

File Name : Pond at Cottage 4-6
Site Code : 00235002
Start Date : 8/5/2015
Page No : 2

|  | Auburn Street From North |  |  |  |  | Pond Street From East |  |  |  |  | Cottage Court From South |  |  |  |  | Pond Street From West |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru $\mid$ | Left | Peds | App. Total | Right | Thus | Left | Peds | App. Total | Right | Thru | Left | Peds | App. Taral | Right | Thru | Left | Peds | App Total | Int Total |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Fak Hour for Entire Intersection Begins at 04:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 04:00 PM | 7 | 1 | 0 | 1 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 0 | 0 | $1 i$ | 0 | 10 | 23 |
| 04:15 PM | 5 | 0 | 0 | 0 | 5 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 8 | 14 |
| 04:30 PM | 3 | 0 | 1 | 4 | 8 | 1 | 0 | 1 | 0 | 2 | 0 | 1 | 3 | 0 | 4 | 2 | 0 | 5 | 0 | 7 | 21 |
| 04:45 PM | 2 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 6 | 2 | 0 | 2 | 0 | 4 | 12 |
| Total Volume | 17 | 1 | 1 | 5 | 24 | 1 | 0 | 2 | 0 | 3 | 0 | 1 | 12 | 0 | 13 | 4 | 0 | 26 | 0 | 30 | 70 |
| \% App. Total | 70.8 | 4.2 | 4.2 | 20.8 |  | 33.3 | 0 | 66.7 | 0 |  | 0 | 7.7 | 92.3 | 0 |  | 13.3 | 0 | 86.7 | 0 |  |  |
| PHF | . 607 | . 250 | . 250 | . 313 | . 667 | . 250 | 000 | . 500 | . 000 | . 375 | 000 | 250 | 500 | 000 | 542 | 500 | . 000 | . 591 | 000 | 682 | . 761 |



# MDM Transportation Consultants, Inc. 

28 Lord Road, Suite 280
Marlborough, MA 01752
noww.mdmtrans.com

N/S: Hillside Ave
N: Pond St
, Newburyport,MA

File Name : Pond at Hillside 4-6
Site Code : 00235002
Start Date : 8/5/2015
Page No : 2

|  | Pond Street From East |  |  |  | Hillside Avenue From South |  |  |  | Pond Street <br> From West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Thru | Left | Peds | App. Total | Right | Left | Peds | App. Total | Right | Thru | Peds | App. Total | Int Total |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| -ak Hour for Entir | ersec | Begin | $104: 30$ | PM |  |  |  |  |  |  |  |  |  |
| 04:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 2 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 05:00 PM | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 3 |
| 05:15 PM | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 3 | 0 | 0 | 0 | 0 | 3 |
| Total Volume | 0 | 2 | 0 | 2 | 1 | 2 | 0 | 3 | 3 | 0 | 0 | 3 | 8 |
| \% App. Total | 0 | 100 | 0 |  | 33.3 | 66.7 | 0 |  | 100 | 0 | 0 |  |  |
| PHF | . 000 | . 250 | . 000 | 250 | 250 | . 250 | 000 | . 250 | . 375 | . 000 | . 000 | 375 | . 667 |



## - Seasonal Data/ Yearly Growth



## Speed Data

## MDM Transportation Consultants, Inc.

28 Lord Road, Suite 280 Marlborough, MA 01752
www.mdmtrans.com

Route 1
South of Pond Street
Newburyport, MA

File Name : rte 1 spot speed
Site Code : 848
Start Date : 9/2/2015
Page No : 1

| \# | Northbound |
| :---: | :---: |
| 1 | 47 |
| 2 | 47 |
| 3 | 47 |
| 4 | 37 |
| 5 | 42 |
| 6 | 38 |
| 7 | 40 |
| 8 | 39 |
| 9 | 46 |
| 10 | 40 |
| 11 | 32 |
| 12 | 45 |
| 13 | 55 |
| 14 | 42 |
| 15 | 39 |
| 16 | 38 |
| 17 | 44 |
| 18 | 43 |
| 19 | 40 |
| 20 | 47 |
| 21 | 48 |
| 22 | 38 |
| 23 | 40 |
| 24 | 43 |
| 25 | 38 |
| 26 | 39 |
| 27 | 44 |
| 28 | 42 |
| 29 | 40 |
| 30 | 50 |
| 31 | 52 |
| 32 | 38 |
| 33 | 45 |
| 34 | 38 |
| 35 | 39 |
| 36 | 50 |
| 37 | 36 |
| 38 | 37 |
| 39 | 39 |
| 40 | 39 |
| 41 | 45 |
| 42 | 52 |
| 43 | 41 |
| 44 | 40 |
| 45 | 50 |
| 46 | 40 |
| 47 | 34 |
| 48 | 54 |
| 49 | 37 |
| 50 | 38 |
| 51 | 39 |
| 52 | 49 |
| 53 | 44 |
| 54 |  |


| Class | Vehicle Count | Average Speed | True Median (50th Percentile) | $\begin{gathered} 85 \\ \text { Percentile } \end{gathered}$ | 10 MPH <br> Pace Speed | Number in Pace | Percent in Pace | Number of Vehicles Over 45 MPH | Percent of Vehicles Over 45 MPH |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Northbound | 53 | 42 | 40 | $4 \overline{8}$ | 38-47 | 38 | 72 | 14 | 26 |

## INTERSECTION CRASH RATE WORKSHEET



PEAK HOUR VOLUMES
APPROACH :
DIRECTION :
PEAK HOURLY VOLURES (PMI) :

| $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ | $\mathbf{5}$ | Total Peak <br> Hourly <br> Approach <br> Volume |
| :---: | :---: | :---: | :---: | :---: | :---: |
| EB | WB | SB | NB |  | W7.75, |
| 437 | 162 | 540 | 576 |  |  |

"K" FACTOR: $\square$ INTERSECTION ADT $(V)=$ TOTAL DAILY APPROACH VOLUME :

19,056

TOTAL \# OF CRASHES : 4


AVERAGE \# OF CRASHES PER YEAR ( A):

CRASH RATE CALCULATION:
$0.19, \quad$ RATE $=\frac{(A * 1,000,000)}{(V * 365)}$
Comments : MassDOT District 4 Avg: Signalized $=0.77$; Unsignalized $=0.58$
Project Title \& Date: 848 - Newburyport

$\square$ Public Transportation


|  | 9:54 | 10:00 | 10:10 | 10:20 | 10:23 | 10:29 | 10:36 | 10:45 | 10:50 | 10:52 | 51 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PM | 11:04 | 11:10 | 11:20 | 11:30 | $11: 33$ | 11:39 | 11:46 | 11:55 | 12:00 | 12:02 | 51 |
|  | 12:14 | 12:20 | 12:30 | 12:40 | 12:43 | 12:49 | 12:56 | 1:05 | 1:10 | 1:12 | 51 |
|  | 1:24 | 1:30 | 1:40 | 1:50 | 1:53 | 1:59 | 2:06 | 2:15 | 2:20 | 2:22 | 51 |
|  | 2:34 | 2:40 | 2:50 | 3:00 | 3:03 | $3: 09$ | 3:16 | 3.25 | $3: 30$ | 3:32 | 51 |
|  | 3:44 | $3: 50$ | $4: 00$ | $4: 10$ | 4:13 | 4:19 | $4: 26$ | 4:35 | 4:40 | 4:42 | 51 |
|  | 4:54 | 5:00 | 5:10 | 5:20 | 5:23 | 5:29 | 5:36 | 5:45 | 5:50 | 5:52 | 51 |
|  | 6:04 | 6:10 | 6:20 | 6:30 | 6:33 | 6:39 | 6:46 | 6:55 | 7:00 | 7:02 | 51 |
| SATURDAY/SUNDAY |  |  |  |  |  |  |  |  |  |  |  |
| AM | 7:34* | 7:40* | 7:50* | 8:00 | 8:03 | 8:09 | 8:16 | 8:25 | 8:30 | 8:32 | 51 |
|  | 8:44 | $8: 50$ | 9:00 | 9:10 | 9:13 | 9:19 | 9:26 | 9:35 | 9:40 | 9:42 | 51 |
|  | 9:54 | 10:00 | 10:10 | 10:20 | 10:23 | 10:29 | 10:36 | 10:45 | 10:50 | 10:52 | 51 |
| PM | 11:04 | $11: 10$ | 11:20 | 11:30 | $11: 33$ | 11:39 | 11:46 | 11:55 | 12:00 | 12:02 | 51 |
|  | 12:14 | 12:20 | 12:30 | 12:40 | 12:43 | 12:49 | 12:56 | 1:05 | 1:10 | 1:12 | 51 |
|  | 1:24 | 1:30 | 1:40 | 1:50 | 1:53 | $1: 59$ | 2:06 | 2:75 | $2: 20$ | 2:22 | 51 |
|  | 2:34 | 2:40 | 2:50 | 3:00 | 3:03 | 3.09 | 3:16 | 3:25 | 3:30 | 3:32 | 51 |
|  | $3: 44$ | $3: 50$ | $4: 00$ | $4: 10$ | $4: 13$ | 4:19 | $4: 26$ | $4: 35$ | 4:40 | $4: 42$ | 51 |
|  | 4:54 | 5:00 | 5:10 | $5: 20$ | $5: 23$ | $5: 29$ | 5:36 | 5:45 | 5:50 | 5:52 | 51 |
|  | 6:04* | 6:10* | 6:20* | 6:30* | 6:33* | 6:39* | 6:46* | 6:55* | 7:00* | 7:02* | 51 |



## Summer Shuttle Schedule

Friday, Saturday \& Sunday Service Only - MAY 29 - SEPTEMBER 6, 2015
洨
*FINAL TRAIN TO NORTH STATION - Friday 5:26 p.m. / Weekends 5:34 p.m.
$\square$ Sight Distance Calculations

Route 1 - Posted Speed Limit

|  | BRAKE <br> SPEED <br> (MPH) | REACTION <br> DISTANCE <br> (FT) | BRAKING DISTANCE <br> (FT) | CALCULATED STOPPING <br> SIGHT DISTANCE <br> (FT) |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| Direction 1 |  |  |  |  |
|  | 45 | 165.375 | 194.4 | 359.7 |

INPUTS
Travel Direction NB
Speed 45
t 2.5
a 11.2

## Stopping Sight Distance (SSD) - Source: AASHTO

SSD = Reaction Distance + Brake Distance
Reaction Distance $=1.47 \times t \times V$
Brake Distance $=1.075 \mathrm{xV}^{\wedge} 2 / \mathrm{a}$
Where:
$t=$ reaction time (sec)
$\mathrm{V}=$ travel speed (mph)
a - deceleration rate ( $\mathrm{f} / \mathrm{sec}^{\wedge} 2$ )

## Stopping Sight Distance

Route 1-85th Percentile Observed Travel Speeds

|  | BRAKE <br> SPEED <br> $(M P H)$ | REACTION <br> DISTANCE <br> $(\mathrm{FT})$ | BRAKING DISTANCE <br> (FT) | CALCULATED STOPPING <br> SIGHT DISTANCE <br> (FT) |
| :--- | :---: | :---: | :---: | :---: |
|  |  |  |  |  |
| Direction $1 \quad$ NB | 48 |  |  |  |
|  |  |  | 221.1 | 397.5 |

INPUTS

| Travel Direction | NB |
| :--- | ---: |
| Speed | 48 |
| t | 2.5 |
| a | 11.2 |

## Stopping Sight Distance (SSD) - Source: AASHTO

SSD $=$ Reaction Distance + Brake Distance
Reaction Distance $=1.47 \times t \times V$
Brake Distance $=1.075 \times \mathrm{V}^{\wedge} 2 / \mathrm{a}$
Where:
$\mathrm{t}=$ reaction time (sec)
$V=$ travel speed (mph)
a - deceleration rate (ft/sec^2)

- Background Growth

Newburyport, Massachusetts

$\square$ Trip Generation Calculations

Institute of Transportation Engineers (ITE) 9th Edition Land Use Code (LUC) 220 - Apartment

Average Vehicle Trips Ends vs: Dwelling Units Independent Variable (X): 58

```
Average Weekday Daily
    T=6.65*X
    T=6.65 * 58
    T=385.70
    T=386 vehicle trips
        with 50% ( }193\textrm{vpd})\mathrm{ entering and 50% ( }193\textrm{vpd})\mathrm{ exiting.
```


Weekday Morning Peak Hour Of Adjacent Street Traffic
$\mathrm{T}=0.51^{*} \mathrm{X}$
$\mathrm{T}=0.51^{*} \quad 58$
$\mathrm{T}=29.58$
$\mathrm{T}=30 \quad$ vehicle trips
with $20 \%$ ( 6 vph$)$ entering and $80 \%$ ( 24 vph$)$ exiting.

Saturday Dally
$\mathrm{T}=6.39^{*} \mathrm{X}$
$\mathrm{T}=6.39^{*} \quad 58$
$\mathrm{T}=370.62$
$\mathrm{T}=370 \quad$ vehicle trips
with $50 \%$ ( 185 vpd ) entering and $50 \%$ ( 185 vpd ) exiting.

```
Saturday Midday Peak Hour Of Generaitor
    \(T=0.52^{*} X\)
    \(\mathrm{T}=0.52^{*} \quad 58\)
    \(\mathrm{T}=30.16\)
    \(\mathrm{T}=30 \quad\) vehicle trips
        with \(50 \%\) ( 15 vph ) entering and \(50 \%\) ( 15 vph ) exiting.
```

- Trip Distribution Calculations


## Journey-to-Work Distribution

| Residence <br> Town <br> Name | Workplace <br> Town <br> Name | All Workers | \% of Totai Rourcled |
| :---: | :---: | :---: | :---: |
| Newbunpor, MA | Newburypor, MA | 3,532 | 39\% |
| Newburyport, MA | Boston, MA | 709 | 8\% |
| Newburyport, MA | Havertill, MA | 235 | 3\% |
| Newburypor, MA | Andover, MA | 234 | 3\% |
| Newburypari, MA | Peaboty, MA | 229 | 3\% |
| Newburypor, MA | Danvers, MA | 192 | 2\% |
| Newburyporf, MA | Salisbury, MA | 188 | 2\% |
| Newburypor, MA | Newbury, MA | 170 | 2\% |
| Nawburyport, MA | Portsmouth, NH | 169 | 2\% |
| Newburyport, MA | Amesbury, MA | 155 | 2\% |
| Newburypor, MA | Lawrence, MA | 136 | 1\% |
| Newburyport, MA | Rowley, MA | 132 | 1\% |
| Newburypor, MA | Medord, MA | 128 | 1\% |
| Newburypor, MA | Beverly, MA | 124 | 1\% |
| Newburyport, MA | lpswlch, MA | 114 | 1\% |
| Newburyport, MA | Seabrook, NH | 104 | 1\% |
| Nawbunyport, MA | Cambricge, MA: | 102 | 1\% |
| Newburypor, MA. | Georgelown, MA | 87 | 1\% |
| Nawburyport, MA | Lynn, MA | 85 | 1\% |
| Newburypot, MA | Wesi Newbur, MA | 85 | 1\% |
| Newburyport, MA | Gloucesier, MA | 82 | 1\% |
| Newburypor, MA | Chelminford, MA | 75 | 1\% |
| Newburyporf MA | Lowell, MA | 75 | 1\% |
| Newburypor, MA | North Andover, MA | 73 | 1\% |
| Newburyport MA | Salem, NH | 67 | 0.5\% |
| Newburyport, MA | Winthrop, MA | 65 | 0.5\% |
| Newburyport, MA | Tewkstury, MA | 64 | 0.5\% |
| Newburyport MA | Quirlinglon, MA | 61 | 0.5\% |
| Newburyport, MA | Topsfield, MA | 58 | 0.5\% |
| Nawburyport, MA | Somerville, MA | 56 | 0.5\% |
| Newburyport, MA | Newton, MA | 54. | 0.5\% |
| Newburypon, MA | Soulhboraugh, MA | 50 | 0.5\% |
| Newisuryport, MA | Framingham, MA | 15 | 0.5\% |
| Newburypor, MA | Lexington, MA | 14 | 0.5\% |
| Newburypord, MA | Hamplon, NH | 43 | 0.5\% |
| Newburyport, MA | Chelsea, MA | 12 | 0.5\% |
| Newburypori, MA | Other | 1,268 | 14\% |
|  | Total | 9,132 | 100\% |

Source: 2006-2010 US Census Journey-fo-Work Data


- Capacity Analyses

1: Newburyport Turnpike (Route 1) \& Low Street/Pond Street

|  | $\stackrel{*}{4}$ | $\rightarrow$ | - | $\%$ | - | + | 4 | $\stackrel{4}{\text { + }}$ | $\stackrel{P}{ }$ |  | $\frac{1}{4}$ | \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * | \% |  | * |  | ${ }^{7}$ | 䗆 |  | \% | 4t |  |
| Volume (vph) | 123 | 112 | 129 | 6 | 125 | 11 | 133 | 183 | 11 | 29 | 354 | 147 |
| Ideal Flow (vphpl). | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (ti) | 11 | 11 | 11 | 15 | 15 | 15 | 12 | 13 | 13 | 12 | 13 | 13 |
| Storage Length ( t ) | 0 |  | 150 | 0 |  | 0 | 165 |  | 0 | 165 |  | 0 |
| Storage Lanes | 0 |  | 1 | 0 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (tt) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Utill. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Fit |  |  | 0.850 |  | 0.989 |  |  | 0.991 |  |  | 0.956 |  |
| Flt Protected |  | 0.974 |  |  | 0.998 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1744 | 1487 | 0 | 1976 | 0 | 1752 | 3499 | 0 | 1752 | 3393 | 0 |
| Flt Permitted |  | 0.974 |  |  | 0.998 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (perm) | 0 | 1744 | 1487 | 0 | 1976 | 0 | 1752 | 3499 | 0 | 1752 | 3393 | 0 |
| Right Turn on Red |  |  | No |  |  | Yes |  |  | No |  |  | No |
| Satd. Flow (RTOR) |  |  |  |  | 3 |  |  |  |  |  |  |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 45 |  |  | 45 |  |
| Link Distance ( f ) |  | 525 |  |  | 133 |  |  | 750 |  |  | 1500 |  |
| Travel Time (s) |  | 11.9 |  |  | 3.0 |  |  | 11.4 |  |  | 22.7 |  |
| Peak Hour Factor | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 |
| Heavy Vehicles (\%) | 4\% | 1\% | 5\% | 0\% | 5\% | 0\% | 3\% | 6\% | 0\% | 3\% | 6\% | 3\% |
| Adj. Flow (vph) | 145 | 132 | 152 | 7 | 147 | 13 | 156 | 215 | 13 | 34 | 416 | 173 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 277 | 152 | 0 | 167 | 0 | 156 | 228 | 0 | 34 | 589 | 0 |
| Enter Blocked Intersection - | No | No | No | No | No | No | No | No | No | No | No | No. |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(tt) |  | 0 |  |  | 0 |  |  | 12 |  |  | 12 |  |
| Link Offset(f) |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width(t) |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| Headway Factor | 1.04 | 1.04 | 1.04 | 0.88 | 0.88 | 0.88 | 1.00 | 0.96 | 0.96 | 1.00 | 0.96 | 0.96 |
| Turning Speed (mph) | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Number of Detectors | 1 | 1 | 1. | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  |
| Detector Template |  |  |  |  |  |  |  |  |  |  |  |  |
| Leading Detector (ti) | 50 | 50 | 50 | 50 | 50 |  | 50 | 50 |  | 50 | 50 |  |
| Traiiing Detector ( f ) | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Detector 1 Position(fi) | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Detector 1 Size(fi) | 50 | 50 | 50 | 50 | 50 |  | 50 | 50 |  | 50 | 50 |  |
| Detector 1 Type | $\mathrm{Cl}+\mathrm{EX}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | CI+Ex | $\mathrm{Cl}+\mathrm{Ex}$ |  | $\mathrm{Cl}+\mathrm{Ex}$ | Cl+Ex |  | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ |  |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Turn Type | Spiit | NA | pt+ov | Split | NA |  | Prot | NA |  | Prot | NA |  |
| Protected Phases | 4 | 4 | 45 | 8 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector Phase | 4 | 4 | 45 | 8 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Inital (s) | 10.0 | 10.0 |  | 10.0 | 10.0 |  | 5.0 | 17.0 |  | 5.0 | 17.0 |  |
| Minimum Split (s) | 16.0 | 16.0 |  | 16.0 | 16.0 |  | 11.0 | 23.0 |  | 11.0 | 23.0 |  |

MDM Transportation Consultants, Inc.
G:IProjects 1848 - Newburyport (Hall)ISynchrol848 EX AM.syn

Analysis Period (min) 15
90th \%ile Actuated Cycle: 109
70th \%ile Actuated Cycle: 96.2
50th \%ile Actuated Cycle: 87.4
30th \%ile Actuated Cycle: 78
10th \%ile Actuated Cycle: 69.4
\# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Splits and Phases: 1: Newburyport Turnpike (Route 1) \& Low Street/Pond Street


Intersection
Int Delay, s/veh 0

| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol, veh/h | 132 | 0 | 0 | 136 | 0 | 0 |
| Conflicing Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Contro | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - None | - | None | - | None |  |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 85 | 85 | 85 | 85 | 85 | 85 |
| Heavy Vehicles, \% | 1 | 0 | 0 | 5 | 0 | 0 |
| Mvmt Flow | 155 | 0 | 0 | 160 | 0 | 0 |


| Major/Minor | Major1 | Maior2 |  |  | Minor1 |  |
| :--- | ---: | :--- | ---: | :--- | ---: | ---: |
| Conflicting Flow All | 0 | 0 | 155 | 0 | 315 | 155 |
| $\quad$ Stage 1 | - | - | - | - | 155 | - |
| Stage 2 | - | - | - | - | 160 | - |
| Critical Hdwy | - | - | 4.1 | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | - | 1438 | - | 682 | 896 |
| $\quad$ Stage 1 | - | - | - | 878 | - |  |
| Stage 2 | - | - | - | - | 874 | - |
| Platoon blocked, \% | - | - | 1438 | - | 682 | 896 |
| Mov Cap-1 Maneevver | - | - | - | - | 682 | - |
| Mov Cap-2 Maneuver | - | - | - | - | 878 | - |
| Stage 1 | - | - | - | - | 874 | - |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 0 | 0 |
| HCM LOS |  |  | A |


| Minor Lane/Major Mivmt | NBL_n1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | - | - | - | 1438 | - |
| HCM Lane V/C Ratio | - | - | - | - | - |
| HCM Control Delay (s) | 0 | - | - | 0 | - |
| HCM Lane LOS | A | - | - | A | - |
| HCM 95th \%tile Q(veh) | - | - | - | 0 | - |



Intersection Summary
Area Type: Other
Cycle Length: 109
Actuated Cycle Length: 89.6
Natural Cycle: 70
Control Type: Actuated-Uncoordinated
Maximum vic Ratio: 0.76
Intersection Signal Delay: 34.4
Intersection LOS: C
Intersection Capacity Utilization 57.5\%
ICU Level of Service B

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| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Vol, veh/h | 19 | 135 | 3 | 6 | 134 | 1 | 1 | 0 | 1 | 0 | 0 | 12 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | - |  | - |  |  |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 |
| Heavy Vehicles, \% | 0 | 1 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Murnt Flow | 22 | 159 | 4 | 7 | 158 | 1 | 1 | 0 | 1 | 0 | 0 | 14 |


| Major/Minor | Major1 |  |  | ajor2 |  |  | Minor1 |  |  | Minor2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conficting Flow All | 159 | 0 | 0 | 162 | 0 | 0 | 384 | 378 | 161 | 378 | 379 | 158 |
| Stage 1 | - | - | - | - | - | - | 205 | 205 | - | 172 | 172 | - |
| Stage 2 | - | - | - | - | - | - | 179 | 173 | - | 206 | 207 | - |
| Critical Hdwy | 4.1 | - | - | 4.1 | - | - | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Follow-up Hdwy | 2.2 | - | - | 2.2 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1433 | - | - | 1429 | - | - | 578 | 557 | 889 | 583 | 556 | 893 |
| Stage 1 | - | - | - | - | - | - | 802 | 736 | - | 835 | 760 | - |
| Stage 2 | - | - | - | - | - | - | 827 | 760 | - | 801 | 734 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 1433 | - | - | 1429 | - | - | 559 | 545 | 889 | 572 | 544 | 893 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 559 | 545 | - | 572 | 544 | - |
| Stage 1 | - | - | - | - | - | - | 788 | 723 | - | 821 | 756 | - |
| Stage 2 | - | - | - | - | - | - | 810 | 756 | - | 786 | 722 | - |


| Approach | EB | WB | NB | SB |
| :--- | :--- | :---: | ---: | :---: |
| HCM Control Delay, s | 0.9 | 0.3 | 10.3 | 9.1 |
| HCM LOS |  | $B$ | A |  |


| Minor Lane/Major Mvint | NBLn1 | EBL | CBT | EBR | WBL | WBT | WBR SBLn1 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 686 | 1433 | - | -1429 | - | -893 |  |  |
| HCM Lane V/C Ratio | 0.003 | 0.016 | - | -0.005 | - | -0.016 |  |  |
| HCM Control Delay (s) | 10.3 | 7.6 | 0 | - | 7.5 | 0 | - | 9.1 |
| HCM Lane LOS | 8 | A | A | - | A | A | - | A |
| HCM 95th \%tile Q(veh) | 0 | 0 | - | - | 0 | - | - | 0 |

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1: Newburyport Turnpike (Route 1) \& Low Street/Pond Street
Analysis Period (min) 15
90th \%ile Actuated Cycle: 109
70th \%ile Actuated Cycle: 100.1
50th \%ile Actuated Cycle: 90.4
30th \%ile Actuated Cycle: 82.2
10th \%ile Actuated Cycle: 71.7
\# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Splits and Phases: 1: Newburyport Turnpike (Route 1) \& Low Street/Pond Street


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| Intersection |  |
| :--- | :--- |
| Int Delay, s/veh | 0.2 |


| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol, veh/h | 137 | 2 | 0 | 141 | 6 | 0 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - None | - | None |  |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 85 | 85 | 85 | 85 | 85 | 85 |
| Heavy Vehicles, \% | 1 | 0 | 0 | 5 | 0 | 0 |
| Mvint Flow | 161 | 2 | 0 | 166 | 7 | 0 |


| Major/Minor | Major1 | Major2 |  |  |  |  |
| :--- | ---: | :--- | ---: | :--- | ---: | ---: |
| Conflicting Flow All | 0 | 0 | 164 | 0 | 328 | 162 |
| Stage 1 | - | - | - | - | 162 | - |
| Stage 2 | - | - | - | - | 166 | - |
| Critical Hdwy | - | - | 4.1 | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | - | 1427 | - | 671 | 888 |
| Stage 1 | - | - | - | - | 872 | - |
| Stage 2 | - | - | - | - | 868 | - |
| Platoon blocked, \% | - | - | 1427 | - | 671 | 888 |
| Mov Cap-1 Maneuver | - | - | - | 671 | - |  |
| Mov Cap-2 Maneuver | - | - | - | - | 872 | - |
| Stage 1 | - | - | - | - | - |  |
| Stage 2 | - | - | - | - | 868 | - |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 0 | 10.4 |
| HCM LOS |  | $B$ |  |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 671 | - | -1427 | - |  |
| HCM Lane V/C Ratio | 0.011 | - | - | - | - |
| HCM Control Delay (s) | 10.4 | - | - | 0 | - |
| HCM Lane LOS | B | - | - | A | - |
| HCM 95th \%tilie Q(veh) | 0 | - | - | 0 | - |

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|  | \% |  | V | $\square$ | - |  | 4 | $\stackrel{4}{4}$ | $\stackrel{7}{ }$ |  | 1 | 8 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 | \% |  | \$ |  | ${ }^{9}$ | 性 |  | ${ }^{5}$ | 中 ${ }_{\text {c }}$ |  |
| Volume (vph) | 186 | 124 | 127 | 16 | 127 | 19 | 165 | 398 | 13 | 53 | 357 | 124 |
| Ideal Flow (vphpi) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (t) | 11 | 11 | 11 | 15 | 15 | 15 | 12 | 13 | 13 | 12 | 13 | 13 |
| Storage Length (t) | 0 |  | 150 | 0 |  | 0 | 165 |  | 0 | 165 |  | 0 |
| Storage Lanes | 0 |  | 1 | 0 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Utill. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Fit |  |  | 0.850 |  | 0.984 |  |  | 0.995 |  |  | 0.961 |  |
| Fit Protected |  | 0.971 |  |  | 0.995 |  | 0.550 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1759 | 1561 | 0 | 2003 | 0 | 1787 | 3676 | 0 | 1805 | 3513 | 0 |
| Flt Permitted |  | 0.971 |  |  | 0.995 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Fow (perm) | 0 | 1759 | 1561 | 0 | 2003 | 0 | 1787 | 3676 | 0 | 1805 | 3513 | 0 |
| Right Turn on Red |  |  | No |  |  | Yes |  |  | No |  |  | No |
| Satd. Flow (RTOR) |  |  |  |  | 5 |  |  |  |  |  |  |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 45 |  |  | 45 |  |
| Link Distance (f) |  | 525 |  |  | 133 |  |  | 750 |  |  | 1500 |  |
| Travel Time (s) |  | 11.9 |  |  | 3.0 |  |  | 11.4 |  |  | 22.7 |  |
| Peak Hour Facior | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Heavy Vehicles (\%) | 1\% | 2\% | 0\% | 6\% | 2\% | 0\% | 1\% | 1\% | 0\% | 0\% | 1\% | 5\% |
| Adj. Flow (vph) | 198 | 132 | 135 | 17 | 135 | 20 | 176 | 423 | 14 | 56 | 380 | 132 |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 330 | 135 | 0 | 172 | 0 | 176 | 437 | 0 | 56 | 512 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(ft) |  | 0 |  |  | 0 |  |  | 12 |  |  | 12 |  |
| Link Offset(fi) |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width(ft) |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Tum Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| Headway Factor | 1.04 | 1.04 | 1.04 | 0.88 | 0.88 | 0.88 | 1.00 | 0.96 | 0.96 | 1.00 | 0.96 | 0.96 |
| Turning Speed (mph) | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Number of Detectors | 1 | 1 | 1 | 1 | 1 |  | 1 | 1 |  | 1 | 1 |  |
| Detector Template |  |  |  |  |  |  |  |  |  |  |  |  |
| Leading Detector (ft) | 50 | 50 | 50 | 50 | 50 |  | 50 | 50 |  | 50 | 50 |  |
| Trailing Detector ( t ) | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Detector 1 Position(ft) | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Detector 1 Size(ft) | 50 | 50 | 50 | 50 | 50 |  | 50 | 50 |  | 50 | 50 |  |
| Detector 1 Type | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ |  | CltEx | $\mathrm{Cl}+\mathrm{Ex}$ |  | Cl+Ex | CltEx |  |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Turn Type | Split | NA | pt + ov | Split | NA |  | Prot | NA |  | Prot | NA |  |
| Protected Phases | 4 | 4 | 45 | 8 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector Phase | 4 | 4 | 45 | 8 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 10.0 |  | 10.0 | 10.0 |  | 5.0 | 17.0 |  | 5.0 | 17.0 |  |
| Minimum Spitit (s) | 16.0 | 16.0 |  | 16.0 | 16.0 |  | 11.0 | 23.0 |  | 11.0 | 23.0 |  |

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Analysis Period (min) 15
90th \%ile Actuated Cycle: 104.7
70th \%ile Actuated Cycle: 93.6
50th \%ile Actuated Cycle: 84.1
30th \%ile Actuated Cycle: 78.5
10th \%ile Actuated Cycle: 75.7
\# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Splits and Phases: 1: Newburyport Turnpike (Route 1) \& Low StreetPond Street


3: Hillside Avenue \& Pond Street

| Intersection |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.1 |  |  |  |  |  |  |
|  |  | EBT | EBR | WBL | WBT | NBL | NBR |
| Movement | 158 | 3 | 2 | 134 | 2 | 1 |  |
| Vol, veh/h | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Conficting Peds, \#hr | Free | Free | Free | Free | Stop | Stop |  |
| Sign Control | - None | - None | - | None |  |  |  |
| RTChannelized | - | - | - | - | 0 | - |  |
| Storage Length | 0 | - | - | 0 | 0 | - |  |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |  |
| Grade, \% | 94 | 94 | 94 | 94 | 94 | 94 |  |
| Peak Hour Factor | 2 | 0 | 0 | 2 | 0 | 0 |  |
| Heavy Vehicles, \% | 168 | 3 | 2 | 143 | 2 | 1 |  |


|  | Major1 | Major2 |  |  | Minor1 |  |
| :--- | ---: | :--- | ---: | :--- | ---: | ---: |
| Major/Minor | 0 | 0 | 171 | 0 | 317 | 170 |
| Conflicting Flow All | - | - | - | - | 170 | - |
| Stage 1 | - | - | - | - | 147 | - |
| Stage 2 | - | - | 4.1 | - | 6.4 | 6.2 |
| Critical Hdwy | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | 2.2 | - | 3.5 | 3.3 |
| Follow-up Hdwy | - | - | 1418 | - | 680 | 879 |
| Pot Cap-1 Maneuver | - | - | - | - | 865 | - |
| Stage 1 | - | - | - | - | 885 | - |
| Stage 2 | - | - | 1418 | - | 679 | 879 |
| Platoon blocked, \% | - | - | - | - | 679 | - |
| Mov Cap-1 Maneuver | - | - | - | - | 865 | - |
| Mov Cap-2 Maneuver | - | - | - | - | 883 | - |
| Stage 1 |  |  |  |  |  |  |
| Stage 2 | EB |  | WB |  | NB |  |
|  | 0 | 0.1 | 9.9 |  |  |  |
| Approach |  |  |  | A |  |  |


| Minor Lane/Major Mvint | NBLn1 | EBT | EBR | WBI | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 735 | - | -1418 | - |  |
| HCM Lane V/C Ratio | 0.004 | - | -0.002 | - |  |
| HCM Control Delay (s) | 9.9 | - | - | 7.5 | 0 |
| HCM Lane LOS | A | - | - | A | A |
| HCM 95th \%tile Q(veh) | 0 | - | - | 0 | - |

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Intersection
int Deiay, slveh 1.5

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol, veh/h | 27 | 165 | 4 | 2 | 139 | 1 | 12 | 1 | 0 | 1 | 18 |  |  |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |  |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | - | - |
| Storage Length | - | - | - | - | - | - | - | - | - | - | - |  |  |
| Veh in Median Storage, \# | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 | 94 |  |
| Heavy Vehicles, \% | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Murnt Flow | 29 | 176 | 4 | 2 | 148 | 1 | 13 | 1 | 0 | 1 | 1 | 19 |  |


| Major/Minor | Major 1 |  | Major2 |  |  |  | Minor 1 |  |  | Minor2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 149 | 0 | 0 | 180 | 0 | 0 | 398 | 388 | 178 | 389 | 390 | 148 |
| Stage 1 | - | - | - | - | - | - | 235 | 235 | - | 153 | 153 | - |
| Stage 2 | - | - | - | - | - | - | 163 | 153 | - | 236 | 237 | - |
| Critical Hdwy | 4.1 | - | - | 4.1 | - | - | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | . |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Follow-up Hdwy | 2.2 | - | - | 2.2 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 1445 | - | - | 1408 | - | - | 566 | 550 | 870 | 574 | 548 | 904 |
| Stage 1 | - | - | - | - | - | - | 773 | 714 | - | 854 | 775 | - |
| Stage 2 | - | - | - | - | - | - | 844 | 775 | - | 772 | 713 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 1445 | - | - | 1408 | - | - | 543 | 537 | 870 | 563 | 535 | 904 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 543 | 537 | - | 563 | 535 | - |
| Stage 1 | - | - | - | - | - | - | 756 | 698 | - | 835 | 773 | - |
| Stage 2 | - | - | - | - | - | - | 823 | 773 | - | 754 | 697 | - |
| Approach | EB |  |  | WB |  |  | NB |  |  | SB |  |  |
| HCM Control Delay, s | 1 |  |  | 0.1 |  |  | 11.8 |  |  | 9.3 |  |  |
| HCMLOS |  |  |  |  |  |  | B |  |  | A |  |  |


| Minor Lane/Major Mvmt | NBL_n1 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 543 | 1445 | - | -1408 | - | -849 |  |  |
| HCM Lane V/C Ratio | 0.025 | 0.02 | - | -0.002 | - | -0.025 |  |  |
| HCM Control Delay (s) | 11.8 | 7.5 | 0 | - | 7.6 | 0 | - | 9.3 |
| HCM Lane LOS | B | A | A | - | A | A | - | A |
| HCM 95th \%file Q(veh) | 0.1 | 0.1 | - | - | 0 | - | - | 0.1 |

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| Lane Group | ¢ EBL | $\overrightarrow{E B T}$ | EBR | WBL | - WBT | WBR | 4 | NBT | $\stackrel{F}{\text { NBR }}$ | P SBL | $\frac{1}{7}$ | a SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | * | F |  | ${ }_{*}$ |  | ${ }^{7}$ | 虫 |  | ${ }^{7}$ | 个t |  |
| Volume (vph) | 193 | 141 | 132 | 17 | 133 | 21 | 177 | 415 | 14 | 61 | 370 | 128 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Widh (ft) | 11 | 11 | 11 | 15 | 15 | 15 | 12 | 13 | 13 | 12 | 13 | 13 |
| Storage Length (ft) | 0 |  | 150 | 0 |  | 0 | 165 |  | 0 | 165 |  | 0 |
| Storage Lanes | 0 |  | 1 | 0 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Fit |  |  | 0.850 |  | 0.984 |  |  | 0.995 |  |  | 0.962 |  |
| FII Protected |  | 0.972 |  |  | 0.995 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1760 | 1561 | 0 | 2003 | 0 | 1787 | 3676 | 0 | 1805 | 3517 | 0 |
| Fit Permitted |  | 0.972 |  |  | 0.995 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (perm) | 0 | 1760 | 1561 | 0 | 2003 | 0 | 1787 | 3676 | 0 | 1805 | 3517 | 0 |
| Right Turn on Red |  |  | No |  |  | Yes |  |  | No |  |  | No |
| Satd. Flow (RTOR) |  |  |  |  | 6 |  |  |  |  |  |  |  |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 45 |  |  | 45 |  |
| Link Distance (ft) |  | 525 |  |  | 133 |  |  | 750 |  |  | 1500 |  |
| Travel Time (s) |  | 11.9 |  |  | 3.0 |  |  | 11.4 |  |  | 22.7 |  |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Heavy Vehicles (\%) | 1\% | 2\% | 0\% | 6\% | 2\% | 0\% | 1\% | 1\% | 0\% | 0\% | 1\% | 5\% |
| Adj. Flow (vph) | 205 | 150 | 140 | 18 | 141 | 22 | 188 | 441 | 15 | 65 | 394 | 136 |
| Shared Lane Trafic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 355 | 140 | 0 | 181 | 0 | 188 | 456 |  | 65 | 530 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(ft) |  | 0 |  |  | 0 |  |  | 12 |  |  | 12 |  |
| Link Offset(fit) |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width( ft ) |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  |  |  |  |  |  |  |  |  |
| Headway Factor | 1.04 | 1.04 | 1.04 | 0.88 | 0.88 | 0.88 | 1.00 | 0.96 | 0.96 | 1.00 | 0.96 | 0.96 |
| Turning Speed (mph) | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Number of Detectors | 1 | 1 | 1 | 1 | 1 |  | 1 | 1 |  | 1 | - 1 |  |
| Detector Template |  |  |  |  |  |  |  |  |  |  |  |  |
| Leading Detector ( t ) | 50 | 50 | 50 | 50 | 50 |  | 50 | 50 |  | 50 | 50 |  |
| Trailing Detector (fi) | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Detector 1 Position(ft) | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Detector 1 Size(ft) | 50 | 50 | 50 | 50 | 50 |  | 50 | 50 |  | 50 | 50 |  |
| Detector 1 Type | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ |  | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ |  | $\mathrm{Cl}+\mathrm{Ex}$ | Cl+Ex |  |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Turn Type | Split | NA | pt+ov | Split | NA |  | Prot | NA |  | Prot | NA |  |
| Protected Phasés | 4 | 4 | 45 | 8 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector Phase | 4 | 4 | 45 | 8 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial ( $s$ ) | 10.0 | 10.0 |  | 10.0 | 10.0 |  | 5.0 | 17.0 |  | 5.0 | 17.0 |  |
| Minimum Split (s) | 16.0 | 16.0 |  | 16.0 | 16.0 |  | 11.0 | 23.0 |  | 11.0 | 23.0 |  |

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Analysis Period (min) 15
90th \%ile Actuated Cycle: 105.5
70th \%ile Actuated Cycle: 96
50th \%ile Actuated Cycle: 87.3
30th \%ile Actuated Cycle: 79.1
10th \%ile Actuated Cycle: 76.1
\# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Splits and Phases: 1: Newburyport Turnpike (Route 1) \& Low Street/Pond Street


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Intersection

Int Delay, s/veh 0.2

| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Vol, veh/h | 163 | 10 | 2 | 141 | 4 | 2 |
| Conflicting Peds, \#hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 94 | 94 | 94 | 94 | 94 | 94 |
| Heavy Vehicles, \% | 2 | 0 | 0 | 2 | 0 | 0 |
| Mvmt Flow | 173 | 11 | 2 | 150 | 4 | 2 |


| Major/Minor | Major1 | Major2 |  |  |  | Minor1 |
| :--- | ---: | :--- | ---: | :--- | ---: | ---: |
| Conflicting Flow All | 0 | 0 | 184 | 0 | 333 | 179 |
| Stage 1 | - | - | - | - | 179 | - |
| Stage 2 | - | - | - | - | 154 | - |
| Critical Hdwy | - | - | 4.1 | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | - | - | 2.2 | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | - | - | 1403 | - | 666 | 869 |
| Stage 1 | - | - | - | - | 857 | - |
| Stage 2 | - | - | - | - | 879 | - |
| Platoon blocked, \% | - | - | 1403 | - |  | 665 |
| Mov Cap-1 Maneuver | - | - | - | 869 |  |  |
| Mov Cap-2 Maneuver | - | - | - | - | 665 | - |
| Stage 1 | - | - | - | - | 857 | - |
| Stage 2 | - | - | - | - | 877 | - |


| Approach | EB | WB | NB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, S | 0 | 0.1 | 10 |
| HCM LOS |  | $B$ |  |


| Minor Lane/Major Mvmt | NBLn1 | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 721 | - | -1403 | - |  |
| HCM Lane V/C Ratio | 0.009 | - | -0.002 | - |  |
| HCM Control Delay (s) | 10 | - | - | 7.6 | 0 |
| HCM Lane LOS | B | - | - | A | A |
| HCM 95th \% file Q(veh) | 0 | - | - | 0 | - |

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## TRAFFIC IMMPACT AND ACCESS STUDY

## PROPOSED RESIDENTIAL DEVELOPMENT

## 4 Hillside Avenue

Newburyport, Massachusetts

## Prepared for:

Hall and Moskow Corporation

November 2015


[^0]:    ${ }^{1}$ A policy on Geometric Design of Highways and Streets, American Association of State Highway and Transportation Officials (AASHTO), 2011.

[^1]:    ${ }^{2}$ Memorandum, Re: Proposed Residential Development, Route 1 (Netoburyport Turnpike) - Newburyport, MA; by MDM Transportation Consultants, Inc (MDM); December 17, 2014.

[^2]:    Date: November 2015
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[^3]:    1Volume-to-capacity ratio
    ${ }^{2}$ Average control delay per vehicle (in seconds)
    ${ }^{3}$ Level of service
    ${ }^{4}$ Not Applicable

[^4]:    MDM Transportation Consultants, Inc.

