PROJECT NARRATIVE AND STORMWATER ANALYSIS 18 Boyd Drive

Newburyport, MA May 22, 2017 Rev. Aug. 8, 2017

Submitted to:

Newburyport Planning Board & Conservation Commission City Hall 60 Pleasant Street Newburyport, MA 01950

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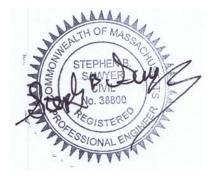


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1. Site Plan Review

Checklist for Stormwater Report



Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program Checklist for Stormwater Report

A. Introduction

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key.



A Stormwater Report must be submitted with the Notice of Intent permit application to document compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for the Stormwater Report (which should provide more substantive and detailed information) but is offered here as a tool to help the applicant organize their Stormwater Management documentation for their Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist, the Stormwater Report must contain the engineering computations and supporting information set forth in Volume 3 of the Massachusetts Stormwater Handbook. The Stormwater Report must be prepared and certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals.¹ This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report
- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 8²
- Operation and Maintenance Plan required by Standard 9

In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification must be submitted with the Stormwater Report.

¹ The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

² For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.



B. Stormwater Checklist and Certification

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

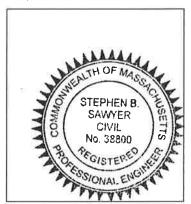
Note: Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

Registered Professional Engineer's Certification

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Longterm Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature



ten 1 MAL 22,2017

Checklist

Project Type: Is the application for new development, redevelopment, or a mix of new and redevelopment?

New development

Redevelopment

Mix of New Development and Redevelopment



LID Measures: Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project:

\bowtie	No disturbance to any Wetland Resource Areas
	Site Design Practices (e.g. clustered development, reduced frontage setbacks)
	Reduced Impervious Area (Redevelopment Only)
	Minimizing disturbance to existing trees and shrubs
	LID Site Design Credit Requested:
	Credit 1
	Credit 2
	Credit 3
	Use of "country drainage" versus curb and gutter conveyance and pipe
\boxtimes	Bioretention Cells (includes Rain Gardens)
\boxtimes	Constructed Stormwater Wetlands (includes Gravel Wetlands designs)
	Treebox Filter
	Water Quality Swale
	Grass Channel
	Green Roof
	Other (describe):
640	ndard 1. No. New Untrooted Discharges

Standard 1: No New Untreated Discharges

No new untreated discharges

- \boxtimes Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth
- Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.



Standard 2: Peak Rate Attenuation

- Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding.
- Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm.

Calculations provided to show that post-development peak discharge rates do not exceed predevelopment rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24hour storm.

Standard 3: Recharge

\bowtie	Soil	Anal	ysis	provided.
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- Required Recharge Volume calculation provided.
- Required Recharge volume reduced through use of the LID site Design Credits.
- Sizing the infiltration, BMPs is based on the following method: Check the method used.

\boxtimes	Static
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Dynamic Field¹

Runoff from all impervious areas at the site discharging to the infiltration BMP.

Simple Dynamic

Runoff from all impervious areas at the site is *not* discharging to the infiltration BMP and calculations are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume.

	Recharge BMPs ha	ave been sized to	infiltrate the	Required Re	echarge Volume.
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- Recharge BMPs have been sized to infiltrate the Required Recharge Volume *only* to the maximum extent practicable for the following reason:
 - Site is comprised solely of C and D soils and/or bedrock at the land surface
 - M.G.L. c. 21E sites pursuant to 310 CMR 40.0000
 - Solid Waste Landfill pursuant to 310 CMR 19.000
 - Project is otherwise subject to Stormwater Management Standards only to the maximum extent practicable.
- \boxtimes Calculations showing that the infiltration BMPs will drain in 72 hours are provided.
- Property includes a M.G.L. c. 21E site or a solid waste landfill and a mounding analysis is included.

¹ 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



Standard 3: Recharge (continued)

- The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.
- Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.

Standard 4: Water Quality

The Long-Term Pollution Prevention Plan typically includes the following:

- Good housekeeping practices;
- Provisions for storing materials and waste products inside or under cover;
- Vehicle washing controls;
- Requirements for routine inspections and maintenance of stormwater BMPs;
- Spill prevention and response plans;
- Provisions for maintenance of lawns, gardens, and other landscaped areas;
- Requirements for storage and use of fertilizers, herbicides, and pesticides;
- Pet waste management provisions;
- Provisions for operation and management of septic systems;
- Provisions for solid waste management;
- Snow disposal and plowing plans relative to Wetland Resource Areas;
- Winter Road Salt and/or Sand Use and Storage restrictions;
- Street sweeping schedules;
- Provisions for prevention of illicit discharges to the stormwater management system;
- Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL;
- Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan;
- List of Emergency contacts for implementing Long-Term Pollution Prevention Plan.
- A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent.
- Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:
 - is within the Zone II or Interim Wellhead Protection Area
 - is near or to other critical areas
 - is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)
 - involves runoff from land uses with higher potential pollutant loads.
- The Required Water Quality Volume is reduced through use of the LID site Design Credits.
- Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if applicable, the 44% TSS removal pretreatment requirement, are provided.



Checklist	(continued)
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Standard 4: Water Quality (continued)

- The BMP is sized (and calculations provided) based on:
 - The ½" or 1" Water Quality Volume or
 - The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume.
- The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs.
- A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided.

Standard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs)

- The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report.
- The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted **prior to** the discharge of stormwater to the post-construction stormwater BMPs.
- The NPDES Multi-Sector General Permit does *not* cover the land use.
- LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan.
- All exposure has been eliminated.
- All exposure has *not* been eliminated and all BMPs selected are on MassDEP LUHPPL list.
- The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent.

Standard 6: Critical Areas

- The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.
- Critical areas and BMPs are identified in the Stormwater Report.



Standard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum extent practicable

The project is subject to the Stormwater Management Standards only to the maximum Extent Practicable as a:

 Limited Project Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family developrovided there is no discharge that may potentially affect a critical area. Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development. 	
provided there is no discharge that may potentially affect a critical area.	
 with a discharge to a critical area Marina and/or boatyard provided the hull painting, service and maintenance areas are p from exposure to rain, snow, snow melt and runoff 	pment
Bike Path and/or Foot Path	
Redevelopment Project	
Redevelopment portion of mix of new and redevelopment.	
 Certain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) explanation of why these standards are not met is contained in the Stormwater Report. The preject involves redevelopment and a description of all measures that have been taken 	

☐ The project involves redevelopment and a description of all measures that have been taken to improve existing conditions is provided in the Stormwater Report. The redevelopment checklist found in Volume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that the proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment and structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) improves existing conditions.

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative;
- Construction Period Operation and Maintenance Plan;
- Names of Persons or Entity Responsible for Plan Compliance;
- Construction Period Pollution Prevention Measures;
- Erosion and Sedimentation Control Plan Drawings;
- Detail drawings and specifications for erosion control BMPs, including sizing calculations;
- Vegetation Planning;
- Site Development Plan;
- Construction Sequencing Plan;
- Sequencing of Erosion and Sedimentation Controls;
- Operation and Maintenance of Erosion and Sedimentation Controls;
- Inspection Schedule;
- Maintenance Schedule;
- Inspection and Maintenance Log Form.

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control (continued)

The project is highly complex and information is included in the Stormwater Report that explains why
it is not possible to submit the Construction Period Pollution Prevention and Erosion and
Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and
Erosion and Sedimentation Control has <i>not</i> been included in the Stormwater Report but will be
submitted <i>before</i> land disturbance begins.

- The project is *not* covered by a NPDES Construction General Permit.
- The project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the Stormwater Report.
- The project is covered by a NPDES Construction General Permit but no SWPPP been submitted. The SWPPP will be submitted BEFORE land disturbance begins.

Standard 9: Operation and Maintenance Plan

\boxtimes	The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and
	includes the following information:

- Name of the stormwater management system owners;
- Party responsible for operation and maintenance;
- Schedule for implementation of routine and non-routine maintenance tasks;
- Plan showing the location of all stormwater BMPs maintenance access areas;
- Description and delineation of public safety features;
- Estimated operation and maintenance budget; and
- Operation and Maintenance Log Form.
- The responsible party is **not** the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions:
 - A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs;
 - A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions.

Standard 10: Prohibition of Illicit Discharges

- The Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges;
- An Illicit Discharge Compliance Statement is attached;
- NO Illicit Discharge Compliance Statement is attached but will be submitted *prior to* the discharge of any stormwater to post-construction BMPs.

2. Project Overview

Introduction

The project proposes a Definitive Plan pursuant to the approval of the Open Space Residential Design (OSRD) Special Permit which authorized a OSRD consisting of thirty-eight (38) lots on approximately thirty-six acres, (36.84 +/- acres) (the "Property"). The Property is located off of Boyd Drive and Brown Avenue and is currently operated as a golf course. The Brown Avenue lot is currently a single-family home. The Property lies within the R-1 and R-2 zoning district as well as the Water Resource Protection Overlay District ("WRPD") and is a Zone II designation for that purpose. The portion of the Property on which homes and roadways would be constructed includes 13.36 +/- acres and the remaining 22.816 +/- acres will be preserved for conservation and recreational uses – open to the public but owned and maintained by the home-owner's association

Existing Conditions

The existing site is comprised of City of Newburyport Assessors tax map, Map 110 Parcel 20 for 18 Boyd Drive and Map 111 Parcel 13 for the 5 Brown Avenue parcel. The majority of the existing land proposed for development was originally used as a gravel pit creating a low flat area with relatively steep slopes surrounding the lot area. It is currently utilized as a 9 hole golf course. After advancing 13 deep hole tests and 8 test holes for the hydrological study it has been determined that there is a loam surface with underlying soils consisting of well drained sands and gravels.

This low area is classified as Isolated Land Subject to Flooding. Additionally, one of the low areas has been delineated is isolated wetland under the local Newburyport Wetland Regulations. The Conservation Commission issued an Order of Resource Area Delineation(ORAD) confirming the isolated wetland area and a peak ILSF flood elevation of 55.60 based upon 7 inches of rain per the MA DEP regulations. The drainage system from Boyd Drive currently discharges untreated stormwater onto the property.

Project Description

The proposed redevelopment will consist of 38 new homes and approximately 3,100 linear feet of new roads. Consistent with section XIV of the Newburyport Zoning Ordinance ("OSRD") the proposed development maximizes the amount of preserved open space and protects local resources while not impacting the number of units permitted by a conventional plan. The Proposed Development has received an OSRD Special Permit and is therefore in conformance with the OSRD zoning requirements.

Specifically, the land within the project site resides within the R1 zoning district with lot areas of 20,000 square feet and minimum lot frontage of 125 feet. As provided in the OSRD approval the development provides 10,000 square foot minimum lots with at least 50% minimum setbacks as is required in the underlying district – All front yard setbacks are a minimum of 15 feet and side yards are a minimum of 10 feet as required.

Further, as required in the OSRD, at least 60% of the total lot area is Open Space and will include a restriction assuring the open space in perpetuity. The Open Space is specifically designed to be maintained for wildlife habitat, conservation, outdoor education, passive and active recreation. The Open Space is programed as shown on the site plans and includes the requisite long term operation and maintenance plan.

The project proposes to improve the Boyd Drive drainage outfall to current DEP treatment standards for a Zone II watershed. This will be accomplished by constructing a new Constructed Stormwater Wetland. Five biorention areas or rain gardens will provide water quality treatment for the new development. The 22.8 Acres of open space including the expanded and improved Isolated Wetland and a new expansive pollinator meadow. This will provide new wildlife habitat and new diverse natural plant species replacing much of the current golf fairways and greens. This change in land use from the current golf course fairway and greens to a naturally vegetated open space area provides a substantial benefit in regards to the Zone II watershed quality.

Utilities

The new building is proposed to be serviced with new water, sewer, gas services, electric and communications conduits from Boyd Drive and Brown Avenue. Public and private utilities are all available along the property frontage. The project will replace the existing sewerage pump station at the bottom of Boyd Drive.

3. Stormwater Management

Introduction

The project is located within a Zone II wellhead protection area. This will require added water quality treatment measures including a 1" water quality volume for all paved areas. Currently the Boyd Drive drainage system discharges onto the property and does not meet the current DEP design standards. Included in this project, the stormwater treatment for Boyd Drive will be brought up to Current DEP treatment standards. The project proposes for the Boyd Drive stormwater flow be directed to a new Constructed Stormwater Wetland designed in accordance with the Massachusetts Stormwater Handbook published by the Massachusetts Department of Environmental Protection (DEP). The new subdivision will utilize Low Impact Design techniques designed in accordance with the Massachusetts Stormwater Handbook with the development divided up into five smaller drainage areas where the stormwater will be directed to Bioretention areas for final treatment prior to discharging to the improved isolated wetland area. These systems will be landscaped and visually appealing. These systems will be maintained by the new homeowners association with no maintenance responsibility to the Newburyport Department of Public Services. Pre-treatment is provided with deep sump catch basins followed by hydrodynamic separation prior to the stormwater flowing into the Bioretention areas. Additionally, a detailed study was completed during the OSRD permit process to determine the impact of the new subdivision on the Newburyport Well located over 700' from the proposed development.

Consistency with the DEP Stormwater Management Policy

The project is a new development and therefore must meet all ten of the Stormwater Management Standards. Each of the standards of the DEP Stormwater Handbook and how the project meets or exceeds them is discussed below.

Standard 1 – Untreated Stormwater

Standard 1 states that "No new stormwater conveyances (e.g. outfalls) will discharge untreated stormwater directly to or cause erosion in wetlands or waters of the Commonwealth."

The proposed drainage system does not include new conveyances that discharge directly without pretreatment. Several BMP's are proposed to treat stormwater and to prevent any erosion to the surrounding Resource Areas. Since no new conveyances will directly discharge untreated stormwater, the project meets this standard. The project proposes to bring the off-site Boyd Drive drainage system into compliance with DEP Stormwater Standards

Standard 2 – Post Development Peak Discharge Rates

Standard 2 states that "Stormwater management systems shall be designed so that post-development peak discharge rates do not exceed pre-development peak discharge rates."

The site was analyzed under both the existing and proposed conditions to compare the pre and post development peak discharge rates at two design points leaving the property. The analysis divides the site into several subcatchments that discharge at the borders of the site. The discharge points were analyzed to ensure that there is no impact on abutting properties as a result of the project. Most of the runoff remains on the property area designated as Isolated Land Subject to Flooding (ILSF). This area is analyzed to confirm the proposed ILSF elevation on the property with the new development. A detailed description of both the existing and proposed conditions hydrology is described below. A copy of the HydroCAD printouts for the ILSF calculation, existing and proposed conditions is included in Appendix B.

Existing Conditions Hydrology

The majority of the site runoff is directed to a large Isolated Land Subject to Flooding area on the property. There are two small portions of the property that flow off site, one area is directed to Brown Avenue and the other onto Boyd Drive. These design points have been analyzed for Standard 2 compliance. The main drainage area does not require compliance to Standard 2 where no runoff leaves the property. Alternately this drainage area had been evaluated as Isolated Land Subject to Flooding to determine the new 100 year flood elevation and confirm it has no negative impact to the proposed development. This analysis is provided below under Standard 2.

Proposed Conditions Hydrology

Proposed Subcatchment PR 2: This subcatchment located northern side of the property, it consists of a new access road and landscaped areas. The new catch basins here divert stormwater runoff back to the ILSF area on the property reducing the flow off property at this location.

Proposed Subcatchment PR 3: This subcatchment located on the eastern side directing water onto Boyd Drive consists new access drive, 3 new homes, driveways and new landscaped lawn areas. This area eventually flows back onto the property and into the ILSF area.

Summary

The project does not increase flow rate for 2, 10 & 100 year design storm off the property. The calculations are based upon the rainfall rates in the City of Newburyport Drainage regulations. A summary of the pre and post development discharge rates is shown on Table 1 below.

Table 2: Existing and Proposed Peak Discharge Rate Comparison at Design Points

	2 Year Storm - (3.10 in)		10 Year Storm - (4.70 in)		100 Year Storm - (8.30 in)	
Design Point	Existing (cfs)	Proposed (cfs)	Existing (cfs)	Proposed (cfs)	Existing (cfs)	Proposed (cfs)
2 Brown Ave.	0.17	0.03	0.26	0.05	0.71	0.15
3 Boyd Dr	2.07	1.16	3.16	1.77	5.80	4.24

DESIGN POINT 2 & 3 – To Brown Ave., & Boyd Drive Offsite

Since the proposed project is designed so that post-development peak discharge rates do not exceed pre-development peak discharge rates, the project is in compliance with Standard 2.

Design Point 1 – Isolated Land Subject to Flooding.

This low area is classified as Isolated Land Subject to Flooding meaning the water ponds at the bottom low areas during large storm events. Additionally, one of the low areas has been delineated is isolated wetland under the local Newburyport Wetland Regulations. The Conservation Commission issued an Order of Resource Area Delineation(ORAD) confirming a the isolated wetland area and a peak ILSF flood elevation of 55.60 based upon 7 inches of rain per the MA DEP regulations. The project proposes to improve the Isolated Wetland area by expanding the area and excavating the bottom down to interface with the spring high ground water elevation of 50 as determined by numerous observations taken this April and May in the observation wells installed throughout the property. The ILSF calculations do not take credit for any volume below elevation 52.0 due to estimated seasonal high groundwater elevation as determined by averaging numerous test pits completed within and adjacent to the ILSF area. With the improved Isolated Wetland area and New Constructed Stormwater Wetland, the proposed ILSF flood elevation is lowered to elevation 55.20. This lower elevation accounts for the increased impervious surface with the proposed development and using 8.3 inches of rainfall, the 100 year rainfall amount from the Newburyport Wetland Regulations verses the 7 inch rainfall depth as defined the DEP regulations and used in the existing ORAD for the property. The ILSF elevation based upon using the DEP requirement of 7" rainfall event is lowered to elevation 54.70.

Numerous groundwater observation wells have been installed on the property with wells #'s 2, 3 & 6 located with the areas of the improved Isolated Wetland and Constructed Stormwater Wetland. The peak readings this spring ranged from elevation 51.1 in well no 2 in the northwest corner of the site to 49.6 adjacent to the Isolated Wetlands. These reading were taken on or before May 19th prior to any pumping of groundwater by City Well #2, the golf course irrigation system, or the city pump testing program. Based

on these reading the Isolated Wetland and Constructed Stormwater Wetland will be excavated down to between elevations 49.0 to 50.0 providing high and low marsh zones in these features. However, for our ILSF calculation volume we have not taken credit for storage volume below elevation 52.0. This takes into account potential for any standing groundwater during seasonal high periods as determined by the test pit evaluations. This is the most conservative approach for the ILSF calculation given the local groundwater reading were very high this spring, in the 90 percentile, as determined by the USGS groundwater well located in Newbury at the intersection of Central Street and Route 95.

Please refer to Appendix B for the proposed ILSF hydoCAD hydrology model for the proposed conditions using the City's 8.3" 100 year rainfall depth versus the 7" rainfall as standardly used for this calculation per Massachusetts DEP regulations. Refer to Appendix D for the drainage areas contributing to this ILSF areas and location of the ILSF areas. This calculation rendered a required volume of 579,253 cubic feet for storage. Based upon the proposed grading plan, the peak ILSF elevation is 55.20. This only takes credit for the volume above elevation 52.0. This volume is calculated by a Gird volume analysis using Carlson Software with the proposed site grading. The report summary is provided on the Proposed ILSF Drainage Plan in Appendix D. The project proposes the lowest new home basement elevation at 56.60. This gives 1.4 feet of freeboard above the potential ILSF elevation. The ILSF elevation for the DEP requirement of 7" of rainfall is 54.70 providing for the 444,713 cubic feet required for this event.

The city completed a well pump test on the property pumping 200 gpm for 72 hours. This operation pumped a total of 864,000 gallons or 115,508 cubic feet water that was discharged into the Isolated Vegetated Wetland. During this pump test the water never accumulated more than 12" of depth within an area of 28,430 square feet. Approximately 95,000 cubic feet of the pumped water was infiltrated over a 72 hour period covering the 28,430 square feet. Based on this data the infiltration rate within the Isolated Vegetated Wetland is 0.56" per hour. Using this infiltration rate, the time projected for the ILSf area to drain from an elevation of 54.70 down to elevation 52.0 is approximately 58 hours. This does not take into account the infiltration rate in the proposed meadow area should be double the rate of the IVW area. Based on a Rawl's table, an infiltration rate of 1.02 inches per hour should applied over the meadow area given the proposed sandy loam soils. Using the 0.56" calculated from the pump test gives a conservative estimate of time for the ILSF area to drain.

Standard 3 – Recharge to Groundwater

Standard 3 states that "Loss of annual recharge to groundwater shall be eliminated or minimized through the use of infiltration measures including environmentally sensitive site design, low impact development techniques, stormwater best management practices, and good operation and maintenance. At a minimum, the annual recharge from the post-development site shall approximate the annual recharge from pre-development conditions based on soil type. This condition is met when the stormwater management system is designed to infiltrate the required recharge volume as determined in accordance with the Massachusetts Stormwater Handbook."

The volume of the recharge system was calculated according to the Massachusetts Stormwater Handbook. The proposed site design increases impervious area by 141,262 square feet. For this calculation, all impervious areas will be counted as being on Hydrologic Group A soils having a volume requirement of 0.60 inches multiplied by the new area of impervious cover. **The project proposes five biorentention areas with a minimum sump depth of 8 inches. The bottom of these areas are 3 feet above seasonal high groundwater so can be utilized for groundwater recharge. The sumps of the five bioretention areas provides 10,383 cubic feet of recharge satisfying the groundwater recharge** standard. Additionally, drip edge infiltration trenches will be provided for infiltration of roof runoff. A minimum of 50 linear feet, 18" x 18" stone trench will be provided for each home. With 38 homes, this will provide an additional 1,410 cubic feet of recharge. On this site there is no stomwater runoff from the property. It all ponds and slowly infiltrates in the lower area of the property with 100% of the stomwater recharged other than water lost to evaporation.

Standard 4 – Removal of 80% Total Suspended Solids (TSS)

Standard 4 states that "Stormwater management systems shall be designed to remove 80% of the average annual post-construction load of Total Suspended Solids (TSS). This Standard is met when: (a) Suitable practices for source control and pollution prevention are identified in long-term pollution prevention plan, and thereafter implemented and maintained; (b) Structural stormwater best management practices are sized to capture the required water quality volume determined in accordance with the Massachusetts Stormwater Handbook; and (c) Pretreatment is provided in accordance with the Massachusetts Stormwater Handbook."

Removal of Total Suspended Solids (TSS) is proposed for the developed areas of the site. TSS removal is accomplished by the combination of the following structural and non-structural BMPs:

• Five Bio retention Areas and a Constructed Stormwater Wetland

Below is a summary of each discharge point analyzed and the provided stormwater treatment. The TSS Removal worksheets are also provided in the section.

Constructed Stormwater Wetland "A" – The runoff to this basin is passed a sediment forebay prior to entering the stormwater wetland. <u>80% TSS removal is provided for this drainage area</u>. This area requires 1" water quality volume (WQV) over the new impervious surfaces. The total impervious surface including the Boyd Drive drainage system contributing to this basin is 104,328 sf with a required WQV of 8,694 cubic feet. Basin #A provides 14,336 cubic feet of water quality volume. Refer to details provided in the drawings for a detailed breakdown of the water quality volumes. The required pretreatment is provided in the sediment forebay with 0.1" rendering a required volume of 870 cubic feet and 1,567 cubic feet provided.

For the following five Bio retention areas pretreatment is provided for each. Deep sump catch basins provide 25% TSS removal followed by hydrodynamic separators providing another 25% TSS removal. This provides the required 44% TSS pretreatment requirement.

Bio retention Area "B" – The runoff to this basin is passed thru a deep sump catch basin and particle separator providing pretreatment prior to entering the rain garden. <u>90% TSS removal is provided for this</u> <u>drainage area</u>. This area requires 1" water quality volume (WQV) over the new impervious surfaces. The total impervious surface contributing to this basin is 20,619 sf with a required WQV of 1,718 cubic feet. Bio retention Area "B" provides 2,434 cubic feet of water quality volume in the 8" deep sump.

Bio retention Area "C" – The runoff to this basin is passed thru a deep sump catch basin and particle separator providing pretreatment prior to entering the rain garden. <u>90% TSS removal is provided for this</u> <u>drainage area</u>. This area requires 1" water quality volume (WQV) over the new impervious surfaces. The total impervious surface contributing to this basin is 20,315 sf with a required WQV of 1,692 cubic feet. Bio retention Area "B" provides 1,838 cubic feet of water quality volume in the 8" deep sump.

Bio retention Area "D" – The runoff to this basin is passed thru a deep sump catch basin and particle separator providing pretreatment prior to entering the rain garden. <u>90% TSS removal is provided for this</u> <u>drainage area</u>. This area requires 1" water quality volume (WQV) over the new impervious surfaces. The total impervious surface contributing to this basin is 32,301 sf with a required WQV of 2,692 cubic feet. Bio retention Area "B" provides 3,082 cubic feet of water quality volume in the 8" deep sump.

Bio retention Area "E"– The runoff to this basin is passed thru a deep sump catch basin and particle separator providing pretreatment prior to entering the rain garden. <u>90% TSS removal is provided for this</u> <u>drainage area</u>. This area requires 1" water quality volume (WQV) over the new impervious surfaces. The total impervious surface contributing to this basin is 12,990 sf with a required WQV of 1,082 cubic feet. Bio retention Area "B" provides 1,295 cubic feet of water quality volume in the 8" deep sump.

Bio retention Area "F"- The runoff to this basin is passed thru a deep sump catch basin and particle separator providing pretreatment prior to entering the rain garden. <u>90% TSS removal is provided for this</u> <u>drainage area</u>. This area requires 1" water quality volume (WQV) over the new impervious surfaces. The total impervious surface contributing to this basin is 29,771 sf with a required WQV of 2,481 cubic feet. Bio retention Area "B" provides 2.641 cubic feet of water quality volume in the 8" deep sump.

Standard 5 – Land Uses with Higher Potential Pollutant Loads

Standard 5 states that "For land uses with higher potential pollutant loads, source control and pollution prevention shall be implemented in accordance with the Massachusetts Stormwater Handbook to eliminate or reduce the discharge of stormwater runoff from such land uses to the maximum extent practicable. If through source control and/or pollution prevention all land uses with higher potential pollutant loads cannot be completely protected from exposure to rain, snow, snow melt, and stormwater runoff, the proponent shall use the specific structural stormwater BMPs determined by the Department to be suitable for such uses as provided in the Massachusetts Stormwater Handbook."

The project use is not a Land Use with Higher Potential Pollutant Loads. Therefore, Standard 5 is not applicable to this project.

Standard 6 – Critical Areas

Standard 6 states that "Stormwater discharges within the Zone II or Interim Wellhead Protection Area of a public water supply and stormwater discharges near or to any other critical area require the use of the specific source control and pollution prevention measures and the specific structural stormwater best management practices determined by the Department to be suitable for managing discharges to such areas as provided in the Massachusetts Stormwater Handbook."

The project located in a Zone II wellhead protection area. The Water Quality Volume of 1" x Contributing Impervious Area has been used for sizing all of the bio-retention areas and constructed stormwater wetland. Refer to Standard 4 for detailed water quality calculations.

The project's is not located in estimated habitat or any critical area.

Standard 7 - Redevelopment

Standard 7 states that "A redevelopment project is required to meet the following Stormwater Management Standards only to the maximum extent practicable: Standard 2, Standard 3, and the pretreatment and structural best management practice requirements of Standards 4, 5 and 6. Existing stormwater discharges shall comply with Standard 1 only to the maximum extent practicable. A redevelopment project shall also comply with all other requirements of the Stormwater Management Standards and improve existing conditions."

The proposed project is currently a 9-hole golf course with associated structures and paved parking area. The project fully complies with all DEP Stormwater Standards and additionally brings the existing Boyd Drive drainage system into full compliance with Zone II water quality requirements.

Standard 8 – Erosion and Sedimentation Controls

Standard 8 states that "A plan to control construction related impacts including erosion, sedimentation and other pollutant sources during construction and land disturbance activities (construction period erosion, sedimentation, and pollution prevention plan) shall be developed and implemented."

A Stormwater Pollution Prevention Plan for the Project will be submitted prior to any land disturbance on the site.

Standard 9 – Operation and Maintenance Plans

Standard 9 states: "A long-term operation and maintenance plan shall be developed and implemented to ensure that stormwater management systems function as designed. "

A long-term operation and maintenance plan is included in Appendix C. The Plan includes provisions for Construction-Phase measures, as well as long term maintenance and inspections. Therefore the Project complies with Standard 9.

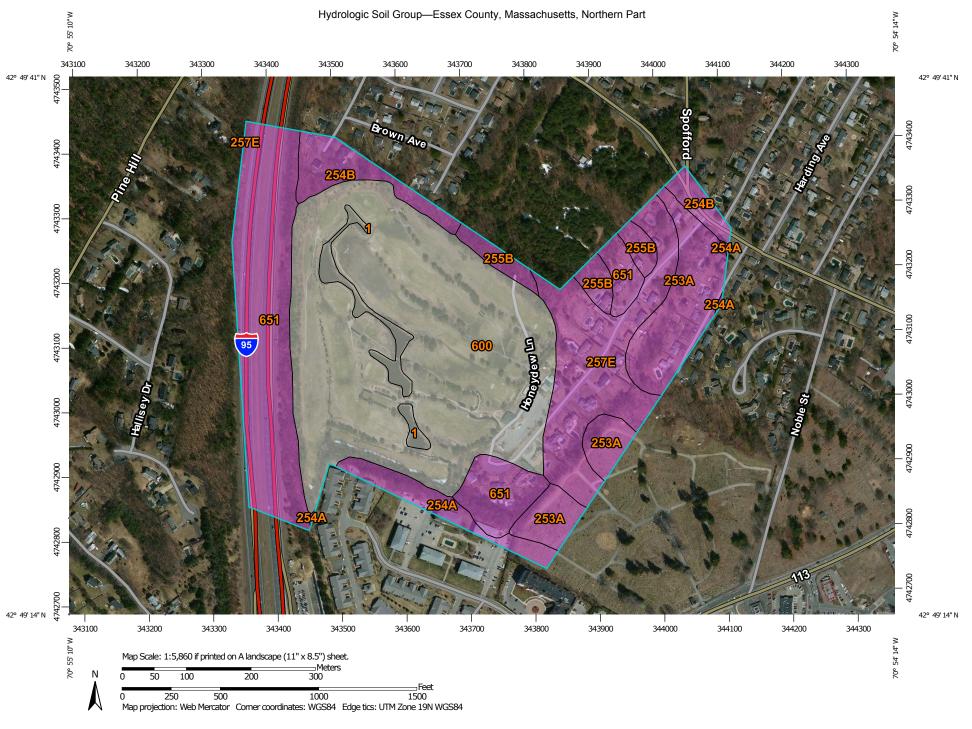
Standard 10 – Illicit Discharges to Drainage System

Standard 10 states: "All illicit discharges to the stormwater management system are prohibited."

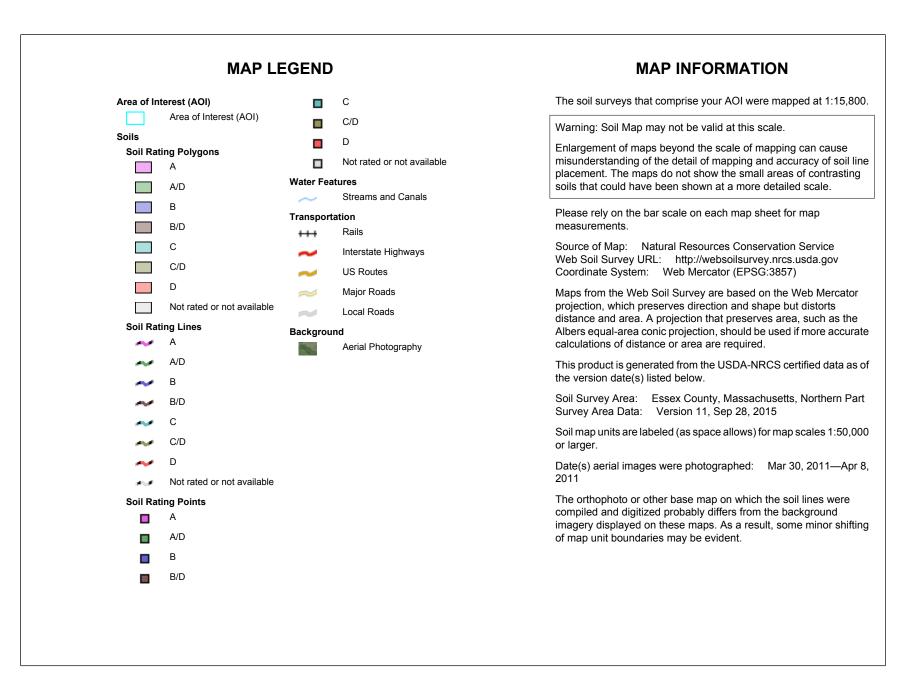
There are no known or suspected illicit discharges to the stormwater management system at the project site. Therefore the Project complies with Standard 10.

Appendix A

USDA NRCS Soil Map, Deep Observation Hole Logs, Observation Well Readings & Test Pit/OW Well Location Figure



USDA Natural Resources Conservation Service





Hydrologic Soil Group

Hydrologic S	Hydrologic Soil Group— Summary by Map Unit — Essex County, Massachusetts, Northern Part (MA605)						
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI			
1	Water		1.8	2.2%			
253A	Hinckley loamy sand, 0 to 3 percent slopes	A	8.6	10.4%			
254A	Merrimac fine sandy loam, 0 to 3 percent slopes	A	2.5	3.1%			
254B	Merrimac fine sandy loam, 3 to 8 percent slopes	A	3.9	4.7%			
255B	Windsor loamy sand, 3 to 8 percent slopes	A	2.5	3.0%			
257E	Hinckley and Windsor soils, 25 to 35 percent slopes	A	10.3	12.4%			
600	Pits, gravel		36.2	43.7%			
651	Udorthents, smoothed	А	16.9	20.4%			
Totals for Area of Inter	rest	·	82.8	100.0%			

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher

SOIL SUITABILITY ASSESSMENT REPORT COMMONWEALTH OF MASSACHUSETTS NEWBURYPORT, MASSACHUSETTS

SOIL SUITABILITY ASSESSMENT FOR ON-SITE STORMWATER MANAGEMENT

SITE INFORMATION

Map 110 & Lot 20

Street Address: <u>18 Boyd Drive</u>Town: <u>Newburyport</u>State: <u>Massachusetts</u>Zip Code: <u>01950</u>County: <u>Essex</u>Land Use: <u>Recreational; Evergreen Golf Course</u>Latitude: <u>~42° 49' 27.3"N</u>Longitude: <u>~70° 54' 46.4" W</u>

PUBLISHED SOIL DATA AND MAP UNIT DESCRIPTION

Physiographic Division: <u>Appalachian Highlands</u> Physio. Province: <u>New England</u> Physio. Section: <u>Seaboard lowland section</u> Soil map unit: <u>254A – Merrimac fine sandy loam (sandy, mixed, mesic, Typic Dystrochrepts), 0-3% slopes</u> NRCS/USDA web soil survey: <u>Essex County, Massachusetts, Northern part.</u> Map Scale: <u>1:500'</u> Hydric or upland soil: <u>Upland soil</u> Average depth to water table: <u>>120''</u> Depth to restrictive feature: <u>>120''</u> Frequency of flooding: <u>None</u> Frequency of ponding: <u>None</u> Available water capacity: <u>Low (~4.6'')</u> Drainage Class: <u>Somewhat excessively drained</u> Hydrologic Soil Group: <u>A</u> Ksat: <u>High (1.42 – 99.00 in/hr)</u> Soil limitations: <u>High permeability, deep seasonal and apparent groundwater elevations, loose & unstable substratum.</u>

WETLAND AREA & USGS WELL MEASUREMENTS

National Wetland Inventory Map: <u>NA</u> Wetlands Conservancy Program: <u>NA</u> Bordering vegetative wetland: <u>>100 feet</u>
Current Water Resource Condition (USGS): <u>Well Site # 424841071004101-MA-HLW 23 Haverhill, MA.</u>,
<u>Well completed in Sand and gravel aquifers and ice-contact deposits, including kames and eskers.</u>
Well depth: <u>15.10 feet</u> Land surface altitude: <u>100.00 feet above NGVD29</u> Latitude: <u>~42°48'41.8" N</u> Longitude: <u>~71°00'41.7"</u>
Most recent data value: 13.01' on 2/03/16 (depth to water level in feet below land surface). Range: Below normal

SURFICIAL & BEDROCK GEOLOGY:

Surficial geology: <u>Osu: Late Pleistocene, Wisconsin Stage – undifferentiated sandy glaciofluvial deposits</u>
Geologic parent material: <u>Sandy proglacial outwash deposits</u> Geomorphic landform: <u>Outwash terrace</u>
Slope aspect: <u>Westerly</u> Landform position (2D): <u>footslope</u> Landform position (3D): <u>tread</u>
Slope gradient: <u>~03-05%</u> Down slope shape: <u>Convex</u> Across slope shape: <u>Convex</u> Slope complexity: <u>Simple</u>
Bedrock outcropping in vicinity: <u>Not observed</u> Glacial erratics in vicinity: <u>None observed</u>
Bedrock Type: <u>Newburyport Volcanic Complex: Lower Devonian, Porphyritic andesite, includes tuffaceous mudstone beds</u>
containing fossils of Late Silurian through Early Devonian age.

TP16-1 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

Date:January 28, 2016Time:12:01Weather:Clear, cool, ~45°F, light East windPosition on landscape:Terrace treadSlope aspect:WesterlyLand Cover:GrassProperty line:10+ feetDrainage way:50+ feetDrinking water well:100+ feetWetlands:100+ feetOpen water body:400+ feetAbutting septic system:NA

SOIL PROFILE ► TP16-1

Depth below land surface (inches)	Soil Horizon/ Layer	Soil Texture (USDA/ NRCS)	Soil Color (Munsell)	Redoxomorphic Features/ ESHGWT	Consistence, grade, size, structure, grain size, soil moisture state, roots, horizon boundary, clasts, stratification, artifacts, restrictive features, etc.
00 → 15"	A _p	Sandy Loam	10YR3/2 very dark grayish brown	none observed	Very friable; moderate-grade fine to medium subangular granular structure; cohesive matrix; fine grained mineral content; slightly damp; common grass roots; free of clasts; clear wavy boundary.
15 → 18"	B_{w}	Loamy Sand	10YR5/6 yellowish brown	none observed	Very friable; moderate-grade fine to medium angular blocky structure; cohesive matrix; mixed medium to mostly fine grained mineral content; damp; ~5% subrounded gravel content; clear smooth boundary.
18 → 101"	С	Sand gravelly	2.5Y5/3 lite olive brown	@ 93" (c,2,p) 7.5R5/8 10Y7/1	Loose; structurless; very unstable; mixed fine to medium grained mineral content; slightly damp matrix; stratified and well graded; ~20% rounded to subrounded gravel & ~15% rounded to subrounded cobble content of mixed lithology; stratified beds dipping gently to the North-Northeast; no redoximorphic features nor apparent water observed and no refusal at test hole depth.

Depth to bedrock: $\geq 101^{\circ}$

Seasonal High Groundwater Table: <u>93</u>"

Phreatic water table (weep) : >101"

TP16-1 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

DEPTH TO APPARENT/ PHREATIC GROUNDWATER TABLE: None Observed

Apparent water seeping from pit face:_____(Below land surface) Depth to stabilized apparent water: _____(Below land surface) Soil moisture state: Damp

ESTIMATED SEASONAL HIGH GROUNDWATER TABLE:

Depth of Estimated Seasonal High Groundwater Table: 93" (below land surface)Type: Masses on sand grainsAbundance: CommonSize: MediumContrast: ProminentShape: Irregular; laminar to spheroidalMoisture state: DampLocation: C matrixHardness: SoftBoundary: DiffuseConcentration color: 7.5R 5/8 (red)Reduction color: 10Y 7/1 (bluish gray)

DETERMINATION OF HIGH GROUNDWATER ELEVATION

 Observed depth to stabilized phreatic water:
 inches below grade

 Observed water weeping from side of deep hole:
 inches below grade

 Observed depth to redoximorphic features:
 93"

 inches below grade
 inches below grade

DEPTH OF NATURALLY OCCURRING PERVIOUS MATERIAL: ► 7.16 feet

Depth of naturally occurring pervious material in TP16-1

Upper boundary: <u>15"</u> Lower boundary: <u>101"</u>

Certification

I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.017.

Alexander F. Parker License #1848

Printed name of evaluator & license number

Unofficial soil evaluation for drainage

Town of Newburyport witness

June 1998

Date of Soil Evaluator Certification

01/28/16

Date of soil testing

TP16-2 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

Date:January 28, 2016Time: 12:14Weather:Clear, cool, ~45°F, light East windPosition on landscape:Terrace treadSlope aspect:WesterlyLand Cover:GrassProperty line:10+ feetDrainage way:50+ feetDrinking water well:100+ feetWetlands:100+ feetOpen water body:400+ feetAbutting septic system:NA

SOIL PROFILE ► TP16-2

Depth below land surface (inches)	Soil Horizon/ Layer	Soil Texture (USDA/ NRCS)	Soil Color (Munsell)	Redoxomorphic Features/ ESHGWT	Consistence, grade, size, structure, grain size, soil moisture state, roots, horizon boundary, clasts, stratification, artifacts, restrictive features, etc.
00 → 05"	A _p	Sandy Loam	10YR3/2 very dark grayish brown	none observed	Very friable; moderate-grade fine to medium subangular granular structure; cohesive matrix; fine grained mineral content; slightly damp; common grass roots; free of clasts; clear wavy boundary.
05 → 47"	C^	Sandy Loam	10YR2/1 black	none observed	Human transported material; Anthropogenic layer; loose; structurless; mixed very fine to medium grained mineral content in a sandy loam matrix; damp; ~15% angular to subangular gravel content of mixed lithology; ash and shells within matrix; clear wavy boundary.
47 → 102"	С	Sand very gravelly	2.5Y5/3 lite olive brown	@ 91" (c,2,p) 7.5R5/8 10Y7/1	Loose; structurless; very unstable; mixed fine to medium grained mineral content; slightly damp matrix; stratified and well graded; ~40% rounded to subrounded gravel & ~20% rounded to subrounded cobble content of mixed lithology; stratified beds dipping gently to the North-Northeast; no refusal at test hole depth.

Depth to bedrock: $\geq 102^{"}$

Seasonal High Groundwater Table: <u>91</u>"

Phreatic water table (weep) : >102"

TP16-2 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

DEPTH TO APPARENT/ PHREATIC GROUNDWATER TABLE: None Observed

Apparent water seeping from pit face:_____(Below land surface) Depth to stabilized apparent water: _____(Below land surface) Soil moisture state: Damp

ESTIMATED SEASONAL HIGH GROUNDWATER TABLE:

Depth of Estimated Seasonal High Groundwater Table: 91" (below land surface)Type: Masses on sand grainsAbundance: CommonSize: MediumContrast: ProminentShape: Irregular; laminar to spheroidalMoisture state: DampLocation: C matrixHardness: SoftBoundary: DiffuseConcentration color: 7.5R 5/8 (red)Reduction color: 10Y 7/1 (bluish gray)

DETERMINATION OF HIGH GROUNDWATER ELEVATION

 Observed depth to stabilized phreatic water:
 inches below grade

 Observed water weeping from side of deep hole:
 inches below grade

 Observed depth to redoximorphic features:
 91"

 inches below grade
 inches below grade

DEPTH OF NATURALLY OCCURRING PERVIOUS MATERIAL: ► 4.58 feet

Depth of naturally occurring pervious material in TP16-2

Upper boundary: $47^{"}$ Lower boundary: $102^{"}$

Certification

I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.017.

Alexander F. Parker License #1848

Printed name of evaluator & license number

Unofficial soil evaluation for drainage

Town of Newburyport witness

June 1998

Date of Soil Evaluator Certification

01/28/16

Date of soil testing

TP16-3 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

Date:January 28, 2016Time: 12:43Weather: Clear, cool, ~45°F, light East windPosition on landscape:Terrace treadSlope aspect:WesterlyLand Cover:Property line:10+ feetDrainage way:50+ feetDrinking water well:100+ feetWetlands:100+ feetOpen water body:400+ feetAbutting septic system:NA

SOIL PROFILE ► TP16-3

Depth below land surface (inches)	Soil Horizon/ Layer	Soil Texture (USDA/ NRCS)	Soil Color (Munsell)	Redoxomorphic Features/ ESHGWT	Consistence, grade, size, structure, grain size, soil moisture state, roots, horizon boundary, clasts, stratification, artifacts, restrictive features, etc.
00 → 06"	A _p	Sandy Loam	10YR3/2 very dark grayish brown	none observed	Very friable; moderate-grade fine to medium subangular granular structure; cohesive matrix; fine grained mineral content; slightly damp; common grass roots; free of clasts; clear wavy boundary.
06 → 42"	C^	Sandy Loam	10YR2/1 black	none observed	Human transported material; Anthropogenic layer; loose; structurless; mixed very fine to medium grained mineral content in a sandy loam matrix; damp; ~15% angular to subangular gravel content of mixed lithology; ash and shells within matrix; clear wavy boundary.
42 → 108"	С	Sand very gravelly	2.5Y5/6 lite olive brown	@ 91" (c,2,p) 7.5R5/8 10Y7/1	Loose; structurless; very unstable; mixed fine to medium grained mineral content; slightly damp matrix; stratified and well graded; ~40% rounded to subrounded gravel & ~20% rounded to subrounded cobble content of mixed lithology; stratified beds dipping gently to the North-Northeast; no refusal at test hole depth.

Depth to bedrock: ≥ 108 "

Seasonal High Groundwater Table: <u>91</u>"

Phreatic water table (weep) : >108"

TP16-3 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

DEPTH TO APPARENT/ PHREATIC GROUNDWATER TABLE: None Observed

Apparent water seeping from pit face:_____(Below land surface) Depth to stabilized apparent water: _____(Below land surface) Soil moisture state: Damp

ESTIMATED SEASONAL HIGH GROUNDWATER TABLE:

Depth of Estimated Seasonal High Groundwater Table: 91" (below land surface)Type: Masses on sand grainsAbundance: CommonSize: MediumContrast: ProminentShape: Irregular; laminar to spheroidalMoisture state: DampLocation: C matrixHardness: SoftBoundary: DiffuseConcentration color: 7.5R 5/8 (red)Reduction color: 10Y 7/1 (bluish gray)

DETERMINATION OF HIGH GROUNDWATER ELEVATION

 Observed depth to stabilized phreatic water:
 inches below grade

 Observed water weeping from side of deep hole:
 inches below grade

 Observed depth to redoximorphic features:
 91"

 inches below grade
 inches below grade

DEPTH OF NATURALLY OCCURRING PERVIOUS MATERIAL: ► 4.58 feet

Depth of naturally occurring pervious material in TP16-3

Upper boundary: $47^{"}$ Lower boundary: $102^{"}$

Certification

I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.017.

Alexander F. Parker License #1848

Printed name of evaluator & license number

Unofficial soil evaluation for drainage

Town of Newburyport witness

June 1998

Date of Soil Evaluator Certification

01/28/16

Date of soil testing

TP16-4 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

Date:January 28, 2016Time: 12:26Weather: Clear, cool, ~45°F, light East windPosition on landscape:Terrace treadSlope aspect:WesterlyLand Cover:Property line:10+ feetDrainage way:50+ feetDrinking water well:100+ feetWetlands:100+ feetOpen water body:400+ feetAbutting septic system:NA

SOIL PROFILE ► TP16-4

Depth below land surface (inches)	Soil Horizon/ Layer	Soil Texture (USDA/ NRCS)	Soil Color (Munsell)	Redoxomorphic Features/ ESHGWT	Consistence, grade, size, structure, grain size, soil moisture state, roots, horizon boundary, clasts, stratification, artifacts, restrictive features, etc.
00 → 11"	A _p	Sandy Loam	10YR3/2 very dark grayish brown	none observed	Very friable; moderate-grade fine to medium subangular granular structure; cohesive matrix; fine grained mineral content; slightly damp; common grass roots; free of clasts; clear wavy boundary.
11 → 52"	C ₁	Sand gravelly	2.5Y5/3 lite olive brown	none observed	Loose; structurless; very unstable; mixed fine to medium grained mineral content; slightly damp matrix; stratified and well graded; ~20% rounded to subrounded gravel & ~15% rounded to subrounded cobble content of mixed lithology; stratified beds dipping gently to the North-Northeast; clear smooth boundary.
52 → 103"	C ₂	Sand	2.5Y5/6 lite olive brown	@ 93" (c,2,p) 7.5R5/8 10Y7/1	Loose; massive angular structure; unstable; mixed very fine to fine grained mineral content; slightly damp matrix; stratified and well graded; ~5% rounded to subrounded content of mixed lithology; stratified beds dipping gently to the North-Northeast; no apparent water observed and no refusal at test hole depth.

Depth to bedrock: ≥ 103 "

Seasonal High Groundwater Table: <u>93</u>"

Phreatic water table (weep) : >103"

TP16-4 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

DEPTH TO APPARENT/ PHREATIC GROUNDWATER TABLE: None Observed

Apparent water seeping from pit face:_____(Below land surface) Depth to stabilized apparent water: _____(Below land surface) Soil moisture state: Damp

ESTIMATED SEASONAL HIGH GROUNDWATER TABLE:

Depth of Estimated Seasonal High Groundwater Table: 93" (below land surface)Type: Masses on sand grainsAbundance: CommonSize: MediumContrast: ProminentShape: Irregular; laminar to spheroidalMoisture state: DampLocation: C2 matrixHardness: SoftBoundary: DiffuseConcentration color: 7.5R 5/8 (red)Reduction color: 10Y 7/1 (bluish gray)

DETERMINATION OF HIGH GROUNDWATER ELEVATION

 Observed depth to stabilized phreatic water:
 inches below grade

 Observed water weeping from side of deep hole:
 inches below grade

 Observed depth to redoximorphic features:
 93"

 inches below grade
 inches below grade

DEPTH OF NATURALLY OCCURRING PERVIOUS MATERIAL: ► 7.66 feet

Depth of naturally occurring pervious material in TP16-4

Upper boundary: <u>11"</u> Lower boundary: <u>103"</u>

Certification

I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.017.

Alexander F. Parker License #1848

Printed name of evaluator & license number

Unofficial soil evaluation for drainage

Town of Newburyport witness

June 1998

Date of Soil Evaluator Certification

01/28/16

Date of soil testing

TP16-5 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

Date:January 28, 2016Time: 12:57Weather:Clear, cool, ~45°F, light East windPosition on landscape:Terrace treadSlope aspect:WesterlyLand Cover:GrassProperty line:10+ feetDrainage way:50+ feetDrinking water well:100+ feetWetlands:100+ feetOpen water body:400+ feetAbutting septic system:NA

SOIL PROFILE ► TP16-5

Depth below land surface (inches)	Soil Horizon/ Layer	Soil Texture (USDA/ NRCS)	Soil Color (Munsell)	Redoxomorphic Features/ ESHGWT	Consistence, grade, size, structure, grain size, soil moisture state, roots, horizon boundary, clasts, stratification, artifacts, restrictive features, etc.
00 → 06"	A _p	Sandy Loam	10YR3/2 very dark grayish brown	none observed	Very friable; moderate-grade fine to medium subangular granular structure; cohesive matrix; fine grained mineral content; slightly damp; common grass roots; free of clasts; clear wavy boundary.
06 → 42"	C^	Sandy Loam gravelly	10YR2/2 very dark brown	none observed	Human transported material; Anthropogenic layer; loose; structurless; mixed very fine to medium grained mineral content in a sandy loam matrix; damp; ~15% angular to subangular gravel content of mixed lithology; ash and shells within matrix; clear wavy boundary.
42 → 110"	С	Sand very gravelly	2.5Y5/6 lite olive brown	@ 89" (c,2,p) 7.5R5/8 10Y7/1	Loose; structurless; very unstable; mixed medium to coarse grained mineral content; slightly damp matrix; stratified and well graded; ~40% rounded to subrounded gravel & ~20% rounded to subrounded cobble content of mixed lithology; stratified beds dipping gently to the North-Northeast; no refusal at test hole depth.

Depth to bedrock: $\geq 110^{\circ\circ}$

Seasonal High Groundwater Table: <u>89</u>"

Phreatic water table (weep) : >110"

TP16-5 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

DEPTH TO APPARENT/ PHREATIC GROUNDWATER TABLE: None Observed

Apparent water seeping from pit face:_____(Below land surface) Depth to stabilized apparent water: _____(Below land surface) Soil moisture state: Damp

ESTIMATED SEASONAL HIGH GROUNDWATER TABLE:

Depth of Estimated Seasonal High Groundwater Table: <u>89</u>" (below land surface)Type: <u>Masses on sand grains</u>Abundance: <u>Common</u>Size: <u>Medium</u>Contrast: <u>Prominent</u>Shape: <u>Irregular; laminar to spheroidal</u>Moisture state: <u>Damp</u>Location: <u>C matrix</u>Hardness: <u>Soft</u>Boundary: <u>Diffuse</u>Concentration color: <u>7.5R 5/8 (red)</u>Reduction color: <u>10Y 7/1 (bluish gray)</u>

DETERMINATION OF HIGH GROUNDWATER ELEVATION

 Observed depth to stabilized phreatic water:
 inches below grade

 Observed water weeping from side of deep hole:
 inches below grade

 Observed depth to redoximorphic features:
 89"

 inches below grade
 inches below grade

DEPTH OF NATURALLY OCCURRING PERVIOUS MATERIAL: ► <u>5.66 feet</u>

Depth of naturally occurring pervious material in TP16-5

Upper boundary: $42^{"}$ Lower boundary: $110^{"}$

Certification

I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.017.

Alexander F. Parker License #1848

Printed name of evaluator & license number

Unofficial soil evaluation for drainage

Town of Newburyport witness

June 1998

Date of Soil Evaluator Certification

01/28/16

TP16-6 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

Date:January 28, 2016Time:13:07Weather:Clear, cool, ~45°F, light East windPosition on landscape:Terrace treadSlope aspect:WesterlyLand Cover:GrassProperty line:10⁺ feetDrainage way:50⁺ feetDrinking water well:100⁺ feetWetlands:100⁺ feetOpen water body:400⁺ feetAbutting septic system:NA

SOIL PROFILE ► TP16-6

Depth below land surface (inches)	Soil Horizon/ Layer	Soil Texture (USDA/ NRCS)	Soil Color (Munsell)	Redoxomorphic Features/ ESHGWT	Consistence, grade, size, structure, grain size, soil moisture state, roots, horizon boundary, clasts, stratification, artifacts, restrictive features, etc.
00 → 08"	A _p	Sandy Loam	10YR3/2 very dark grayish brown	none observed	Very friable; moderate-grade fine to medium subangular granular structure; cohesive matrix; fine grained mineral content; slightly damp; common grass roots; free of clasts; clear wavy boundary.
08 → 65"	C ₁	Sand gravelly	2.5Y5/3 lite olive brown	none observed	Loose; structurless; very unstable; mixed fine to medium grained mineral content; slightly damp matrix; stratified and well graded; ~20% rounded to subrounded gravel & ~15% rounded to subrounded cobble content of mixed lithology; stratified beds dipping gently to the North-Northeast; clear smooth boundary.
65 → 109"	C ₂	Sand	2.5Y6/4 lite yellowish brown	@ 90" (c,2,p) 7.5R5/8 10Y7/1	Loose; massive angular structure; unstable; mixed medium to coarse grained mineral content; slightly damp matrix; stratified and well graded; ~5% rounded to subrounded content of mixed lithology; stratified beds dipping gently to the North-Northeast; no apparent water observed and no refusal at test hole depth.

Depth to bedrock: >109"

Seasonal High Groundwater Table: 90"

Phreatic water table (weep) : >109"

TP16-6 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

DEPTH TO APPARENT/ PHREATIC GROUNDWATER TABLE: None Observed

Apparent water seeping from pit face:_____(Below land surface) Depth to stabilized apparent water: _____(Below land surface) Soil moisture state: Damp

ESTIMATED SEASONAL HIGH GROUNDWATER TABLE:

Depth of Estimated Seasonal High Groundwater Table: 90" (below land surface)Type: Masses on sand grainsAbundance: CommonSize: MediumContrast: ProminentShape: Irregular; laminar to spheroidalMoisture state: DampLocation: C2 matrixHardness: SoftBoundary: DiffuseConcentration color: 7.5R 5/8 (red)Reduction color: 10Y 7/1 (bluish gray)

DETERMINATION OF HIGH GROUNDWATER ELEVATION

 Observed depth to stabilized phreatic water:
 inches below grade

 Observed water weeping from side of deep hole:
 inches below grade

 Observed depth to redoximorphic features:
 90"

 inches below grade
 inches below grade

DEPTH OF NATURALLY OCCURRING PERVIOUS MATERIAL: ► 8.42 feet

Depth of naturally occurring pervious material in TP16-6

Upper boundary: <u>08"</u> Lower boundary: <u>109"</u>

Certification

I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.017.

Alexander F. Parker License #1848

Printed name of evaluator & license number

Unofficial soil evaluation for drainage

Town of Newburyport witness

June 1998

Date of Soil Evaluator Certification

01/28/16

TP16-7 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

Date:January 28, 2016Time: 13:16Weather: Clear, cool, ~45°F, light East windPosition on landscape:Terrace treadSlope aspect:WesterlyLand Cover:Property line:10+ feetDrainage way:50+ feetDrinking water well:100+ feetWetlands:100+ feetOpen water body:400+ feetAbutting septic system:NA

SOIL PROFILE ► TP16-7

Depth below land surface (inches)	surface Horizon/ (USDA/ NRCS) (Munse		Soil Color (Munsell)	Redoxomorphic Features/ ESHGWT	Consistence, grade, size, structure, grain size, soil moisture state, roots, horizon boundary, clasts, stratification, artifacts, restrictive features, etc.
00 → 62"	C^	Sandy Loam gravelly	10YR2/2 very dark brown	none observed	Human transported material; Anthropogenic layer; loose; structurless; mixed very fine to medium grained mineral content in a sandy loam matrix; damp; ~15% angular to subangular gravel content of mixed lithology; ash and shells within matrix; clear wavy boundary.
62 → 110"	С	Sand very gravelly	2.5Y6/4 lite yellowish brown	@ 89" (c,2,p) 7.5R5/8 10Y7/1	Loose; structurless; very unstable; mixed medium to coarse grained mineral content; slightly damp matrix; stratified and well graded; ~40% rounded to subrounded gravel & ~20% rounded to subrounded cobble content of mixed lithology; stratified beds dipping gently to the North-Northeast; no refusal at test hole depth.

Depth to bedrock: $\geq 110^{\circ\circ}$

Seasonal High Groundwater Table: <u>89</u>"

Phreatic water table (weep) : >110"

TP16-7 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

DEPTH TO APPARENT/ PHREATIC GROUNDWATER TABLE: None Observed

Apparent water seeping from pit face:_____(Below land surface) Depth to stabilized apparent water: _____(Below land surface) Soil moisture state: Damp

ESTIMATED SEASONAL HIGH GROUNDWATER TABLE:

Depth of Estimated Seasonal High Groundwater Table: <u>89</u>" (below land surface)Type: Masses on sand grainsAbundance: CommonSize: MediumContrast: ProminentShape: Irregular; laminar to spheroidalMoisture state: DampLocation: C matrixHardness: SoftBoundary: DiffuseConcentration color: 7.5R 5/8 (red)Reduction color: 10Y 7/1 (bluish gray)

DETERMINATION OF HIGH GROUNDWATER ELEVATION

 Observed depth to stabilized phreatic water:
 inches below grade

 Observed water weeping from side of deep hole:
 inches below grade

 Observed depth to redoximorphic features:
 89"

 inches below grade
 inches below grade

DEPTH OF NATURALLY OCCURRING PERVIOUS MATERIAL: ► <u>5.66 feet</u>

Depth of naturally occurring pervious material in TP16-7

Upper boundary: $42^{"}$ Lower boundary: $110^{"}$

Certification

I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.017.

Alexander F. Parker License #1848

Printed name of evaluator & license number

Unofficial soil evaluation for drainage

Town of Newburyport witness

June 1998

Date of Soil Evaluator Certification

01/28/16

TP16-8 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

Date:January 28, 2016Time: 13:45Weather:Clear, cool, ~45°F, light East windPosition on landscape:Terrace treadSlope aspect:WesterlyLand Cover:GrassProperty line:10+ feetDrainage way:50+ feetDrinking water well:100+ feetWetlands:100+ feetOpen water body:400+ feetAbutting septic system:NA

SOIL PROFILE ► TP16-8

Depth below land surface (inches)	Soil Horizon/ Layer	Soil Texture (USDA/ NRCS)	Soil Color (Munsell)	Redoxomorphic Features/ ESHGWT	Consistence, grade, size, structure, grain size, soil moisture state, roots, horizon boundary, clasts, stratification, artifacts, restrictive features, etc.
00 → 08"	A _p	Sandy Loam	10YR3/2 very dark grayish brown	none observed	Very friable; moderate-grade fine to medium subangular granular structure; cohesive matrix; fine grained mineral content; slightly damp; common grass roots; free of clasts; clear wavy boundary.
08 → 61"	C^	Loamy Sand	2.5Y5/2 grayish brown	none observed	Human transported material; Anthropogenic layer; loose; structurless; mixed very fine to medium grained mineral content in a sandy loam matrix; damp; ~5% angular to subangular gravel content of mixed lithology; ash and shells within matrix; clear wavy boundary.
61 → 112"	С	Sand gravelly	2.5Y7/3 pale yellow	@ 92" (c,2,p) 7.5R5/8 10Y7/1	Loose; structurless; very unstable; mixed fine to medium grained mineral content; slightly damp matrix; stratified and well graded; ~20% rounded to subrounded gravel & ~5% rounded to subrounded cobble content of mixed lithology; stratified beds dipping gently to the North-Northeast; no refusal at test hole depth.

Depth to bedrock: >112"

Seasonal High Groundwater Table: <u>92</u>"

Phreatic water table (weep) : >112"

TP16-8 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

DEPTH TO APPARENT/ PHREATIC GROUNDWATER TABLE: None Observed

Apparent water seeping from pit face:_____(Below land surface) Depth to stabilized apparent water: _____(Below land surface) Soil moisture state: Damp

ESTIMATED SEASONAL HIGH GROUNDWATER TABLE:

Depth of Estimated Seasonal High Groundwater Table: 92" (below land surface)Type: Masses on sand grainsAbundance: CommonSize: MediumContrast: ProminentShape: Irregular; laminar to spheroidalMoisture state: DampLocation: C matrixHardness: SoftBoundary: DiffuseConcentration color: 7.5R 5/8 (red)Reduction color: 10Y 7/1 (bluish gray)

DETERMINATION OF HIGH GROUNDWATER ELEVATION

 Observed depth to stabilized phreatic water:
 inches below grade

 Observed water weeping from side of deep hole:
 inches below grade

 Observed depth to redoximorphic features:
 92"

 inches below grade
 inches below grade

DEPTH OF NATURALLY OCCURRING PERVIOUS MATERIAL: ► 4.25 feet

Depth of naturally occurring pervious material in TP16-8

Upper boundary: $\underline{61^{"}}$ Lower boundary: $\underline{112^{"}}$

Certification

I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.017.

Alexander F. Parker License #1848

Printed name of evaluator & license number

Unofficial soil evaluation for drainage

Town of Newburyport witness

June 1998

Date of Soil Evaluator Certification

01/28/16

TP16-9 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

Date:January 28, 2016Time: 13:21Weather:Clear, cool, ~45°F, light East windPosition on landscape:Terrace treadSlope aspect:WesterlyLand Cover:GrassProperty line:10+ feetDrainage way:50+ feetDrinking water well:100+ feetWetlands:100+ feetOpen water body:400+ feetAbutting septic system:NA

SOIL PROFILE ► TP16-9

Depth below land surface (inches)	Soil Horizon/ Layer	Soil Texture (USDA/ NRCS) Soil Color (Munsell) Features/ ESHGWT			Consistence, grade, size, structure, grain size, soil moisture state, roots, horizon boundary, clasts, stratification, artifacts, restrictive features, etc.
00 → 12"	C^	Sandy Loam	10YR2/2 very dark brown	none observed	Human transported material; Anthropogenic layer; loose; structurless; mixed very fine to medium grained mineral content in a sandy loam matrix; damp; ~5% angular to subangular gravel content of mixed lithology; ash and shells within matrix; clear wavy boundary.
12 → 98"	С	Sand very gravelly	2.5Y6/4 lite yellowish brown	@ 66" (m,2,p) 7.5R5/8 10Y7/1	Loose; structurless; very unstable; mixed medium to coarse grained mineral content; slightly damp matrix; stratified and well graded; ~40% rounded to subrounded gravel & ~20% rounded to subrounded cobble content of mixed lithology; stratified beds dipping gently to the North-Northeast; no refusal at test hole depth.

Depth to bedrock: ≥ 98 "

Seasonal High Groundwater Table: <u>66</u>"

Phreatic water table (weep) : <u>>98</u>"

TP16-9 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

DEPTH TO APPARENT/ PHREATIC GROUNDWATER TABLE: None Observed

Apparent water seeping from pit face:_____(Below land surface) Depth to stabilized apparent water: _____(Below land surface) Soil moisture state: Damp

ESTIMATED SEASONAL HIGH GROUNDWATER TABLE:

Depth of Estimated Seasonal High Groundwater Table: 66" (below land surface)Type: Masses on sand grainsAbundance: ManySize: MediumContrast: ProminentShape: Irregular; laminar to spheroidalMoisture state: DampLocation: C matrixHardness: SoftBoundary: DiffuseConcentration color: 7.5R 5/8 (red)Reduction color: 10Y 7/1 (bluish gray)

DETERMINATION OF HIGH GROUNDWATER ELEVATION

 Observed depth to stabilized phreatic water:
 inches below grade

 Observed water weeping from side of deep hole:
 inches below grade

 Observed depth to redoximorphic features:
 <u>66</u>" inches below grade

DEPTH OF NATURALLY OCCURRING PERVIOUS MATERIAL: ► 7.16 feet

Depth of naturally occurring pervious material in TP16-9

Upper boundary: <u>12</u>" Lower boundary: <u>98</u>"

Certification

I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.017.

Alexander F. Parker License #1848

Printed name of evaluator & license number

Unofficial soil evaluation for drainage

Town of Newburyport witness

June 1998

Date of Soil Evaluator Certification

<u>01/28/16</u>

TP16-10 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

Date:January 28, 2016Time: 13:15Weather:Clear, cool, ~45°F, light East windPosition on landscape:Terrace treadSlope aspect:WesterlyLand Cover:GrassProperty line:10+ feetDrainage way:50+ feetDrinking water well:100+ feetWetlands:100+ feetOpen water body:400+ feetAbutting septic system:NA

SOIL PROFILE ► TP16-10

Depth below land surface (inches)	Soil Horizon/ Layer	Soil Texture (USDA/ NRCS)	Soil Color (Munsell)	Redoxomorphic Features/ ESHGWT	Consistence, grade, size, structure, grain size, soil moisture state, roots, horizon boundary, clasts, stratification, artifacts, restrictive features, etc.
00 → 06"	A _p	Sandy Loam	10YR3/2 very dark grayish brown	none observed	Very friable; moderate-grade fine to medium subangular granular structure; cohesive matrix; fine grained mineral content; slightly damp; common grass roots; free of clasts; clear wavy boundary.
06 → 25"	C^	Loamy Sand	2.5Y5/2 grayish brown	none observed	Human transported material; Anthropogenic layer; loose; structurless; mixed very fine to medium grained mineral content in a sandy loam matrix; damp; ~5% angular to subangular gravel content of mixed lithology; ash and shells within matrix; clear wavy boundary.
25 → 100"	С	Sand gravelly	2.5Y7/3 pale yellow	@ 70" (c,2,p) 7.5R5/8 10Y7/1	Loose; structurless; very unstable; mixed fine to medium grained mineral content; slightly damp matrix; stratified and well graded; ~20% rounded to subrounded gravel & ~5% rounded to subrounded cobble content of mixed lithology; stratified beds dipping gently to the North-Northeast; no refusal at test hole depth.

Depth to bedrock: $\geq 100^{\circ\circ}$

Seasonal High Groundwater Table: <u>70</u>"

Phreatic water table (weep) : >100"

TP16-10 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

DEPTH TO APPARENT/ PHREATIC GROUNDWATER TABLE: None Observed

Apparent water seeping from pit face:_____(Below land surface) Depth to stabilized apparent water: _____(Below land surface) Soil moisture state: Damp

ESTIMATED SEASONAL HIGH GROUNDWATER TABLE:

Depth of Estimated Seasonal High Groundwater Table: 70" (below land surface)Type: Masses on sand grainsAbundance: CommonSize: MediumContrast: ProminentShape: Irregular; laminar to spheroidalMoisture state: DampLocation: C matrixHardness: SoftBoundary: DiffuseConcentration color: 7.5R 5/8 (red)Reduction color: 10Y 7/1 (bluish gray)

DETERMINATION OF HIGH GROUNDWATER ELEVATION

 Observed depth to stabilized phreatic water:
 inches below grade

 Observed water weeping from side of deep hole:
 inches below grade

 Observed depth to redoximorphic features:
 70"

 inches below grade
 inches below grade

DEPTH OF NATURALLY OCCURRING PERVIOUS MATERIAL: ► 6.25 feet

Depth of naturally occurring pervious material in TP16-10

Upper boundary: <u>25"</u> Lower boundary: <u>100"</u>

Certification

I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.017.

Alexander F. Parker License #1848

Printed name of evaluator & license number

Unofficial soil evaluation for drainage

Town of Newburyport witness

June 1998

Date of Soil Evaluator Certification

01/28/16

TP16-11 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

Date:January 28, 2016Time: 13:24Weather:Clear, cool, ~45°F, light East windPosition on landscape:Terrace treadSlope aspect:WesterlyLand Cover:GrassProperty line:10+ feetDrainage way:50+ feetDrinking water well:100+ feetWetlands:100+ feetOpen water body:400+ feetAbutting septic system:NA

SOIL PROFILE ► TP16-11

Depth below land surface (inches)	Soil Horizon/ Layer	Soil Texture (USDA/ NRCS)	Soil Color (Munsell)	Redoxomorphic Features/ ESHGWT	Consistence, grade, size, structure, grain size, soil moisture state, roots, horizon boundary, clasts, stratification, artifacts, restrictive features, etc.
00 → 09"	A _p	Sandy Loam	10YR3/2 very dark grayish brown	none observed	Very friable; moderate-grade fine to medium subangular granular structure; cohesive matrix; fine grained mineral content; slightly damp; common grass roots; free of clasts; clear wavy boundary.
09 → 70"	C ₁	Sand gravelly	2.5Y5/3 lite olive brown	none observed	Loose; structurless; very unstable; mixed fine to medium grained mineral content; slightly damp matrix; stratified and well graded; ~20% rounded to subrounded gravel & ~15% rounded to subrounded cobble content of mixed lithology; stratified beds dipping gently to the North-Northeast; clear smooth boundary.
70 → 100"	C ₂	Sand	2.5Y6/4 lite yellowish brown	@ 93" (c,2,p) 7.5R5/8 10Y7/1	Loose; massive angular structure; unstable; mixed medium to coarse grained mineral content; slightly damp matrix; stratified and well graded; ~5% rounded to subrounded content of mixed lithology; stratified beds dipping gently to the North-Northeast; no apparent water observed and no refusal at test hole depth.

Depth to bedrock: >100"

Seasonal High Groundwater Table: <u>93</u>"

Phreatic water table (weep) : >100"

TP16-11 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

DEPTH TO APPARENT/ PHREATIC GROUNDWATER TABLE: None Observed

Apparent water seeping from pit face:_____(Below land surface) Depth to stabilized apparent water: _____(Below land surface) Soil moisture state: Damp

ESTIMATED SEASONAL HIGH GROUNDWATER TABLE:

Depth of Estimated Seasonal High Groundwater Table: 93" (below land surface)Type: Masses on sand grainsAbundance: CommonSize: MediumContrast: ProminentShape: Irregular; laminar to spheroidalMoisture state: DampLocation: C2 matrixHardness: SoftBoundary: DiffuseConcentration color: 7.5R 5/8 (red)Reduction color: 10Y 7/1 (bluish gray)

DETERMINATION OF HIGH GROUNDWATER ELEVATION

 Observed depth to stabilized phreatic water:
 inches below grade

 Observed water weeping from side of deep hole:
 inches below grade

Observed depth to redoximorphic features: <u>93</u>" inches below grade

DEPTH OF NATURALLY OCCURRING PERVIOUS MATERIAL: ► 7.58 feet

Depth of naturally occurring pervious material in TP16-11

Upper boundary: <u>09"</u> Lower boundary: <u>100"</u>

Certification

I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.017.

Alexander F. Parker License #1848

Printed name of evaluator & license number

Unofficial soil evaluation for drainage

Town of Newburyport witness

June 1998

Date of Soil Evaluator Certification

01/28/16

TP16-12 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

Date:January 28, 2016Time: 13:55Weather:Clear, cool, ~45°F, light East windPosition on landscape:Terrace treadSlope aspect:WesterlyLand Cover:GrassProperty line:10+ feetDrainage way:50+ feetDrinking water well:100+ feetWetlands:100+ feetOpen water body:400+ feetAbutting septic system:NA

SOIL PROFILE ► TP16-12

Depth below land surface (inches)	e Horizon/ (USDA/ NRCS) (Munsell) Fea		Redoxomorphic Features/ ESHGWT	Consistence, grade, size, structure, grain size, soil moisture state, roots, horizon boundary, clasts, stratification, artifacts, restrictive features, etc.	
00 → 41"	C^	Sandy Loam	10YR2/2 very dark brown	none observed	Human transported material; Anthropogenic layer; loose; structurless; mixed very fine to medium grained mineral content in a sandy loam matrix; damp; ~5% angular to subangular gravel content of mixed lithology; ash and shells within matrix; clear wavy boundary.
41 → 98"	С	Sand very gravelly	2.5Y6/4 lite yellowish brown	@ 85" (m,2,p) 7.5R5/8 10Y7/1	Loose; structurless; very unstable; mixed medium to coarse grained mineral content; slightly damp matrix; stratified and well graded; ~40% rounded to subrounded gravel & ~20% rounded to subrounded cobble content of mixed lithology; stratified beds dipping gently to the North-Northeast; no refusal at test hole depth.

Depth to bedrock: ≥ 98 "

Seasonal High Groundwater Table: <u>85</u>"

Phreatic water table (weep) : <u>>98</u>"

TP16-12 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

DEPTH TO APPARENT/ PHREATIC GROUNDWATER TABLE: None Observed

Apparent water seeping from pit face:_____(Below land surface) Depth to stabilized apparent water: _____(Below land surface) Soil moisture state: Damp

ESTIMATED SEASONAL HIGH GROUNDWATER TABLE:

Depth of Estimated Seasonal High Groundwater Table: 85" (below land surface)Type: Masses on sand grainsAbundance: ManySize: MediumContrast: ProminentShape: Irregular; laminar to spheroidalMoisture state: DampLocation: C matrixHardness: SoftBoundary: DiffuseConcentration color: 7.5R 5/8 (red)Reduction color: 10Y 7/1 (bluish gray)

DETERMINATION OF HIGH GROUNDWATER ELEVATION

 Observed depth to stabilized phreatic water:
 inches below grade

 Observed water weeping from side of deep hole:
 inches below grade

Observed depth to redoximorphic features: <u>85</u>" inches below grade

DEPTH OF NATURALLY OCCURRING PERVIOUS MATERIAL: ► 4.75 feet

Depth of naturally occurring pervious material in TP16-12

Upper boundary: <u>41</u>" Lower boundary: <u>98</u>"

Certification

I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.017.

Alexander F. Parker License #1848

Printed name of evaluator & license number

Unofficial soil evaluation for drainage

Town of Newburyport witness

June 1998

Date of Soil Evaluator Certification

01/28/16

TP16-13 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

Date:January 28, 2016Time: 12:37Weather: Clear, cool, ~45°F, light East windPosition on landscape:Terrace treadSlope aspect:WesterlyLand Cover:Property line:10+ feetDrainage way:50+ feetDrinking water well:100+ feetWetlands:100+ feetOpen water body:400+ feetAbutting septic system:NA

SOIL PROFILE ► TP16-13

Depth below land surface (inches)	Soil Horizon/ Layer	zon/ (USDA/ NRCS) (Munsell) Features/			Consistence, grade, size, structure, grain size, soil moisture state, roots, horizon boundary, clasts, stratification, artifacts, restrictive features, etc.		
00 → 24"	C^	Sandy Loam	10YR2/2 very dark brown	none observed	Human transported material; Anthropogenic layer; loose; structurless; mixed very fine to medium grained mineral content in a sandy loam matrix; damp; ~5% angular to subangular gravel content of mixed lithology; ash and shells within matrix; clear wavy boundary.		
24 → 100"	С	Sand very gravelly	2.5Y6/4 lite yellowish brown	@ 70" (m,2,p) 7.5R5/8 10Y7/1	Loose; structurless; very unstable; mixed medium to coarse grained mineral content; slightly damp matrix; stratified and well graded; ~40% rounded to subrounded gravel & ~20% rounded to subrounded cobble content of mixed lithology; stratified beds dipping gently to the North-Northeast; no refusal at test hole depth.		

Depth to bedrock: $\geq 100^{\circ\circ}$

Seasonal High Groundwater Table: <u>70</u>"

Phreatic water table (weep) : >100"

TP16-13 DEEP OBSERVATION HOLE

18 Boyd Drive, Newburyport, Massachusetts

DEPTH TO APPARENT/ PHREATIC GROUNDWATER TABLE: None Observed

Apparent water seeping from pit face:_____(Below land surface) Depth to stabilized apparent water: _____(Below land surface) Soil moisture state: Damp

ESTIMATED SEASONAL HIGH GROUNDWATER TABLE:

Depth of Estimated Seasonal High Groundwater Table: 70" (below land surface)Type: Masses on sand grainsAbundance: ManySize: MediumContrast: ProminentShape: Irregular; laminar to spheroidalMoisture state: DampLocation: C matrixHardness: SoftBoundary: DiffuseConcentration color: 7.5R 5/8 (red)Reduction color: 10Y 7/1 (bluish gray)

DETERMINATION OF HIGH GROUNDWATER ELEVATION

 Observed depth to stabilized phreatic water:
 inches below grade

 Observed water weeping from side of deep hole:
 inches below grade

 Observed depth to redoximorphic features:
 70"

 inches below grade
 inches below grade

DEPTH OF NATURALLY OCCURRING PERVIOUS MATERIAL: ► 6.33 feet

Depth of naturally occurring pervious material in TP16-13

Upper boundary: <u>24"</u> Lower boundary: <u>100"</u>

Certification

I certify that I am currently approved by the Department of Environmental Protection pursuant to 310 CMR 15.017 to conduct evaluations and that the above analysis has been performed by me consistent with the required training, expertise and experience described in 310 CMR 15.017. I further certify that the results of my soil evaluation, as indicated in the attached Soil Evaluation Form, are accurate and in accordance with 310 CMR 15.017.

Alexander F. Parker License #1848

Printed name of evaluator & license number

Unofficial soil evaluation for drainage

Town of Newburyport witness

June 1998

Date of Soil Evaluator Certification

01/28/16

Frimpter High Groundwater Analysis

Well No.	S _c	S _r	OW _c	OW _{max}	OW _r	S _h	Ground Elev	Frimpter GW Elev	GW Elev on 4/30/17
1	9.7	4.2	3.46	0.94	10.47	8.69	60.50	51.81	50.80
3	6.1	4.2	3.46	0.94	10.47	5.09	55.10	50.01	49.00
7	11.7	4.2	3.46	0.94	10.47	10.69	61.10	50.41	49.40
5	8.6	4.2	3.46	0.94	10.47	7.59	57.00	49.41	48.40
6	7.2	4.2	3.46	0.94	10.47	6.19	56.80	50.61	49.60

S_c measured depth to water at the site

S_h estimated depth to probable high water level at site

 OW_c measured depth to water in the observation well which is used to correlate with the water levels at the site

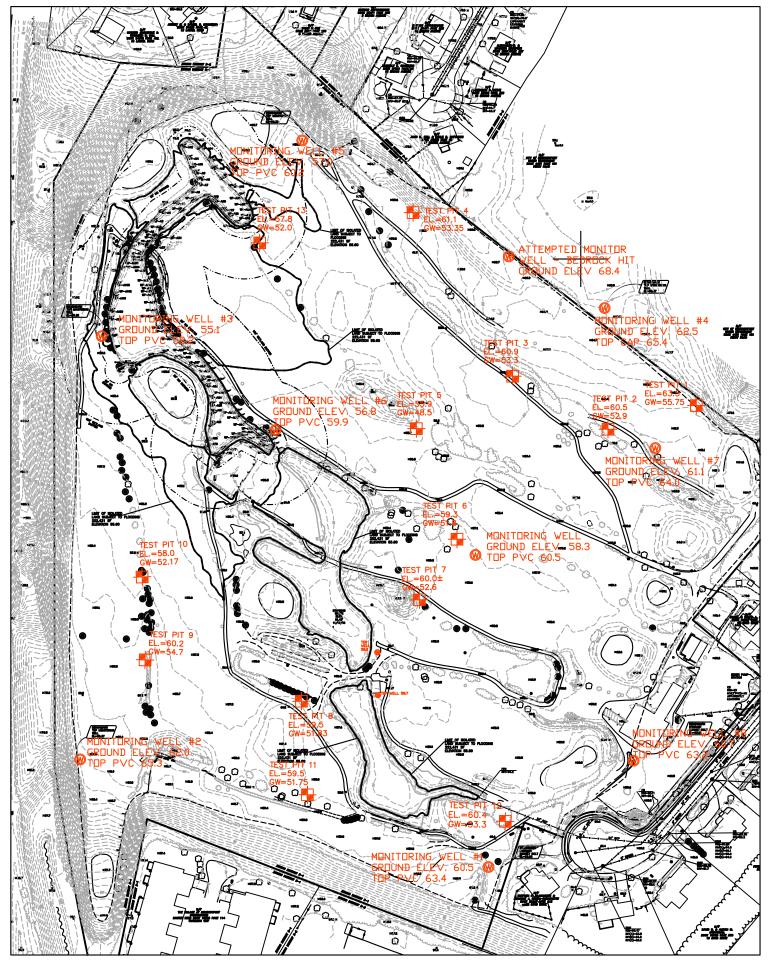
OW_{max} depth to recorded maximum water level at the observation well which is used to correlate with the water levels at the site

 S_r range of water level where the site is located. Values range with varying exceedance probabilities may be selected from figures 8, 11 or 12. For example, a range of 10 feet would be expected to be exceeded at 5 percent of sites in sand and gravel on terraces

OW_r recorded upper limit of annual range of water level at the observation well which is used to correlate with the water levels at the site

Well No.	Ground Elev	GW Elev on 5/08/17	GW Elev on 5/19/17				
1	60.50	50.80	51.00				
2	62.00	50.80	51.10				
3	55.10	49.10	49.80				
5	57.00	48.40	49.10				
6	56.80	49.60	50.10				
7	61.10	49.40	50.10				

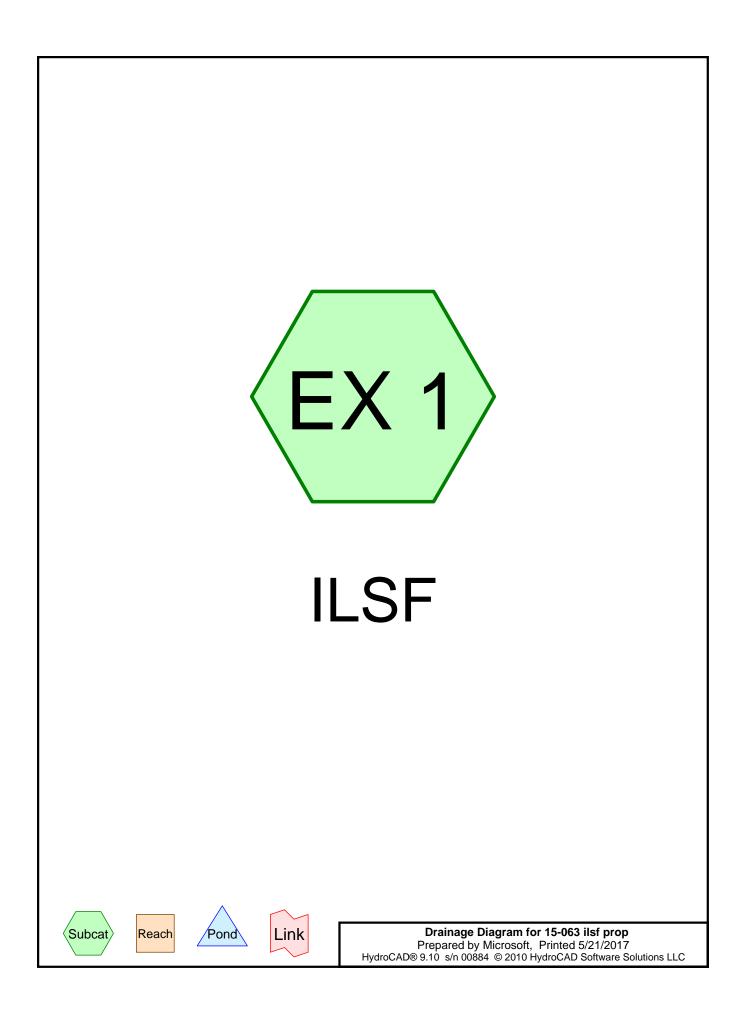
Groundwater Readings



OBSERVATION WELL & TEST PIT LOCATIONS

Appendix B

HydroCAD Hydrology Printouts, Proposed ILSF, Existing & Proposed Drainage Areas



Area Listing (all nodes)

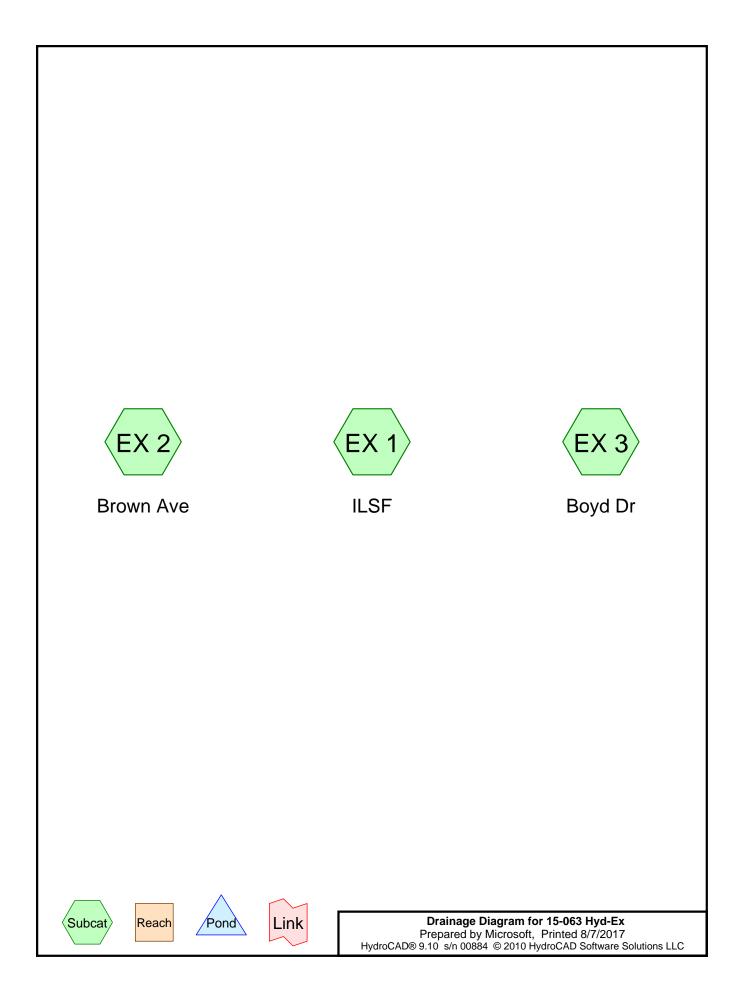
Area (sq-ft)	CN	Description (subcatchment-numbers)
235,450	30	Meadow, non-grazed, HSG A (EX 1)
308,381	30	Woods, Good, HSG A (EX 1)
1,157,906	39	>75% Grass cover, Good, HSG A (EX 1)
19,050	76	Gravel roads, HSG A (EX 1)
130,466	98	Bldg, HSG A (EX 1)
224,140	98	Impervious path, roads, HSG A (EX 1)
278,856	98	Wetlands, HSG A (EX 1)

Summary for Subcatchment EX 1: ILSF

Runoff = 145.07 cfs @ 12.09 hrs, Volume= 579,253 cf, Depth> 2.95"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 2.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

	Area (sf)	CN	Description
*	278,856	98	Wetlands, HSG A
	308,381	30	Woods, Good, HSG A
*	130,466	98	Bldg, HSG A
*	224,140	98	Impervious path, roads, HSG A
	19,050	76	Gravel roads, HSG A
	1,157,906	39	>75% Grass cover, Good, HSG A
	235,450	30	Meadow, non-grazed, HSG A
	2,354,249	53	Weighted Average
	1,720,787	37	73.09% Pervious Area
	633,462	98	26.91% Impervious Area
	Tc Length	Slop	
	(min) (feet)	(ft/	/ft) (ft/sec) (cfs)
	6.0		Direct Entry,
			-



Area Listing (all nodes)

Area	CN	Description		
(sq-ft)		(subcatchment-numbers)		
159,103	30	Woods, Good, HSG A (EX 1, EX 2)		
1,158,318	39	>75% Grass cover, Good, HSG A (EX 1, EX 2, EX 3)		
70,710	98	Bdg & Pavement HSG A (EX 1)		
32,748	98	Bldg & Pavement, HSG A (EX 2, EX 3)		
222,431	98	Wetlands, HSG A (EX 1)		

Summary for Subcatchment EX 1: ILSF

Runoff = 20.23 cfs @ 12.08 hrs, Volume= 69,964 cf, Depth> 0.54"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 2.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

Description				
Wetlands, HSG A				
Bdg & Pavement HSG A				
81.24% Pervious Area				
18.76% Impervious Area				

Summary for Subcatchment EX 2: Brown Ave

Runoff = 0.17 cfs @ 12.13 hrs, Volume= 659 cf, Depth> 0.19"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 2.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

_	A	Area (sf)	CN	Description				
		21,553	30	,	Noods, Good, HSG A			
*		2,761	98	Bldg & Pave	ement, HS0	G A		
_		18,010	39	>75% Gras	s cover, Go	bod, HSG A		
		42,324	38	Weighted A	verage			
		39,563	34	93.48% Per	vious Area			
		2,761	98	6.52% Impe	ervious Are	a		
				-				
	Tc	Length	Slop	e Velocity	Capacity	Description		
_	(min)	(feet)	(ft/ft		(cfs)			
_	8.9	50	0.180	0.09		Sheet Flow,		
						Woods: Dense underbrush n= 0.800 P2= 3.20"		
	0.8	160	0.050	0 3.35		Shallow Concentrated Flow,		
						Grassed Waterway Kv= 15.0 fps		
	97	210	Total					

9.7 210 Total

Summary for Subcatchment EX 3: Boyd Dr

Runoff = 2.07 cfs @ 12.08 hrs, Volume= 7,157 cf, Depth> 2.23"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 2.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

15-063 Hyd-Ex

Type III 24-hr 2 Year Rainfall=3.10" Printed 8/7/2017 Page 4

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	Area (sf)	CN	Description	Description					
*	29,987	98	Bldg & Pave	Bldg & Pavement, HSG A					
	8,585	39	>75% Grass	>75% Grass cover, Good, HSG A					
	38,572	85	Weighted Av	Weighted Average					
	8,585	39	22.26% Per	22.26% Pervious Area					
	29,987	98	77.74% Impervious Area						
	Tc Length	Slop	e Velocity	Capacity	Description				
(r	nin) (feet)	(ft/f	t) (ft/sec)	(cfs)					
	6.0				Direct Entry,				

Summary for Subcatchment EX 1: ILSF

Runoff = 30.92 cfs @ 12.08 hrs, Volume= 120,968 cf, Depth> 0.93"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 2.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

Description				
Wetlands, HSG A				
Bdg & Pavement HSG A				
81.24% Pervious Area				
18.76% Impervious Area				

Summary for Subcatchment EX 2: Brown Ave

Runoff = 0.26 cfs @ 12.13 hrs, Volume= 1,131 cf, Depth> 0.32"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 2.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

_	A	Area (sf)	CN	Description		
		21,553	30	Woods, Go	od, HSG A	
*		2,761	98	Bldg & Pav	ement, HS0	GA
_		18,010	39	>75% Gras	s cover, Go	bod, HSG A
		42,324	38	Weighted A	verage	
		39,563	34	93.48% Per	rvious Area	
		2,761	98	6.52% Impe	ervious Area	a
				-		
	Tc	Length	Slop	e Velocity	Capacity	Description
	(min)	(feet)	(ft/ft	t) (ft/sec)	(cfs)	
	8.9	50	0.180	0 0.09		Sheet Flow,
						Woods: Dense underbrush n= 0.800 P2= 3.20"
	0.8	160	0.050	0 3.35		Shallow Concentrated Flow,
						Grassed Waterway Kv= 15.0 fps
-	07	210	Total			

9.7 210 Total

Summary for Subcatchment EX 3: Boyd Dr

Runoff = 3.16 cfs @ 12.08 hrs, Volume= 11,224 cf, Depth> 3.49"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 2.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

Type III 24-hr 10 Year Rainfall=4.70" Printed 8/7/2017 Page 6

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	Area (sf)	CN	Description	Description				
*	29,987	98	Bldg & Paver	Bldg & Pavement, HSG A				
	8,585	39	>75% Grass of	•75% Grass cover, Good, HSG A				
	38,572	85	Weighted Ave	Weighted Average				
	8,585	39	22.26% Pervic	22.26% Pervious Area				
	29,987	98	77.74% Imper	77.74% Impervious Area				
(m	Tc Length nin) (feet)	Slop (ft/		Capacity (cfs)	Description			
<u> </u>	/	(IV		(015)				
	6.0				Direct Entry,			

Summary for Subcatchment EX 1: ILSF

Runoff = 79.04 cfs @ 12.10 hrs, Volume= 321,096 cf, Depth> 2.47"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 2.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

Description				
Wetlands, HSG A				
Bdg & Pavement HSG A				
81.24% Pervious Area				
18.76% Impervious Area				

Summary for Subcatchment EX 2: Brown Ave

Runoff = 0.71 cfs @ 12.17 hrs, Volume= 4,532 cf, Depth> 1.28"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 2.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

_	A	Area (sf)	CN	Description					
		21,553	30	,	Woods, Good, HSG A				
,		2,761	98	Bldg & Pav	ement, HS0	G A			
_		18,010	39	>75% Gras	s cover, Go	bod, HSG A			
		42,324	38	Weighted A	verage				
		39,563	34	93.48% Per	rvious Area	l			
		2,761	98	6.52% Impe	ervious Are	a			
	Tc	Length	Slope	e Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft		(cfs)	· ·			
_	8.9	50	0.1800	0.09		Sheet Flow,			
						Woods: Dense underbrush n= 0.800 P2= 3.20"			
	0.8	160	0.0500	3.35		Shallow Concentrated Flow,			
_						Grassed Waterway Kv= 15.0 fps			
-	97	210	Total						

9.7 210 Total

Summary for Subcatchment EX 3: Boyd Dr

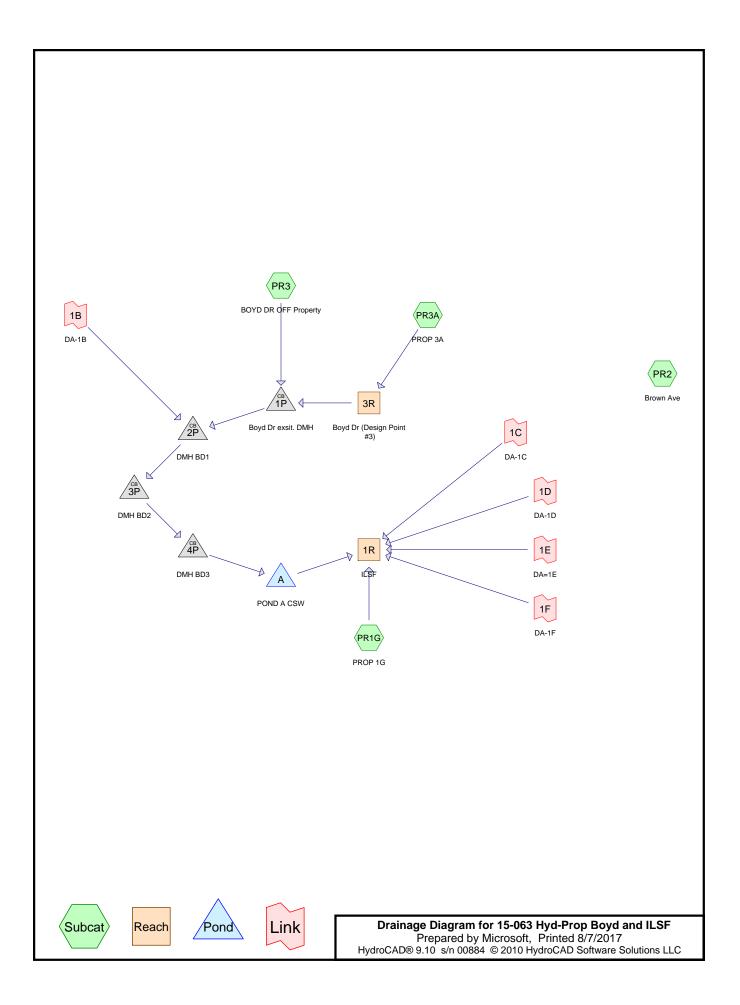
Runoff = 5.80 cfs @ 12.08 hrs, Volume= 20,937 cf, Depth> 6.51"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 2.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

Type III 24-hr 100 Year Rainfall=8.30" Printed 8/7/2017 Page 8

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	Area (sf)	CN	Description			
*	29,987	98	Bldg & Pavement, HSG A			
	8,585	39	>75% Grass cover, Good, HSG A			
	38,572	85	Weighted Average			
	8,585	39	22.26% Pervious Area			
	29,987	98	77.74% Impervious Area			
	Tc Length	Slop				
(min) (feet)	(ft/f	ft) (ft/sec) (cfs)			
	6.0		Direct Entry,			



15-063 Hyd-Prop Boyd and ILSF Prepared by Microsoft HydroCAD® 9.10 s/n 00884 © 2010 HydroCAD Software Solutions LLC

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Area Listing (all nodes)

Area	CN	Description	
(sq-ft)		(subcatchment-numbers)	
400,927	30	Meadow, non-grazed, HSG A (PR1G, PR2)	
256,844	30	Woods, Good, HSG A (PR1G, PR2, PR3)	
486,802	39	>75% Grass cover, Good, HSG A (PR1G, PR3, PR3A)	
18,183	76	Gravel roads, HSG A (PR1G)	
90,970	98	Bdg & Pavement HSG A (PR3)	
480	98	Bldg & Pavement, HSG A (PR2)	
13,358	98	Paved parking, HSG A (PR3A)	
53,303	98	Roofs, HSG A (PR1G, PR3, PR3A)	
278,856	98	Wetlands, HSG A (PR1G)	

Summary for Subcatchment PR1G: PROP 1G

Runoff = 20.08 cfs @ 12.08 hrs, Volume= 69,452 cf, Depth> 0.96"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

	Area (sf)	CN	Description		
*	278,856	98	Wetlands, HSG A		
	94,866	30	Woods, Good, HSG A		
	18,183	76	Gravel roads, HSG A		
	76,610	39	>75% Grass cover, Good, HSG A		
	383,703	30	Meadow, non-grazed, HSG A		
	11,985	98	Roofs, HSG A		
	864,203	55	Weighted Average		
	573,362	33	66.35% Pervious Area		
	290,841	98	33.65% Impervious Area		
To (min)		Slop (ft/			
6.0	/ (/		Direct Entry,		

Summary for Subcatchment PR2: Brown Ave

Runoff = 0.03 cfs @ 12.08 hrs, Volume= 115 cf, Depth> 0.04"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

	Area (sf)	CN	N Description			
	16,386	30	Woods, Go	od, HSG A		
*	480	98	Bldg & Pave	ement, HS	G A	
	17,224	30	Meadow, no	on-grazed,	HSG A	
	34,090	31	Weighted A	verage		
	33,610	30	98.59% Pei	vious Area	a	
	480	98	1.41% Impe	ervious Are	a	
Т	c Length	Slop	be Velocity	Capacity	Description	
(mir	n) (feet)	(ft/f	ft) (ft/sec)	(cfs)		
6.	.0				Direct Entry,	

Summary for Subcatchment PR3: BOYD DR OFF Property

Runoff = 7.15 cfs @ 12.16 hrs, Volume= 29,958 cf, Depth> 0.58"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10" 15-063 Hyd-Prop Boyd and ILSF

Type III 24-hr 2 Year Rainfall=3.10" Printed 8/7/2017 Page 4

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_	A	rea (sf)	CN E	Description		
	1	45,592	30 V	Voods, Go	od, HSG A	
*		90,970	98 E	3dg & Pave	ment HSG	A
	3	48,724	39 >	75% Gras	s cover, Go	ood, HSG A
_		34,597	98 F	Roofs, HSC	З А	
	6	19,883	49 V	Veighted A	verage	
	4	94,316	36 7	'9.74% Pei	vious Area	
	1	25,567	98 2	20.26% Imp	pervious Ar	ea
	_					
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	8.2	50	0.0200	0.10		Sheet Flow,
						Grass: Dense n= 0.240 P2= 3.20"
	2.7	140	0.1200	0.87		Shallow Concentrated Flow,
						Forest w/Heavy Litter Kv= 2.5 fps
	1.2	240	0.0500	3.35		Shallow Concentrated Flow,
_						Grassed Waterway Kv= 15.0 fps
	12.1	430	Total			

Summary for Subcatchment PR3A: PROP 3A

Runoff = 1.16 cfs @ 12.15 hrs, Volume= 4,791 cf, Depth> 0.70"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

_	A	rea (sf)	CN	Description		
		13,358	98	Paved park	ing, HSG A	N
		61,468	39	>75% Gras	s cover, Go	bod, HSG A
_		6,721	98	Roofs, HSC	θA	
		81,547	54	Weighted A	verage	
		61,468	39	75.38% Pe	rvious Area	
		20,079	98	24.62% Imp	pervious Ar	ea
_	Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description
	10.8	50	0.010	0.08		Sheet Flow,
						Grass: Dense n= 0.240 P2= 3.20"
	0.9	115	0.020	0 2.12		Shallow Concentrated Flow,
_						Grassed Waterway Kv= 15.0 fps
	11 7	165	Total			

11.7 165 Total

Summary for Reach 1R: ILSF

Inflow Are	a =	2,196,563 sf, 28.10% Impervious, Inflow Depth > 0.55" for 2 Year event	
Inflow	=	25.07 cfs @ 12.10 hrs, Volume= 101,157 cf	
Outflow	=	25.07 cfs @ 12.10 hrs, Volume= 101,157 cf, Atten= 0%, Lag= 0.0 min	n

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Reach 3R: Boyd Dr (Design Point #3)

Inflow Are	ea =	81,547 sf, 24.62% Impervious, Inflow Depth > 0.70" for 2 Year event	
Inflow	=	1.16 cfs @ 12.15 hrs, Volume= 4,791 cf	
Outflow	=	1.16 cfs @ 12.15 hrs, Volume= 4,791 cf, Atten= 0%, Lag= 0.0 m	nin

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Pond 1P: Boyd Dr exsit. DMH

Inflow Area	a =	701,430 sf, 20.76% Impervious, Inflow Depth > 0.59" for 2 Year event	
Inflow	=	8.31 cfs @ 12.16 hrs, Volume= 34,749 cf	
Outflow	=	8.31 cfs @ 12.16 hrs, Volume= 34,749 cf, Atten= 0%, Lag= 0.0 mi	n
Primary	=	8.31 cfs @ 12.16 hrs, Volume= 34,749 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 55.09' @ 12.16 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	53.60'	30.0" Round Culvert L= 110.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 53.60' / 53.26' S= 0.0031 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=8.30 cfs @ 12.16 hrs HW=55.09' (Free Discharge) 1=Culvert (Barrel Controls 8.30 cfs @ 3.90 fps)

Summary for Pond 2P: DMH BD1

Inflow Area	a =	811,786 sf	, 21.87% Impervious,	Inflow Depth > 0.56	for 2 Year event
Inflow	=	8.38 cfs @	12.16 hrs, Volume=	37,570 cf	
Outflow	=	8.38 cfs @	12.16 hrs, Volume=	37,570 cf, Att	en= 0%, Lag= 0.0 min
Primary	=	8.38 cfs @	12.16 hrs, Volume=	37,570 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 54.77' @ 12.16 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	53.26'	30.0" Round Culvert L= 84.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 53.26' / 53.00' S= 0.0031 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=8.38 cfs @ 12.16 hrs HW=54.77' (Free Discharge) 1=Culvert (Barrel Controls 8.38 cfs @ 3.87 fps)

Summary for Pond 3P: DMH BD2

 Inflow Area =
 811,786 sf, 21.87% Impervious, Inflow Depth > 0.56" for 2 Year event

 Inflow =
 8.38 cfs @ 12.16 hrs, Volume=
 37,570 cf

 Outflow =
 8.38 cfs @ 12.16 hrs, Volume=
 37,570 cf, Atten= 0%, Lag= 0.0 min

 Primary =
 8.38 cfs @ 12.16 hrs, Volume=
 37,570 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 54.38' @ 12.16 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	53.00'	36.0" Round Culvert L= 188.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 53.00' / 52.44' S= 0.0030 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=8.38 cfs @ 12.16 hrs HW=54.38' (Free Discharge) **1=Culvert** (Barrel Controls 8.38 cfs @ 3.89 fps)

Summary for Pond 4P: DMH BD3

Inflow Area	a =	811,786 sf, 21.87% Impervious, Inflow Depth > 0.56" for 2 Y	ear event
Inflow	=	8.38 cfs @ 12.16 hrs, Volume= 37,570 cf	
Outflow	=	8.38 cfs @ 12.16 hrs, Volume= 37,570 cf, Atten= 0%, I	_ag= 0.0 min
Primary	=	8.38 cfs @ 12.16 hrs, Volume= 37,570 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 53.79' @ 12.16 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	52.44'	36.0" Round Culvert L= 490.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 52.44' / 51.00' S= 0.0029 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=8.38 cfs @ 12.16 hrs HW=53.79' (Free Discharge)

Summary for Pond A: POND A CSW

Inflow Area	a =	811,786 sf, 21.87% Impervious	s, Inflow Depth > 0.56" for 2 Year event
Inflow	=	8.38 cfs @ 12.16 hrs, Volume	= 37,570 cf
Outflow	=	0.56 cfs @ 14.55 hrs, Volume:	= 13,683 cf, Atten= 93%, Lag= 143.3 min
Primary	=	0.56 cfs @ 14.55 hrs, Volume:	= 13,683 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 50.91' @ 14.55 hrs Surf.Area= 16,671 sf Storage= 27,400 cf

Plug-Flow detention time= 413.0 min calculated for 13,683 cf (36% of inflow) Center-of-Mass det. time= 259.8 min (1,026.0 - 766.2) 15-063 Hyd-Prop Boyd and ILSF Prepared by Microsoft HydroCAD® 9.10 s/n 00884 © 2010 HydroCAD Software Solutions LLC

Volume	Inv	ert Avail.St	orage	Storage	Description	
#1	49.0	00' 85,0	079 cf	STORM	WATER WETL	AND (Prismatic)Listed below (Recalc)
Elevatio		Surf.Area (sq-ft)	Inc. (cubic	Store -feet)	Cum.Store (cubic-feet)	
49.0	00	7,000		0	0	
49.5	50	14,335	Į	5,334	5,334	
50.0	00	15,550	-	7,471	12,805	
51.0	00	16,787	10	6,169	28,974	
52.0	00	18,050	1	7,419	46,392	
53.0	00	19,337	18	8,694	65,086	
54.0	00	20,649	19	9,993	85,079	
Device #1	Routing Primary	Invert 50.50	12.0 " L= 20 Inlet /	Outlet In	Culvert P, end-section c	onforming to fill, Ke= 0.500 50.30' S= 0.0100 '/' Cc= 0.900 ooth interior

Primary OutFlow Max=0.56 cfs @ 14.55 hrs HW=50.91' (Free Discharge) -1=Culvert (Barrel Controls 0.56 cfs @ 2.77 fps)

Summary for Link 1B: DA-1B

Inflow Area	a =	110,356 sf, 28.88% Impervious, Inflow Depth = 0.31" for 2	Year event
Inflow	=	0.53 cfs @ 12.51 hrs, Volume= 2,820 cf	
Primary	=	0.53 cfs @ 12.51 hrs, Volume= 2,820 cf, Atten= 0%,	Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

2 Year Outflow Imported from 15-063 Hyd-Prop DA-B1~Reach 1R.hce

Summary for Link 1C: DA-1C

Inflow Area	a =	52,998 sf, 53.94% Im	npervious,	Inflow Depth = 0.70	for 2 Year event
Inflow	=	1.49 cfs @ 12.19 hrs,	Volume=	3,111 cf	
Primary	=	1.49 cfs @ 12.19 hrs,	Volume=	3,111 cf, At	ten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

2 Year Outflow Imported from 15-063 Hyd-Prop DA-C1~Reach 1C.hce

Summary for Link 1D: DA-1D

Inflow Area	a =	162,115 sf, 2	29.46% Impervious,	Inflow Depth = 0.34 "	for 2 Year event
Inflow	=	2.41 cfs @ 1	2.20 hrs, Volume=	4,659 cf	
Primary	=	2.41 cfs @ 1	2.20 hrs, Volume=	4,659 cf, Atte	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

2 Year Outflow Imported from 15-063 Hyd-Prop DA-D1~Reach 1D.hce

Summary for Link 1E: DA=1E

Inflow Area =58,829 sf, 36.30% Impervious, Inflow Depth =0.81" for 2 Year eventInflow =1.74 cfs @12.15 hrs, Volume=3,995 cfPrimary =1.74 cfs @12.15 hrs, Volume=3,995 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

2 Year Outflow Imported from 15-063 Hyd-Prop DA-E1~Reach 1E.hce

Summary for Link 1F: DA-1F

Inflow Area	a =	246,632 sf, 20.73% Impervic	ous, Inflow Depth = 0.30 "	for 2 Year event
Inflow	=	2.51 cfs @ 12.14 hrs, Volum	e= 6,257 cf	
Primary	=	2.51 cfs @ 12.14 hrs, Volum	e= 6,257 cf, Atte	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

2 Year Outflow Imported from 15-063 Hyd-Prop DA-F1~Reach 1F.hce

Summary for Subcatchment PR1G: PROP 1G

Runoff = 30.68 cfs @ 12.08 hrs, Volume= 109,021 cf, Depth> 1.51"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

	Area (sf)	CN	Description				
*	278,856	98	Vetlands, HSG A				
	94,866	30	Woods, Good, HSG A				
	18,183	76	Gravel roads, HSG A				
	76,610	39	>75% Grass cover, Good, HSG A				
	383,703	30	Meadow, non-grazed, HSG A				
	11,985	98	Roofs, HSG A				
	864,203	55	Weighted Average				
	573,362	33	66.35% Pervious Area				
	290,841	98	33.65% Impervious Area				
To (min)		Slop (ft/i					
6.0)		Direct Entry,				

Summary for Subcatchment PR2: Brown Ave

Runoff = 0.05 cfs @ 12.08 hrs, Volume= 179 cf, Depth> 0.06"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

	Area (sf)	CN	Description	Description				
16,386 30 Woods, Good, HSG A					Α			
*	480	98	Bldg & Pave	Bldg & Pavement, HSG A				
	17,224	30	Meadow, no	on-grazed,	, HSG A			
	34,090	31	Weighted Average					
	33,610	30	98.59% Per	98.59% Pervious Area				
	480	98	1.41% Impervious Area					
- (mi	Гс Length n) (feet)	Slop (ft/i		Capacity (cfs)				
6	.0				Direct Entry,			

Summary for Subcatchment PR3: BOYD DR OFF Property

Runoff = 10.93 cfs @ 12.16 hrs, Volume= 49,446 cf, Depth> 0.96"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70" 15-063 Hyd-Prop Boyd and ILSF

Prepared by Microsoft

Type III 24-hr 10 Year Rainfall=4.70" Printed 8/7/2017 HydroCAD® 9.10 s/n 00884 © 2010 HydroCAD Software Solutions LLC Page 10

	А	rea (sf)	CN E	Description							
	1	45,592	30 V	Voods, Go	/oods, Good, HSG A						
*		90,970	98 E	Bdg & Pavement HSG A							
	3	48,724				ood, HSG A					
		34,597		Roofs, HSG							
619,883 49 Weighted Average											
	494,316 36			0	vious Area						
	125,567 98			20.26% Impervious Area							
	,										
	Тс	Length	Slope	Velocity	Capacity	Description					
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
-	8.2	50	0.0200	0.10	()	Sheet Flow,					
	0.2	00	0.0200	0.10		Grass: Dense n= 0.240 P2= 3.20"					
	2.7	140	0.1200	0.87		Shallow Concentrated Flow,					
	2.1	110	0.1200	0.07		Forest w/Heavy Litter Kv= 2.5 fps					
	1.2	240	0.0500	3.35		Shallow Concentrated Flow,					
		210	0.0000	0.00		Grassed Waterway Kv= 15.0 fps					
-	12.1	430	Total								
	12.1	430	rotar								

Summary for Subcatchment PR3A: PROP 3A

1.77 cfs @ 12.15 hrs, Volume= Runoff 8,186 cf, Depth> 1.20" =

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

_	A	rea (sf)	CN	Description		
		13,358	98	Paved park	ing, HSG A	
		61,468	39	>75% Gras	s cover, Go	bod, HSG A
_		6,721	98	Roofs, HSC	θA	
		81,547	54	Weighted A	verage	
		61,468	39	75.38% Pe	rvious Area	
		20,079	98	24.62% Imp	pervious Ar	ea
	Tc	Length	Slope		Capacity	Description
_	(min)	(feet)	(ft/ft		(cfs)	
	10.8	50	0.0100	0.08		Sheet Flow,
						Grass: Dense n= 0.240 P2= 3.20"
	0.9	115	0.0200) 2.12		Shallow Concentrated Flow,
_						Grassed Waterway Kv= 15.0 fps
	117	165	Total			

11.7 165 Total

Summary for Reach 1R: ILSF

Inflow Are	a =	2,196,563 sf, 28.10% Impervious, Inflow Depth > 1.04" for 10 Year ev	/ent
Inflow	=	42.26 cfs @ 12.09 hrs, Volume= 189,703 cf	
Outflow	=	42.26 cfs @ 12.09 hrs, Volume= 189,703 cf, Atten= 0%, Lag= 0.0) min

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Reach 3R: Boyd Dr (Design Point #3)

Inflow Area =		81,547 sf, 24.62% Impervious, Inflow Depth > 1.20" for 10 Year even	ent
Inflow	=	1.77 cfs @ 12.15 hrs, Volume= 8,186 cf	
Outflow	=	1.77 cfs @ 12.15 hrs, Volume= 8,186 cf, Atten= 0%, Lag= 0.0	min

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Pond 1P: Boyd Dr exsit. DMH

Inflow Area =		701,430 sf, 20.76% Impervious, Inflow Depth > 0.99" for 10 Year event
Inflow	=	12.69 cfs @ 12.16 hrs, Volume= 57,632 cf
Outflow	=	12.69 cfs @ 12.16 hrs, Volume= 57,632 cf, Atten= 0%, Lag= 0.0 min
Primary	=	12.69 cfs @ 12.16 hrs, Volume= 57,632 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 55.52' @ 12.16 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	53.60'	30.0" Round Culvert L= 110.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 53.60' / 53.26' S= 0.0031 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=12.69 cfs @ 12.16 hrs HW=55.52' (Free Discharge) -1=Culvert (Barrel Controls 12.69 cfs @ 4.33 fps)

Summary for Pond 2P: DMH BD1

Inflow Area =		811,786 sf, 21.87% Impervious, Inflow Depth > 0.96" for 10 Year eve	ent
Inflow	=	13.86 cfs @ 12.17 hrs, Volume= 65,020 cf	
Outflow	=	13.86 cfs @ 12.17 hrs, Volume= 65,020 cf, Atten= 0%, Lag= 0.0	min
Primary	=	13.86 cfs @ 12.17 hrs, Volume= 65,020 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 55.30' @ 12.17 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	53.26'	30.0" Round Culvert L= 84.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 53.26' / 53.00' S= 0.0031 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=13.85 cfs @ 12.17 hrs HW=55.30' (Free Discharge) -1=Culvert (Barrel Controls 13.85 cfs @ 4.40 fps)

Summary for Pond 3P: DMH BD2

Inflow Area =811,786 sf, 21.87% Impervious, Inflow Depth > 0.96" for 10 Year eventInflow =13.86 cfs @ 12.17 hrs, Volume=65,020 cfOutflow =13.86 cfs @ 12.17 hrs, Volume=65,020 cf, Atten= 0%, Lag= 0.0 minPrimary =13.86 cfs @ 12.17 hrs, Volume=65,020 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 54.83' @ 12.17 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	53.00'	36.0" Round Culvert L= 188.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 53.00' / 52.44' S= 0.0030 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=13.85 cfs @ 12.17 hrs HW=54.83' (Free Discharge) **1=Culvert** (Barrel Controls 13.85 cfs @ 4.40 fps)

Summary for Pond 4P: DMH BD3

Inflow Area =		811,786 sf, 21.87% Impervious, Inflow Depth > 0.96" for 10 Year event	
Inflow	=	13.86 cfs @ 12.17 hrs, Volume= 65,020 cf	
Outflow	=	13.86 cfs @ 12.17 hrs, Volume= 65,020 cf, Atten= 0%, Lag= 0.0 mi	in
Primary	=	13.86 cfs @ 12.17 hrs, Volume= 65,020 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 54.22' @ 12.17 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	52.44'	36.0" Round Culvert L= 490.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 52.44' / 51.00' S= 0.0029 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=13.85 cfs @ 12.17 hrs HW=54.22' (Free Discharge) **1=Culvert** (Barrel Controls 13.85 cfs @ 4.56 fps)

Summary for Pond A: POND A CSW

Inflow Area =		811,786 sf, 21.87% Impervious,	Inflow Depth > 0.96" for 10 Year event
Inflow	=	13.86 cfs @ 12.17 hrs, Volume=	65,020 cf
Outflow	=	2.36 cfs @ 12.87 hrs, Volume=	39,684 cf, Atten= 83%, Lag= 42.2 min
Primary	=	2.36 cfs @ 12.87 hrs, Volume=	39,684 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 51.49' @ 12.87 hrs Surf.Area= 17,400 sf Storage= 37,271 cf

Plug-Flow detention time= 295.6 min calculated for 39,667 cf (61% of inflow) Center-of-Mass det. time= 176.9 min (958.2 - 781.3) Prepared by Microsoft HydroCAD® 9.10 s/n 00884 © 2010 HydroCAD Software Solutions LLC Page 13 Volume Invert Avail.Storage Storage Description #1 49.00' 85,079 cf **STORM WATER WETLAND (Prismatic)**Listed below (Recalc) Surf.Area Cum.Store Elevation Inc.Store (feet) (cubic-feet) (sq-ft) (cubic-feet) 49.00 7.000 0 0 49.50 14,335 5,334 5,334 50.00 15,550 7,471 12,805 51.00 16,787 16,169 28,974 46.392 52.00 18.050 17,419 53.00 19,337 18,694 65,086 54.00 20.649 19,993 85.079

Device Routing Invert **Outlet Devices** Primarv 50.50' 12.0" Round Culvert #1 L= 20.0' CPP, end-section conforming to fill, Ke= 0.500 Inlet / Outlet Invert= 50.50' / 50.30' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=2.36 cfs @ 12.87 hrs HW=51.49' (Free Discharge) **1=Culvert** (Barrel Controls 2.36 cfs @ 3.80 fps)

Summary for Link 1B: DA-1B

Inflow Area = 110,356 sf, 28.88% Impervious, Inflow Depth > 0.80" for 10 Year event Inflow 1.53 cfs @ 12.32 hrs, Volume= 7,388 cf = Primarv = 1.53 cfs @ 12.32 hrs. Volume= 7,388 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

10 Year Outflow Imported from 15-063 Hyd-Prop DA-B1~Reach 1R.hce

Summary for Link 1C: DA-1C

Inflow Area = 52,998 sf, 53.94% Impervious, Inflow Depth = 1.55" for 10 Year event 2.46 cfs @ 12.17 hrs, Volume= Inflow 6,844 cf 6,844 cf, Atten= 0%, Lag= 0.0 min Primary 2.46 cfs @ 12.17 hrs, Volume= =

Primary outflow = Inflow, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

10 Year Outflow Imported from 15-063 Hyd-Prop DA-C1~Reach 1C.hce

Summary for Link 1D: DA-1D

162,115 sf, 29.46% Impervious, Inflow Depth > 0.86" Inflow Area = for 10 Year event Inflow 4.14 cfs @ 12.16 hrs, Volume= 11.643 cf = Primarv 4.14 cfs @ 12.16 hrs. Volume= 11,643 cf, Atten= 0%, Lag= 0.0 min =

Primary outflow = Inflow, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

10 Year Outflow Imported from 15-063 Hyd-Prop DA-D1~Reach 1D.hce

15-063 Hyd-Prop Boyd and ILSF

Type III 24-hr 10 Year Rainfall=4.70" Printed 8/7/2017

Summary for Link 1E: DA=1E

 Inflow Area =
 58,829 sf, 36.30% Impervious, Inflow Depth > 1.82" for 10 Year event

 Inflow =
 3.03 cfs @ 12.14 hrs, Volume=
 8,926 cf

 Primary =
 3.03 cfs @ 12.14 hrs, Volume=
 8,926 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

10 Year Outflow Imported from 15-063 Hyd-Prop DA-E1~Reach 1E.hce

Summary for Link 1F: DA-1F

Inflow Area =	246,632 sf, 20.73% Impervious,	Inflow Depth > 0.66"	for 10 Year event
Inflow =	3.90 cfs @ 12.13 hrs, Volume=	13,584 cf	
Primary =	3.90 cfs @ 12.13 hrs, Volume=	13,584 cf, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

10 Year Outflow Imported from 15-063 Hyd-Prop DA-F1~Reach 1F.hce

Summary for Subcatchment PR1G: PROP 1G

Runoff = 56.13 cfs @ 12.09 hrs, Volume= 229,974 cf, Depth> 3.19"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

	Area (sf)	CN	Description
*	278,856	98	Wetlands, HSG A
	94,866	30	Woods, Good, HSG A
	18,183	76	Gravel roads, HSG A
	76,610	39	>75% Grass cover, Good, HSG A
	383,703	30	Meadow, non-grazed, HSG A
	11,985	98	Roofs, HSG A
	864,203	55	Weighted Average
	573,362	33	66.35% Pervious Area
	290,841	98	33.65% Impervious Area
- (mi	Гс Length n) (feet)	Slop (ft/	
6	.0		Direct Entry,

Summary for Subcatchment PR2: Brown Ave

Runoff = 0.15 cfs @ 12.37 hrs, Volume= 1,689 cf, Depth> 0.59"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

	Area (sf)	CN	CN Description				
	16,386	6 30 Woods, Good, HSG A					
*	480	98	Bldg & Pave	ement, HS	IG A		
	17,224	30	Meadow, no	on-grazed,	HSG A		
	34,090	31	Weighted A	verage			
	33,610	30	98.59% Per	vious Area	a		
	480	98	1.41% Impe	ervious Are	ea		
	Tc Length in) (feet)	Slop (ft/f		Capacity (cfs)			
	5.0				Direct Entry,		

Summary for Subcatchment PR3: BOYD DR OFF Property

Runoff = 24.23 cfs @ 12.18 hrs, Volume= 125,138 cf, Depth> 2.42"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30" 15-063 Hyd-Prop Boyd and ILSF

Prepared by Microsoft

Type III 24-hr 100 Year Rainfall=8.30" Printed 8/7/2017 HydroCAD® 9.10 s/n 00884 © 2010 HydroCAD Software Solutions LLC Page 16

	А	rea (sf)	CN [Description		
	1	45,592	30 V	Voods, Go	od, HSG A	
*		90,970	98 E	3dg & Pave	ment HSG	A
	3	48,724	39 >	75% Gras	s cover, Go	bod, HSG A
		34,597		Roofs, HSG		,
	6	19,883	49 V	Veighted A	verage	
	4	94,316	36 7	'9.74% Per	vious Area	
		25,567	98 2	20.26% Imp	ervious Ar	ea
				•		
	Тс	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	•
	8.2	50	0.0200	0.10		Sheet Flow,
						Grass: Dense n= 0.240 P2= 3.20"
	2.7	140	0.1200	0.87		Shallow Concentrated Flow,
		-				Forest w/Heavy Litter Kv= 2.5 fps
	1.2	240	0.0500	3.35		Shallow Concentrated Flow,
						Grassed Waterway Kv= 15.0 fps
-	12.1	430	Total			

Summary for Subcatchment PR3A: PROP 3A

4.24 cfs @ 12.17 hrs, Volume= Runoff 20,015 cf, Depth> 2.95" =

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

_	A	rea (sf)	CN	Description		
		13,358	98	Paved park	ing, HSG A	N
		61,468	39	>75% Gras	s cover, Go	bod, HSG A
_		6,721	98	Roofs, HSC	ΞA	
		81,547	54	Weighted A	verage	
		61,468	39	75.38% Pe	rvious Area	
		20,079	98	24.62% Imp	pervious Ar	ea
_	Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description
	10.8	50	0.010	0.08		Sheet Flow,
						Grass: Dense n= 0.240 P2= 3.20"
	0.9	115	0.020	0 2.12		Shallow Concentrated Flow,
_						Grassed Waterway Kv= 15.0 fps
	11 7	165	Total			

11.7 165 Total

Summary for Reach 1R: ILSF

Inflow Are	a =	2,196,563 sf, 28.10% Impervious	, Inflow Depth > 2.67 "	for 100 Year event
Inflow	=	84.16 cfs @ 12.10 hrs, Volume=	488,348 cf	
Outflow	=	84.16 cfs @ 12.10 hrs, Volume=	488,348 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Reach 3R: Boyd Dr (Design Point #3)

Inflow Area	a =	81,547 sf	, 24.62% Impervious,	Inflow Depth >	2.95"	for 100 Year event
Inflow	=	4.24 cfs @	12.17 hrs, Volume=	20,015 c	f	
Outflow	=	4.24 cfs @	12.17 hrs, Volume=	20,015 c	f, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Pond 1P: Boyd Dr exsit. DMH

Inflow Are	a =	701,430 sf, 20.76% Impervious, Inflow Depth > 2.48" for 100 Year event	∩t
Inflow	=	28.46 cfs @ 12.18 hrs, Volume= 145,153 cf	
Outflow	=	28.46 cfs @ 12.18 hrs, Volume= 145,153 cf, Atten= 0%, Lag= 0.0 min	in
Primary	=	28.46 cfs @ 12.18 hrs, Volume= 145,153 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.28' @ 12.18 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	53.60'	30.0" Round Culvert L= 110.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $53.60' / 53.26'$ S= 0.0031 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=28.44 cfs @ 12.18 hrs HW=57.28' (Free Discharge) **1=Culvert** (Barrel Controls 28.44 cfs @ 5.79 fps)

Summary for Pond 2P: DMH BD1

Inflow Are	a =	811,786 sf, 21.87% Impervious, Inflow Depth > 2.50" for 100 Year event	t
Inflow	=	32.12 cfs @ 12.18 hrs, Volume= 168,913 cf	
Outflow	=	32.12 cfs @ 12.18 hrs, Volume= 168,913 cf, Atten= 0%, Lag= 0.0 min	۱
Primary	=	32.12 cfs @ 12.18 hrs, Volume= 168,913 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.47' @ 12.18 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	53.26'	30.0" Round Culvert L= 84.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 53.26' / 53.00' S= 0.0031 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=32.11 cfs @ 12.18 hrs HW=57.47' (Free Discharge) **1=Culvert** (Inlet Controls 32.11 cfs @ 6.54 fps)

Summary for Pond 3P: DMH BD2

 Inflow Area =
 811,786 sf, 21.87% Impervious, Inflow Depth > 2.50" for 100 Year event

 Inflow =
 32.12 cfs @ 12.18 hrs, Volume=
 168,913 cf

 Outflow =
 32.12 cfs @ 12.18 hrs, Volume=
 168,913 cf, Atten= 0%, Lag= 0.0 min

 Primary =
 32.12 cfs @ 12.18 hrs, Volume=
 168,913 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 56.13' @ 12.18 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	53.00'	36.0" Round Culvert L= 188.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 53.00' / 52.44' S= 0.0030 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=32.11 cfs @ 12.18 hrs HW=56.13' (Free Discharge) **1=Culvert** (Barrel Controls 32.11 cfs @ 5.41 fps)

Summary for Pond 4P: DMH BD3

Inflow Are	a =	811,786 sf, 21.87% Impervious, Inflow Depth > 2.50" for 100 Year event
Inflow	=	32.12 cfs @ 12.18 hrs, Volume= 168,913 cf
Outflow	=	32.12 cfs @ 12.18 hrs, Volume= 168,913 cf, Atten= 0%, Lag= 0.0 min
Primary	=	32.12 cfs @ 12.18 hrs, Volume= 168,913 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 55.51' @ 12.18 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	52.44'	36.0" Round Culvert L= 490.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 52.44' / 51.00' S= 0.0029 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=32.11 cfs @ 12.18 hrs HW=55.50' (Free Discharge) **1=Culvert** (Barrel Controls 32.11 cfs @ 5.52 fps)

Summary for Pond A: POND A CSW

Inflow Are	a =	811,786 sf, 21.87% Impervious	, Inflow Depth > 2.50" for 100 Year event
Inflow	=	32.12 cfs @ 12.18 hrs, Volume=	= 168,913 cf
Outflow	=	6.19 cfs @ 13.01 hrs, Volume=	= 139,723 cf, Atten= 81%, Lag= 49.7 min
Primary	=	6.19 cfs @ 13.01 hrs, Volume=	= 139,723 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 53.68' @ 13.01 hrs Surf.Area= 20,229 sf Storage= 78,540 cf

Plug-Flow detention time= 225.5 min calculated for 139,722 cf (83% of inflow) Center-of-Mass det. time= 148.6 min (958.6 - 810.0)

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Volume	Inv	ert Ava	ail.Storage	Storage [Description	
#1	49.	00'	85,079 cf	STORM	WATER WETL	AND (Prismatic)Listed below (Recalc)
Elevatio (fee		Surf.Area (sq-ft)		c.Store ic-feet)	Cum.Store (cubic-feet)	
49.0	00	7,000		0	0	
49.5	50	14,335		5,334	5,334	
50.0	00	15,550		7,471	12,805	
51.0	00	16,787		16,169	28,974	
52.0	00	18,050		17,419	46,392	
53.0	00	19,337		18,694	65,086	
54.0	00	20,649		19,993	85,079	
Device	Routing	Ir	nvert Out	let Devices		
#1	Primary	50	0.50' 12. 0)" Round	Culvert	
			L= :	20.0' CPP	, end-section c	onforming to fill, Ke= 0.500
			Inle	t / Outlet In	vert= 50.50' / 5	60.30' S= 0.0100 '/' Cc= 0.900
			n= (0.013 Corr	ugated PE, sm	ooth interior

Primary OutFlow Max=6.19 cfs @ 13.01 hrs HW=53.68' (Free Discharge) -1=Culvert (Inlet Controls 6.19 cfs @ 7.88 fps)

Summary for Link 1B: DA-1B

Inflow Area = 110,356 sf, 28.88% Impervious, Inflow Depth > 2.58" for 100 Year event 4.18 cfs @ 12.30 hrs, Volume= 23,760 cf Inflow = 4.18 cfs @ 12.30 hrs. Volume= Primarv = 23,760 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

100 Year Outflow Imported from 15-063 Hyd-Prop DA-B1~Reach 1R.hce

Summary for Link 1C: DA-1C

Inflow Area = 52,998 sf, 53.94% Impervious, Inflow Depth > 3.96" for 100 Year event 4.91 cfs @ 12.17 hrs, Volume= Inflow = 17,487 cf 4.91 cfs @ 12.17 hrs, Volume= Primary 17,487 cf, Atten= 0%, Lag= 0.0 min =

Primary outflow = Inflow, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

100 Year Outflow Imported from 15-063 Hyd-Prop DA-C1~Reach 1C.hce

Summary for Link 1D: DA-1D

162,115 sf, 29.46% Impervious, Inflow Depth > 2.69" for 100 Year event Inflow Area = Inflow 9.46 cfs @ 12.17 hrs, Volume= 36.376 cf = Primary 9.46 cfs @ 12.17 hrs. Volume= 36,376 cf, Atten= 0%, Lag= 0.0 min =

Primary outflow = Inflow, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

100 Year Outflow Imported from 15-063 Hyd-Prop DA-D1~Reach 1D.hce

Summary for Link 1E: DA=1E

 Inflow Area =
 58,829 sf, 36.30% Impervious, Inflow Depth > 4.51" for 100 Year event

 Inflow =
 6.48 cfs @ 12.14 hrs, Volume=
 22,103 cf

 Primary =
 6.48 cfs @ 12.14 hrs, Volume=
 22,103 cf, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

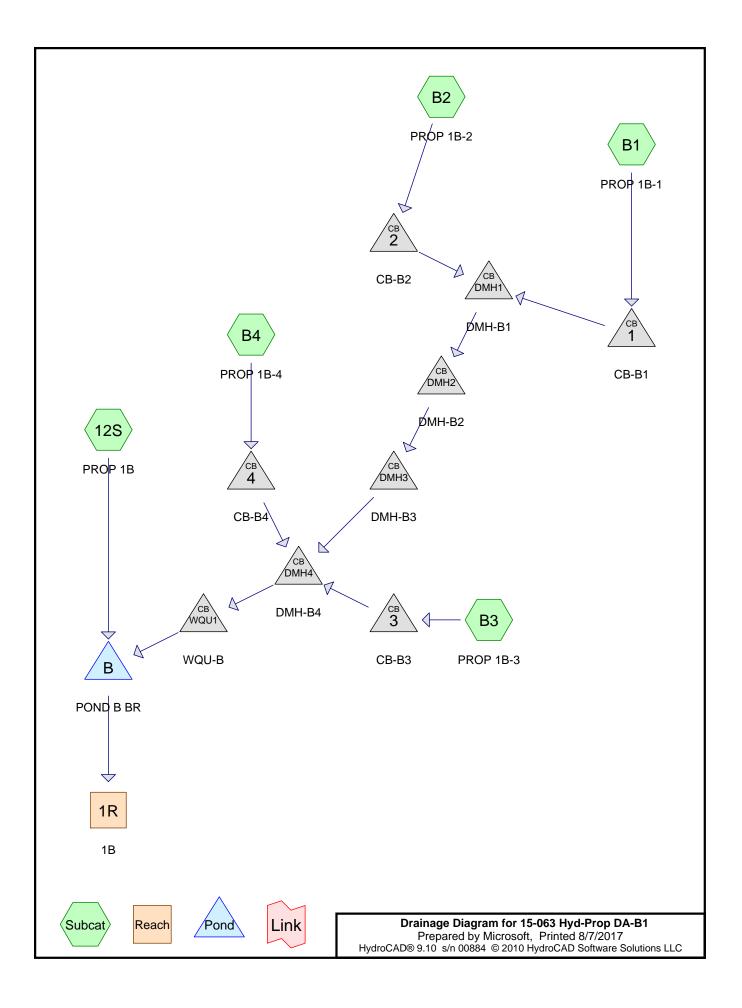
100 Year Outflow Imported from 15-063 Hyd-Prop DA-E1~Reach 1E.hce

Summary for Link 1F: DA-1F

Inflow Area =	246,632 sf, 20.73% Impervious,	Inflow Depth > 2.08"	for 100 Year event
Inflow =	7.94 cfs @ 12.14 hrs, Volume=	42,685 cf	
Primary =	7.94 cfs @ 12.14 hrs, Volume=	42,685 cf, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

100 Year Outflow Imported from 15-063 Hyd-Prop DA-F1~Reach 1F.hce



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Area Listing (all nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
78,484	39	>75% Grass cover, Good, HSG A (12S, B1, B3, B4)
21,565	98	Paved parking, HSG A (B1, B2, B3, B4)
10,307	98	Roofs, HSG A (12S, B1, B3)

Summary for Subcatchment 12S: PROP 1B

Runoff = 0.24 cfs @ 12.25 hrs, Volume= 1,192 cf, Depth> 0.35"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

_	A	rea (sf)	CN	Description		
		5,003	98	Roofs, HSG	βA	
_		35,416	39 :	>75% Gras	s cover, Go	bod, HSG A
	40,419 46 Weighted Average				verage	
		35,416	39	37.62% Pei	vious Area	
		5,003	98	12.38% Imp	pervious Ar	ea
	Тс	Length	Slope		Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	14.3	50	0.0050	0.06		Sheet Flow,
						Grass: Dense n= 0.240 P2= 3.20"
	4.7	300	0.0050	1.06		Shallow Concentrated Flow,
_						Grassed Waterway Kv= 15.0 fps
	10.0	250	Total			

19.0 350 Total

Summary for Subcatchment B1: PROP 1B-1

Runoff = 0.26 cfs @ 12.12 hrs, Volume= 979 cf, Depth> 1.37"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

A	rea (sf)	CN I	Description		
	3,006	98	Paved park	ing, HSG A	N Contraction of the second seco
	1,096	98	Roofs, HSG	βA	
	4,501	39 :	>75% Gras	s cover, Go	bod, HSG A
	8,603	67	Weighted A	verage	
	4,501	39	52.32% Pei	vious Area	l de la constante de
	4,102	98 4	47.68% Imp	pervious Ar	ea
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.2	50	0.0200	0.10		Sheet Flow,
					Grass: Dense n= 0.240 P2= 3.20"
0.8	100	0.0100	2.03		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
9.0	150	Total			

Summary for Subcatchment B2: PROP 1B-2

Runoff = 0.30 cfs @ 12.02 hrs, Volume= 880 cf, Depth> 2.87"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

_	A	rea (sf)	CN [Description		
_		3,683	98 F	Paved park	ing, HSG A	
		3,683	98 1	00.00% In	npervious A	rea
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	0.7	50	0.0200	1.20		Sheet Flow,
	1.0	120	0.0100	2.03		Smooth surfaces n= 0.011 P2= 3.20" Shallow Concentrated Flow, Paved Kv= 20.3 fps
	1.7	170	Total			

Summary for Subcatchment B3: PROP 1B-3

Runoff = 0.83 cfs @ 12.13 hrs, Volume= 3,246 cf, Depth> 1.56"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

_	A	rea (sf)	CN	Description		
		9,392	98	Paved park	ing, HSG A	N Contraction of the second seco
		11,405	39	>75% Gras	s cover, Go	bod, HSG A
_		4,208	98	Roofs, HSC	A 🛛	
		25,005	71	Weighted A	verage	
		11,405	39	45.61% Pe	rvious Area	l
		13,600	98	54.39% Imp	pervious Ar	ea
	_					
	Tc	Length	Slope		Capacity	Description
_	(min)	(feet)	(ft/ft	(ft/sec)	(cfs)	
	8.2	50	0.0200	0.10		Sheet Flow,
						Grass: Dense n= 0.240 P2= 3.20"
	1.5	177	0.0100	2.03		Shallow Concentrated Flow,
_						Paved Kv= 20.3 fps
	07	207	Total			

9.7 227 Total

Summary for Subcatchment B4: PROP 1B-4

Runoff = 0.34 cfs @ 12.13 hrs, Volume= 1,309 cf, Depth> 0.48"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

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Type III 24-hr 2 Year Rainfall=3.10" Printed 8/7/2017 Page 5

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_	A	rea (sf)	CN	Description		
		5,484	98	Paved park	ing, HSG A	ι
_		27,162	39	>75% Ġras	s cover, Go	bod, HSG A
		32,646	49	Weighted A	verage	
27,162 39 83.20% Pervious				83.20% Pei	vious Area	
		5,484	98	16.80% Imp	pervious Ar	ea
	Тс	Length	Slope		Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	8.2	50	0.0200	0.10		Sheet Flow,
						Grass: Dense n= 0.240 P2= 3.20"
	1.5	185	0.0100	2.03		Shallow Concentrated Flow,
_						Paved Kv= 20.3 fps
	~ 7	005	T ()			

9.7 235 Total

Summary for Reach 1R: 1B

Inflow Are	a =	110,356 sf, 28.88% Impervious	, Inflow Depth = 0.31 "	for 2 Year event
Inflow	=	0.53 cfs @ 12.51 hrs, Volume=	2,820 cf	
Outflow	=	0.53 cfs @ 12.51 hrs, Volume=	2,820 cf, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Pond 1: CB-B1

Inflow Area	a =	8,603 sf, 47.68% Impervious, Inflow Depth > 1.37" for 2 Year event
Inflow	=	0.26 cfs @ 12.12 hrs, Volume= 979 cf
Outflow	=	0.26 cfs @ 12.12 hrs, Volume= 979 cf, Atten= 0%, Lag= 0.0 min
Primary	=	0.26 cfs @ 12.12 hrs, Volume= 979 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 60.28' @ 12.12 hrs

#1 Primary 59.98' 12.0" Round Culvert L= 53.0' CPP, projecting, no headwall, Ke= 0.900	
Inlet / Outlet Invert= 59.98' / 59.72' S= 0.0049 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior	

Primary OutFlow Max=0.26 cfs @ 12.12 hrs HW=60.28' (Free Discharge) -1=Culvert (Barrel Controls 0.26 cfs @ 1.94 fps)

Summary for Pond 2: CB-B2

Inflow Area	I =	3,683 sf,	100.00% Impervious	, Inflow Depth > 2	.87" for 2 Year event
Inflow	=	0.30 cfs @	12.02 hrs, Volume=	880 cf	
Outflow	=	0.30 cfs @	12.02 hrs, Volume=	880 cf,	Atten= 0%, Lag= 0.0 min
Primary	=	0.30 cfs @	12.02 hrs, Volume=	880 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

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Peak Elev= 60.13' @ 12.02 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	59.82'	12.0" Round Culvert L= 8.5' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 59.82' / 59.72' S= 0.0118 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.29 cfs @ 12.02 hrs HW=60.13' (Free Discharge) 1=Culvert (Barrel Controls 0.29 cfs @ 2.14 fps)

Summary for Pond 3: CB-B3

Inflow Area	1 =	25,005 sf,	54.39% Impervious,	Inflow Depth > 1.56"	for 2 Year event
Inflow	=	0.83 cfs @	12.13 hrs, Volume=	3,246 cf	
Outflow	=	0.83 cfs @	12.13 hrs, Volume=	3,246 cf, Atte	en= 0%, Lag= 0.0 min
Primary	=	0.83 cfs @ 1	12.13 hrs, Volume=	3,246 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.26' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.70'	12.0" Round Culvert L= 8.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.70' / 57.60' S= 0.0125 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.83 cfs @ 12.13 hrs HW=58.26' (Free Discharge) ☐ 1=Culvert (Barrel Controls 0.83 cfs @ 2.65 fps)

Summary for Pond 4: CB-B4

Inflow Area	a =	32,646 sf,	16.80% Impervious,	Inflow Depth > 0	0.48" for 2 Year event
Inflow	=	0.34 cfs @ 1	12.13 hrs, Volume=	1,309 cf	
Outflow	=	0.34 cfs @ 1	12.13 hrs, Volume=	1,309 cf,	Atten= 0%, Lag= 0.0 min
Primary	=	0.34 cfs @ 1	12.13 hrs, Volume=	1,309 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.04' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.70'	12.0" Round Culvert L= 14.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.70' / 57.60' S= 0.0071 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.34 cfs @ 12.13 hrs HW=58.04' (Free Discharge) **1=Culvert** (Barrel Controls 0.34 cfs @ 2.08 fps)

Summary for Pond B: POND B BR

Inflow Area =	110,356 sf, 28.88% Impervious,	Inflow Depth > 0.83" for 2 Year event
Inflow =	1.74 cfs @ 12.13 hrs, Volume=	7,606 cf
Outflow =	0.58 cfs @ 12.51 hrs, Volume=	5,546 cf, Atten= 67%, Lag= 23.0 min
Discarded =	0.04 cfs @ 12.51 hrs, Volume=	2,725 cf
Primary =	0.53 cfs @ 12.51 hrs, Volume=	2,820 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 56.99' @ 12.51 hrs Surf.Area= 3,665 sf Storage= 3,432 cf

Plug-Flow detention time= 180.6 min calculated for 5,544 cf (73% of inflow) Center-of-Mass det. time= 92.2 min (852.1 - 759.9)

Volume	Invert	Avail.Stor	age Storage I	Description			
#1	55.95'	7,29	6 cf BioRente	ention Area (P	rismatic)Listed below (Recalc)		
Elevatio		ırf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)			
55.9	95	2,930	0	0			
56.9	95	3,633	3,282	3,282			
57.9	95	4,396	4,015	7,296			
Device	Routing	Invert	Outlet Devices	i			
#1	Discarded	55.95'	0.520 in/hr Ex	filtration over	Surface area		
#2	Primary	56.65'	18.0" Round	Culvert			
	-		L= 74.0' CPP	, mitered to cor	nform to fill, Ke= 0.700		
			Inlet / Outlet In	vert= 56.65' / 5	54.06' S= 0.0350 '/' Cc= 0.900		
			n= 0.013 Corr	ugated PE, sm	ooth interior		
Discard	Discarded OutFlow Max=0.04 cfs @ 12.51 hrs HW=56.99' (Free Discharge)						

1=Exfiltration (Exfiltration Controls 0.04 cfs)

Primary OutFlow Max=0.53 cfs @ 12.51 hrs HW=56.99' (Free Discharge) 2=Culvert (Inlet Controls 0.53 cfs @ 1.76 fps)

Summary for Pond DMH1: DMH-B1

Inflow Area	ι =	12,286 sf,	63.36% Impervious,	Inflow Depth > 1.82"	for 2 Year event
Inflow	=	0.47 cfs @	12.04 hrs, Volume=	1,859 cf	
Outflow	=	0.47 cfs @	12.04 hrs, Volume=	1,859 cf, Atte	n= 0%, Lag= 0.0 min
Primary	=	0.47 cfs @	12.04 hrs, Volume=	1,859 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 60.01' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	59.62'	12.0" Round Culvert
			L= 105.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 59.62' / 58.89' S= 0.0070 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.47 cfs @ 12.04 hrs HW=60.01' (Free Discharge) **1=Culvert** (Inlet Controls 0.47 cfs @ 1.67 fps)

Summary for Pond DMH2: DMH-B2

Inflow Area	a =	12,286 sf, 63.36% Impervious, Inflow Depth > 1.82" for 2 Year event	
Inflow	=	0.47 cfs @ 12.04 hrs, Volume= 1,859 cf	
Outflow	=	0.47 cfs @ 12.04 hrs, Volume= 1,859 cf, Atten= 0%, Lag= 0.0 m	nin
Primary	=	0.47 cfs @ 12.04 hrs, Volume= 1,859 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 59.18' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices
	Primary	58.79'	12.0" Round Culvert L= 96.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 58.79' / 58.03' S= 0.0079 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.47 cfs @ 12.04 hrs HW=59.18' (Free Discharge) -1=Culvert (Inlet Controls 0.47 cfs @ 1.67 fps)

Summary for Pond DMH3: DMH-B3

Inflow Area	a =	12,286 sf, 63.36% Impervious,	Inflow Depth > 1.82" for 2 Year event
Inflow	=	0.47 cfs @ 12.04 hrs, Volume=	1,859 cf
Outflow	=	0.47 cfs @ 12.04 hrs, Volume=	1,859 cf, Atten= 0%, Lag= 0.0 min
Primary	=	0.47 cfs @ 12.04 hrs, Volume=	1,859 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.32' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.93'	12.0" Round Culvert L= 43.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.93' / 57.60' S= 0.0077 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.47 cfs @ 12.04 hrs HW=58.32' (Free Discharge) -1=Culvert (Inlet Controls 0.47 cfs @ 1.67 fps)

Summary for Pond DMH4: DMH-B4

Inflow Area :	=	69,937 sf	, 38.42% Impervious,	Inflow Depth > 1.10"	for 2 Year event
Inflow =	=	1.56 cfs @	12.12 hrs, Volume=	6,414 cf	
Outflow =	=	1.56 cfs @	12.12 hrs, Volume=	6,414 cf, Atte	n= 0%, Lag= 0.0 min
Primary =	=	1.56 cfs @	12.12 hrs, Volume=	6,414 cf	-

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Peak Elev= 58.20' @ 12.12 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.50'	18.0" Round Culvert L= 31.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.50' / 57.34' S= 0.0052 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.56 cfs @ 12.12 hrs HW=58.20' (Free Discharge) **1=Culvert** (Barrel Controls 1.56 cfs @ 2.83 fps)

Summary for Pond WQU1: WQU-B

Inflow Area	a =	69,937 sf, 38.42% Impervious, Inflow Depth > 1.10" for 2 Year	event
Inflow	=	1.56 cfs @ 12.12 hrs, Volume= 6,414 cf	
Outflow	=	1.56 cfs @ 12.12 hrs, Volume= 6,414 cf, Atten= 0%, Lag=	= 0.0 min
Primary	=	1.56 cfs @ 12.12 hrs, Volume= 6,414 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.98' @ 12.12 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.34'	18.0" Round Culvert L= 115.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.34' / 56.70' S= 0.0056 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.56 cfs @ 12.12 hrs HW=57.98' (Free Discharge) **1=Culvert** (Barrel Controls 1.56 cfs @ 3.17 fps)

Summary for Subcatchment 12S: PROP 1B

Runoff = 0.37 cfs @ 12.25 hrs, Volume= 2,274 cf, Depth> 0.68"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

_	A	rea (sf)	CN	Description		
		5,003	98	Roofs, HSG	βA	
_		35,416	39	>75% Gras	s cover, Go	bod, HSG A
40,419 46 Weighted Average						
		35,416	39	87.62% Per	vious Area	
5,003 98 12.38% Impervious Area				12.38% Imp	pervious Ar	ea
	_					
	Tc	Length	Slope		Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	14.3	50	0.0050	0.06		Sheet Flow,
						Grass: Dense n= 0.240 P2= 3.20"
	4.7	300	0.0050	1.06		Shallow Concentrated Flow,
_						Grassed Waterway Kv= 15.0 fps
	10.0	250	Total			

19.0 350 Total

Summary for Subcatchment B1: PROP 1B-1

Runoff = 0.39 cfs @ 12.12 hrs, Volume= 1,577 cf, Depth> 2.20"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

A	rea (sf)	CN I	Description						
	3,006	98	Paved park	ing, HSG A	N Contraction of the second seco				
	1,096	98	Roofs, HSG	βA					
	4,501	39 :	>75% Gras	>75% Grass cover, Good, HSG A					
	8,603	67	Weighted A	verage					
	4,501	39	52.32% Pei	vious Area	l de la constante de				
	4,102	98 4	47.68% Imp	pervious Ar	ea				
Тс	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
8.2	50	0.0200	0.10		Sheet Flow,				
					Grass: Dense n= 0.240 P2= 3.20"				
0.8	100	0.0100	2.03		Shallow Concentrated Flow,				
					Paved Kv= 20.3 fps				
9.0	150	Total							

Summary for Subcatchment B2: PROP 1B-2

Runoff = 0.45 cfs @ 12.02 hrs, Volume= 1,370 cf, Depth> 4.46"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

_	A	rea (sf)	CN [Description					
_	3,683 98 Paved parking, HSG A								
		3,683	98 1	98 100.00% Impervious Area					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
_	0.7	50	0.0200	1.20		Sheet Flow,			
	1.0	120	0.0100	2.03		Smooth surfaces n= 0.011 P2= 3.20" Shallow Concentrated Flow, Paved Kv= 20.3 fps			
	1.7	170	Total						

Summary for Subcatchment B3: PROP 1B-3

Runoff = 1.27 cfs @ 12.13 hrs, Volume= 5,188 cf, Depth> 2.49"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

_	A	rea (sf)	CN	N Description						
		9,392	98	Paved parking, HSG A						
		11,405	39	>75% Gras	s cover, Go	bod, HSG A				
_		4,208	98	Roofs, HSG A						
		25,005	71	1 Weighted Average						
		11,405	39	45.61% Pe	rvious Area	l				
		13,600	98	54.39% Imp	pervious Ar	ea				
	_									
	Tc	Length	Slope		Capacity	Description				
_	(min)	(feet)	(ft/ft	(ft/sec)	(cfs)					
	8.2	50	0.0200	0.10		Sheet Flow,				
						Grass: Dense n= 0.240 P2= 3.20"				
	1.5	177	0.0100	2.03		Shallow Concentrated Flow,				
_						Paved Kv= 20.3 fps				
	07	207	Total							

9.7 227 Total

Summary for Subcatchment B4: PROP 1B-4

Runoff = 0.51 cfs @ 12.13 hrs, Volume= 2,360 cf, Depth> 0.87"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70" 15-063 Hyd-Prop DA-B1

 Type III 24-hr 10 Year Rainfall=4.70"

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_	A	rea (sf)	CN	Description	Description						
		5,484	98	Paved park	king, HSG A	A Contraction of the second se					
_		27,162	39	>75% Gras	s cover, Go	bod, HSG A					
		32,646	49	Weighted A	Average						
		27,162	39	83.20% Pe	rvious Area	l					
		5,484	98	16.80% lm	pervious Ar	ea					
	Tc (min)	Length (feet)	Slop (ft/f		Capacity (cfs)	Description					
	8.2	50	0.020	0.10		Sheet Flow,					
	1.5	185	0.010	0 2.03		Grass: Dense n= 0.240 P2= 3.20" Shallow Concentrated Flow, Paved Kv= 20.3 fps					
	07	005	T . (.)								

9.7 235 Total

Summary for Reach 1R: 1B

Inflow Area	a =	110,356 sf, 28.88% Impervious, In	nflow Depth > 0.80"	for 10 Year event
Inflow	=	1.53 cfs @ 12.32 hrs, Volume=	7,388 cf	
Outflow	=	1.53 cfs @ 12.32 hrs, Volume=	7,388 cf, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Pond 1: CB-B1

Inflow Area =	8,603 sf, 47.68% Impervious,	Inflow Depth > 2.20" for 10 Year event
Inflow =	0.39 cfs @ 12.12 hrs, Volume=	1,577 cf
Outflow =	0.39 cfs @ 12.12 hrs, Volume=	1,577 cf, Atten= 0%, Lag= 0.0 min
Primary =	0.39 cfs @ 12.12 hrs, Volume=	1,577 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 60.35' @ 12.12 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary		12.0" Round Culvert L= 53.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 59.98' / 59.72' S= 0.0049 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.39 cfs @ 12.12 hrs HW=60.35' (Free Discharge) -1=Culvert (Barrel Controls 0.39 cfs @ 2.16 fps)

Summary for Pond 2: CB-B2

Inflow Are	a =	3,683 sf,100.00% Impervious, Inflow Depth > 4.46" for 10 Year event	
Inflow	=	0.45 cfs @ 12.02 hrs, Volume= 1,370 cf	
Outflow	=	0.45 cfs @ 12.02 hrs, Volume= 1,370 cf, Atten= 0%, Lag= 0.0 min	l
Primary	=	0.45 cfs @ 12.02 hrs, Volume= 1,370 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

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Peak Elev= 60.21' @ 12.02 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	59.82'	12.0" Round Culvert L= 8.5' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 59.82' / 59.72' S= 0.0118 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.45 cfs @ 12.02 hrs HW=60.21' (Free Discharge) **1=Culvert** (Barrel Controls 0.45 cfs @ 2.33 fps)

Summary for Pond 3: CB-B3

Inflow Area	a =	25,005 sf,	54.39% Impervious,	Inflow Depth > 2.49"	for 10 Year event
Inflow	=	1.27 cfs @	12.13 hrs, Volume=	5,188 cf	
Outflow	=	1.27 cfs @	12.13 hrs, Volume=	5,188 cf, Atte	n= 0%, Lag= 0.0 min
Primary	=	1.27 cfs @	12.13 hrs, Volume=	5,188 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.42' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.70'	12.0" Round Culvert L= 8.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.70' / 57.60' S= 0.0125 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.27 cfs @ 12.13 hrs HW=58.42' (Free Discharge) **1=Culvert** (Barrel Controls 1.27 cfs @ 2.91 fps)

Summary for Pond 4: CB-B4

Inflow Area	a =	32,646 sf, 16.80% Impervious, Inflow Depth > 0.87" for 10 Year ever	nt
Inflow	=	0.51 cfs @ 12.13 hrs, Volume= 2,360 cf	
Outflow	=	0.51 cfs @ 12.13 hrs, Volume= 2,360 cf, Atten= 0%, Lag= 0.0 r	min
Primary	=	0.51 cfs @ 12.13 hrs, Volume= 2,360 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.14' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.70'	12.0" Round Culvert L= 14.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.70' / 57.60' S= 0.0071 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.51 cfs @ 12.13 hrs HW=58.14' (Free Discharge) **1=Culvert** (Barrel Controls 0.51 cfs @ 2.29 fps)

Summary for Pond B: POND B BR

Inflow Area =	110,356 sf, 28.88% Impervious,	Inflow Depth > 1.39" for 10 Year event
Inflow =	2.66 cfs @ 12.13 hrs, Volume=	12,768 cf
Outflow =	1.58 cfs @ 12.32 hrs, Volume=	10,389 cf, Atten= 41%, Lag= 11.5 min
Discarded =	0.05 cfs @ 12.32 hrs, Volume=	3,000 cf
Primary =	1.53 cfs @ 12.32 hrs, Volume=	7,388 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.25' @ 12.32 hrs Surf.Area= 3,861 sf Storage= 4,400 cf

Plug-Flow detention time= 144.8 min calculated for 10,389 cf (81% of inflow) Center-of-Mass det. time= 64.4 min (837.1 - 772.7)

Volume	Invert	Avail.Stor	age Storage D	escription		
#1	55.95'	7,29	6 cf BioRente	ntion Area (P	rismatic)Listed below (Recalc)	
Elevatic (fee 55.9 56.9 57.9	et) 95 95	ırf.Area (sq-ft) 2,930 3,633 4,396	Inc.Store (cubic-feet) 0 3,282 4,015	Cum.Store (cubic-feet) 0 3,282 7,296		
Device	Routing	Invert	Outlet Devices			
#1	Discarded	55.95'	0.520 in/hr Exf	iltration over	Surface area	
#2	Primary	56.65'	18.0" Round (
					nform to fill, Ke= 0.700	
					4.06' S= 0.0350 '/' Cc= 0.900	
			n= 0.013 Corru	ugated PE, sm	ooth interior	
Discord	Disported OutFlow: Mox-0.05 of a @ 12.22 hrs. HW/-57.25' (Free Disphered)					

Discarded OutFlow Max=0.05 cfs @ 12.32 hrs HW=57.25' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.05 cfs)

Primary OutFlow Max=1.53 cfs @ 12.32 hrs HW=57.25' (Free Discharge) 2=Culvert (Inlet Controls 1.53 cfs @ 2.32 fps)

Summary for Pond DMH1: DMH-B1

Inflow Area	=	12,286 sf	, 63.36% Impervious,	Inflow Depth > 2.88"	for 10 Year event
Inflow	=	0.71 cfs @	12.04 hrs, Volume=	2,947 cf	
Outflow	=	0.71 cfs @	12.04 hrs, Volume=	2,947 cf, Atte	en= 0%, Lag= 0.0 min
Primary	=	0.71 cfs @	12.04 hrs, Volume=	2,947 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 60.11' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices	
#1	Primary	59.62'	12.0" Round Culvert	
	-		L= 105.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 59.62' / 58.89' S= 0.0070 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior	

Primary OutFlow Max=0.71 cfs @ 12.04 hrs HW=60.11' (Free Discharge) **1=Culvert** (Inlet Controls 0.71 cfs @ 1.88 fps)

Summary for Pond DMH2: DMH-B2

Inflow Area	a =	12,286 sf, 63.36% Impervious, Inflow Depth > 2.88" for 10 Year event	t
Inflow	=	0.71 cfs @ 12.04 hrs, Volume= 2,947 cf	
Outflow	=	0.71 cfs @ 12.04 hrs, Volume= 2,947 cf, Atten= 0%, Lag= 0.0 m	nin
Primary	=	0.71 cfs @ 12.04 hrs, Volume= 2,947 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 59.28' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices
	Primary	58.79'	12.0" Round Culvert L= 96.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 58.79' / 58.03' S= 0.0079 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.71 cfs @ 12.04 hrs HW=59.28' (Free Discharge) -1=Culvert (Inlet Controls 0.71 cfs @ 1.88 fps)

Summary for Pond DMH3: DMH-B3

Inflow Are	a =	12,286 sf, 63.36% Impervious, Inflow Depth > 2.88" for 10 Year event	
Inflow	=	0.71 cfs @ 12.04 hrs, Volume= 2,947 cf	
Outflow	=	0.71 cfs @ 12.04 hrs, Volume= 2,947 cf, Atten= 0%, Lag= 0.0 mir	n
Primary	=	0.71 cfs @ 12.04 hrs, Volume= 2,947 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.42' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.93'	12.0" Round Culvert L= 43.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.93' / 57.60' S= 0.0077 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.71 cfs @ 12.04 hrs HW=58.42' (Free Discharge) **1=Culvert** (Inlet Controls 0.71 cfs @ 1.88 fps)

Summary for Pond DMH4: DMH-B4

Inflow Area =	69,937 sf, 38.42% Impervious,	Inflow Depth > 1.80" for 10 Year event
Inflow =	2.38 cfs @ 12.12 hrs, Volume=	10,495 cf
Outflow =	2.38 cfs @ 12.12 hrs, Volume=	10,495 cf, Atten= 0%, Lag= 0.0 min
Primary =	2.38 cfs @ 12.12 hrs, Volume=	10,495 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Peak Elev= 58.39' @ 12.12 hrs

Device	Routing	Invert	Outlet Devices
	Primary	57.50'	18.0" Round Culvert L= 31.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.50' / 57.34' S= 0.0052 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=2.38 cfs @ 12.12 hrs HW=58.39' (Free Discharge) -1=Culvert (Barrel Controls 2.38 cfs @ 3.12 fps)

Summary for Pond WQU1: WQU-B

Inflow Area	ı =	69,937 sf	, 38.42% Impervious,	Inflow Depth > 1.80	0" for 10 Year event
Inflow	=	2.38 cfs @	12.12 hrs, Volume=	10,495 cf	
Outflow	=	2.38 cfs @	12.12 hrs, Volume=	10,495 cf, At	tten= 0%, Lag= 0.0 min
Primary	=	2.38 cfs @	12.12 hrs, Volume=	10,495 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.16' @ 12.12 hrs

Device	Routing	Invert	Outlet Devices		
#1	Primary	57.34'	18.0" Round Culvert L= 115.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.34' / 56.70' S= 0.0056 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior		

Primary OutFlow Max=2.38 cfs @ 12.12 hrs HW=58.16' (Free Discharge) -1=Culvert (Barrel Controls 2.38 cfs @ 3.50 fps)

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Summary for Subcatchment 12S: PROP 1B

Runoff = 1.20 cfs @ 12.30 hrs, Volume= 7,117 cf, Depth> 2.11"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

_	A	rea (sf)	CN	CN Description				
		5,003	98	Roofs, HSG	β A			
_		35,416	39	>75% Gras	s cover, Go	bod, HSG A		
		40,419	46	Weighted A	verage			
35,416 39 87.62% Pervious Area					l			
		5,003	98 12.38% Impervious Area			ea		
	_							
	Tc	Length	Slope		Capacity	Description		
_	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)			
	14.3	50	0.0050	0.06		Sheet Flow,		
						Grass: Dense n= 0.240 P2= 3.20"		
	4.7	300	0.0050) 1.06		Shallow Concentrated Flow,		
_						Grassed Waterway Kv= 15.0 fps		
	10.0	250	Tatal					

19.0 350 Total

Summary for Subcatchment B1: PROP 1B-1

Runoff = 0.78 cfs @ 12.13 hrs, Volume= 3,231 cf, Depth> 4.51"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

A	rea (sf)	CN I	Description		
	3,006	98 I	Paved park	ing, HSG A	N
	1,096	98 I	Roofs, HSG	βA	
	4,501	39 >	>75% Gras	s cover, Go	bod, HSG A
	8,603	67 \	Neighted A	verage	
	4,501	39 క	52.32% Pei	vious Area	l
	4,102	98 4	17.68% Imp	pervious Ar	ea
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.2	50	0.0200	0.10		Sheet Flow,
					Grass: Dense n= 0.240 P2= 3.20"
0.8	100	0.0100	2.03		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
9.0	150	Total			

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Summary for Subcatchment B2: PROP 1B-2

Runoff = 0.80 cfs @ 12.02 hrs, Volume= 2,471 cf, Depth> 8.05"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

A	vrea (sf)	CN E	Description					
	3,683	98 F	aved park	ing, HSG A				
	3,683	98 1	100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
0.7	50	0.0200	1.20	· · ·	Sheet Flow,			
1.0	120	0.0100	2.03		Smooth surfaces n= 0.011 P2= 3.20" Shallow Concentrated Flow, Paved Kv= 20.3 fps			
1.7	170	Total						

Summary for Subcatchment B3: PROP 1B-3

Runoff = 2.47 cfs @ 12.13 hrs, Volume= 10,336 cf, Depth> 4.96"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

_	A	rea (sf)	CN Description				
		9,392	98 Paved parking, HSG A				
		11,405	39 :	39 >75% Grass cover, Good, HSG A			
4,208 98 Roofs, HSG A							
25,005 71 Weighted Average							
11,405 39 45.61% Pervious Area					l		
13,600 98 54.39% Impervious Area					ea		
	Тс	Length	Slope	Velocity	Capacity	Description	
_	(min)	(feet)	(ft/ft)		(cfs)		
	8.2	50	0.0200	0.10		Sheet Flow,	
						Grass: Dense n= 0.240 P2= 3.20"	
	1.5	177	0.0100	2.03		Shallow Concentrated Flow,	
_						Paved Kv= 20.3 fps	
	07	207	Total				

9.7 227 Total

Summary for Subcatchment B4: PROP 1B-4

Runoff = 1.44 cfs @ 12.15 hrs, Volume= 6,576 cf, Depth> 2.42"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30" 15-063 Hyd-Prop DA-B1

Type III 24-hr 100 Year Rainfall=8.30" Printed 8/7/2017 LC Page 19

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_	A	rea (sf)	CN	Description		
		5,484	98	Paved park	l.	
_		27,162	39	>75% Ġras	s cover, Go	bod, HSG A
		32,646	49	Weighted A	verage	
	27,162 39 83.20% Pervious Area			83.20% Pe	vious Area	
		5,484	98	16.80% Imp	pervious Ar	ea
	Тс	Length	Slope		Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	8.2	50	0.0200	0.10		Sheet Flow,
						Grass: Dense n= 0.240 P2= 3.20"
	1.5	185	0.0100	2.03		Shallow Concentrated Flow,
_						Paved Kv= 20.3 fps
	07	005	Tatal			

9.7 235 Total

Summary for Reach 1R: 1B

Inflow Are	a =	110,356 sf, 28.88% Impervious,	Inflow Depth > 2.58"	for 100 Year event
Inflow	=	4.18 cfs @ 12.30 hrs, Volume=	23,760 cf	
Outflow	=	4.18 cfs @ 12.30 hrs, Volume=	23,760 cf, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Pond 1: CB-B1

Inflow Area =	8,603 sf, 47.68% Impervious,	Inflow Depth > 4.51" for 100 Year event
Inflow =	0.78 cfs @ 12.13 hrs, Volume=	3,231 cf
Outflow =	0.78 cfs @ 12.13 hrs, Volume=	3,231 cf, Atten= 0%, Lag= 0.0 min
Primary =	0.78 cfs @ 12.13 hrs, Volume=	3,231 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 60.53' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
-	Primary		12.0" Round Culvert L= 53.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 59.98' / 59.72' S= 0.0049 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior
			n= 0.013 Confugated PE, smooth Interior

Primary OutFlow Max=0.78 cfs @ 12.13 hrs HW=60.53' (Free Discharge) -1=Culvert (Barrel Controls 0.78 cfs @ 2.57 fps)

Summary for Pond 2: CB-B2

Inflow Area	a =	3,683 sf,100.00% Impervious, Inflow Depth > 8.05" for 100 Year event	t
Inflow	=	0.80 cfs @ 12.02 hrs, Volume= 2,471 cf	
Outflow	=	0.80 cfs @ 12.02 hrs, Volume= 2,471 cf, Atten= 0%, Lag= 0.0 min	n
Primary	=	0.80 cfs @ 12.02 hrs, Volume= 2,471 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Prepared by Microsoft

Peak Elev= 60.37' @ 12.02 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	59.82'	12.0" Round Culvert L= 8.5' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 59.82' / 59.72' S= 0.0118 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.80 cfs @ 12.02 hrs HW=60.37' (Free Discharge) **1=Culvert** (Barrel Controls 0.80 cfs @ 2.62 fps)

Summary for Pond 3: CB-B3

Inflow Area	ı =	25,005 sf,	54.39% Impervious,	Inflow Depth > 4.96	for 100 Year event
Inflow	=	2.47 cfs @	12.13 hrs, Volume=	10,336 cf	
Outflow	=	2.47 cfs @	12.13 hrs, Volume=	10,336 cf, Atte	en= 0%, Lag= 0.0 min
Primary	=	2.47 cfs @	12.13 hrs, Volume=	10,336 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.88' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.70'	12.0" Round Culvert L= 8.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.70' / 57.60' S= 0.0125 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=2.47 cfs @ 12.13 hrs HW=58.88' (Free Discharge) **1=Culvert** (Inlet Controls 2.47 cfs @ 3.14 fps)

Summary for Pond 4: CB-B4

Inflow Area	a =	32,646 sf,	16.80% Impervious,	Inflow Depth > 2	2.42" for 100 Year event
Inflow	=	1.44 cfs @	12.15 hrs, Volume=	6,576 cf	
Outflow	=	1.44 cfs @	12.15 hrs, Volume=	6,576 cf,	Atten= 0%, Lag= 0.0 min
Primary	=	1.44 cfs @	12.15 hrs, Volume=	6,576 cf	-

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.50' @ 12.15 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.70'	12.0" Round Culvert L= 14.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.70' / 57.60' S= 0.0071 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.44 cfs @ 12.15 hrs HW=58.50' (Free Discharge) **1=Culvert** (Barrel Controls 1.44 cfs @ 2.91 fps)

Summary for Pond B: POND B BR

Inflow Area =	110,356 sf, 28.88% Impervious,	Inflow Depth > 3.23" for 100 Year event
Inflow =	5.78 cfs @ 12.15 hrs, Volume=	29,731 cf
Outflow =	4.23 cfs @ 12.30 hrs, Volume=	27,065 cf, Atten= 27%, Lag= 9.5 min
Discarded =	0.05 cfs @ 12.30 hrs, Volume=	3,304 cf
Primary =	4.18 cfs @ 12.30 hrs, Volume=	23,760 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.72' @ 12.30 hrs Surf.Area= 4,219 sf Storage= 6,297 cf

Plug-Flow detention time= 94.9 min calculated for 27,064 cf (91% of inflow) Center-of-Mass det. time= 47.3 min (838.6 - 791.3)

Volume	Invert	Avail.Stor	age Storage Description				
#1	55.95'	7,29	6 cf BioRente	ention Area (P	rismatic)Listed below (Recalc)		
Elevatio (fee 55.9 56.9 57.9	et) 95 95	urf.Area (sq-ft) 2,930 3,633 4,396	Inc.Store (cubic-feet) 0 3,282 4,015	Cum.Store (cubic-feet) 0 3,282 7,296			
Device	Routing	Invert	Outlet Devices				
#1 #2	Discarded Primary	55.95' 56.65'	0.520 in/hr Exfiltration over Surface area 18.0" Round Culvert L= 74.0' CPP, mitered to conform to fill, Ke= 0.700 Inlet / Outlet Invert= 56.65' / 54.06' S= 0.0350 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior				
Discord	Disported OutFlow Max-0.05 of a 12.20 hrs. HW-57.72' (Free Dispheres)						

Discarded OutFlow Max=0.05 cfs @ 12.30 hrs HW=57.72' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.05 cfs)

Primary OutFlow Max=4.18 cfs @ 12.30 hrs HW=57.72' (Free Discharge) 2=Culvert (Inlet Controls 4.18 cfs @ 3.10 fps)

Summary for Pond DMH1: DMH-B1

Inflow Area =	12,286 sf, 63.36% Impervious,	Inflow Depth > 5.57" for 100 Year event
Inflow =	1.30 cfs @ 12.04 hrs, Volume=	5,702 cf
Outflow =	1.30 cfs @ 12.04 hrs, Volume=	5,702 cf, Atten= 0%, Lag= 0.0 min
Primary =	1.30 cfs @ 12.04 hrs, Volume=	5,702 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 60.31' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices		
#1	Primary	59.62'	12.0" Round Culvert		
	-		L= 105.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 59.62' / 58.89' S= 0.0070 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior		

Primary OutFlow Max=1.30 cfs @ 12.04 hrs HW=60.31' (Free Discharge) **1=Culvert** (Inlet Controls 1.30 cfs @ 2.24 fps)

Summary for Pond DMH2: DMH-B2

Inflow Area	a =	12,286 sf	, 63.36% Impervious,	Inflow Depth > 5.57"	for 100 Year event
Inflow	=	1.30 cfs @	12.04 hrs, Volume=	5,702 cf	
Outflow	=	1.30 cfs @	12.04 hrs, Volume=	5,702 cf, Atte	en= 0%, Lag= 0.0 min
Primary	=	1.30 cfs @	12.04 hrs, Volume=	5,702 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 59.48' @ 12.04 hrs

Device Routing Invert Outlet Devices	Outlet Devices		
#1 Primary 58.79' 12.0" Round Culvert L= 96.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 58.79' / 58.03' S= 0.0079 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior			

Primary OutFlow Max=1.30 cfs @ 12.04 hrs HW=59.48' (Free Discharge) -1=Culvert (Inlet Controls 1.30 cfs @ 2.24 fps)

Summary for Pond DMH3: DMH-B3

Inflow Area	a =	12,286 sf, 63.36%	6 Impervious,	Inflow Depth >	5.57"	for 100 Year event
Inflow	=	1.30 cfs @ 12.04 h	rs, Volume=	5,702 c	f	
Outflow	=	1.30 cfs @ 12.04 h	rs, Volume=	5,702 c	f, Attei	n= 0%, Lag= 0.0 min
Primary	=	1.30 cfs @ 12.04 h	rs, Volume=	5,702 c	f	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.62' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices		
#1	Primary	57.93'	12.0" Round Culvert L= 43.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.93' / 57.60' S= 0.0077 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior		

Primary OutFlow Max=1.30 cfs @ 12.04 hrs HW=58.62' (Free Discharge)

Summary for Pond DMH4: DMH-B4

Inflow Area	=	69,937 sf, 38.42% Impervious, Inflow Depth > 3.88" for	100 Year event
Inflow :	=	5.02 cfs @ 12.13 hrs, Volume= 22,614 cf	
Outflow :	=	5.02 cfs @ 12.13 hrs, Volume= 22,614 cf, Atten= 0%	6, Lag= 0.0 min
Primary :	=	5.02 cfs @ 12.13 hrs, Volume= 22,614 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Peak Elev= 58.92' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices			
#1	Primary	57.50'	18.0" Round Culvert L= 31.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.50' / 57.34' S= 0.0052 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior			

Primary OutFlow Max=5.01 cfs @ 12.13 hrs HW=58.91' (Free Discharge) **1=Culvert** (Barrel Controls 5.01 cfs @ 3.75 fps)

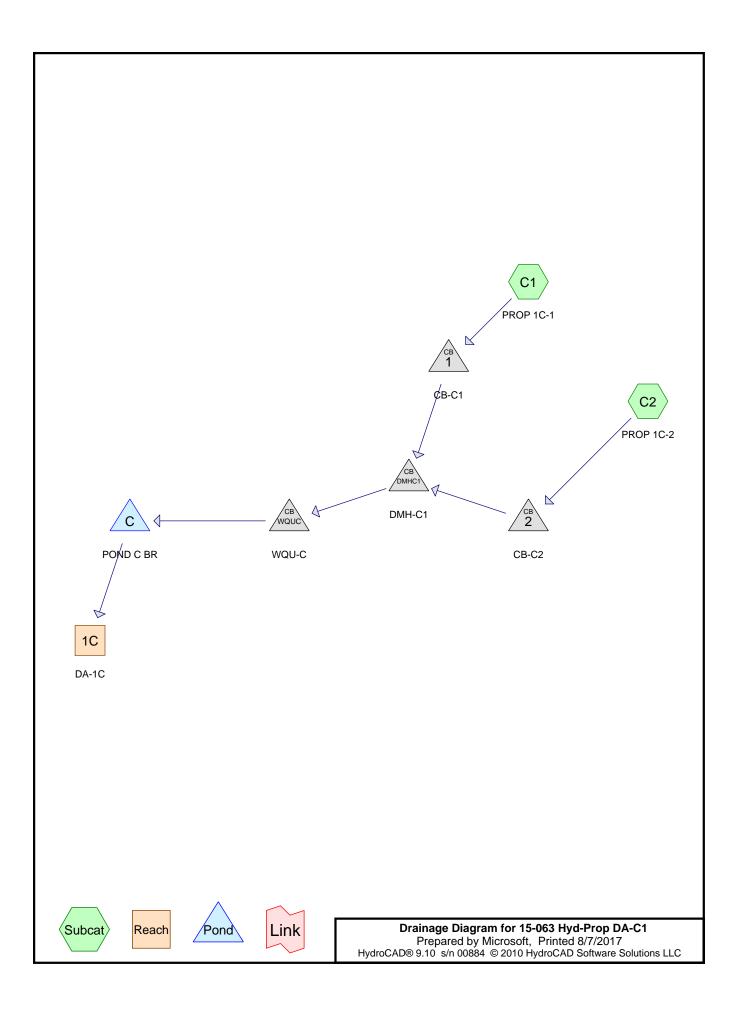
Summary for Pond WQU1: WQU-B

Inflow Area	ι =	69,937 sf	, 38.42% Impervious,	Inflow Depth > 3.88"	for 100 Year event
Inflow	=	5.02 cfs @	12.13 hrs, Volume=	22,614 cf	
Outflow	=	5.02 cfs @	12.13 hrs, Volume=	22,614 cf, Atte	en= 0%, Lag= 0.0 min
Primary	=	5.02 cfs @	12.13 hrs, Volume=	22,614 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.65' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices			
#1	Primary	57.34'	18.0" Round Culvert L= 115.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $57.34' / 56.70'$ S= 0.0056 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior			

Primary OutFlow Max=5.01 cfs @ 12.13 hrs HW=58.65' (Free Discharge) **1=Culvert** (Inlet Controls 5.01 cfs @ 3.07 fps)



Area Listing (all nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
24,410	39	>75% Grass cover, Good, HSG A (C1, C2)
20,099	98	Paved parking, HSG A (C1, C2)
8,489	98	Roofs, HSG A (C1, C2)

Summary for Subcatchment C1: PROP 1C-1

Runoff = 0.77 cfs @ 12.13 hrs, Volume= 3,003 cf, Depth> 1.55"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

_	A	rea (sf)	CN	Description						
		9,184	98	Paved parking, HSG A						
		3,397	98	Roofs, HSC	Roofs, HSG A					
_		10,648	39	>75% Gras	s cover, Go	bod, HSG A				
		23,229	71	Weighted A	verage					
		10,648	39	45.84% Per	rvious Area					
		12,581	98	54.16% Imp	pervious Ar	ea				
	Тс	Length	Slope		Capacity	Description				
_	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)					
	8.2	50	0.0200	0.10		Sheet Flow,				
						Grass: Dense n= 0.240 P2= 3.20"				
	1.4	170	0.0100	2.03		Shallow Concentrated Flow,				
_						Paved Kv= 20.3 fps				
	06	220	Total							

9.6 220 Total

Summary for Subcatchment C2: PROP 1C-2

Runoff = 0.98 cfs @ 12.13 hrs, Volume= 3,820 cf, Depth> 1.54"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

A	rea (sf)	CN	Description		
	10,915	98	Paved park	ing, HSG A	N
	5,092	98	Roofs, HSG	βA	
	13,762	39 :	>75% Gras	s cover, Go	bod, HSG A
	29,769	71	Weighted A	verage	
	13,762	39 4	46.23% Pei	vious Area	
	16,007	98	53.77% Imp	pervious Ar	ea
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.2	50	0.0200	0.10		Sheet Flow,
					Grass: Dense n= 0.240 P2= 3.20"
1.5	180	0.0100	2.03		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
9.7	230	Total			

Summary for Reach 1C: DA-1C

Inflow Are	a =	52,998 sf, 53.94% Impervious	, Inflow Depth = 0.70 "	for 2 Year event
Inflow	=	1.49 cfs @ 12.19 hrs, Volume=	3,111 cf	
Outflow	=	1.49 cfs @ 12.19 hrs, Volume=	3,111 cf, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Pond 1: CB-C1

Inflow Area	a =	23,229 sf	, 54.16% Impervious,	Inflow Depth > 1.55	for 2 Year event
Inflow	=	0.77 cfs @	12.13 hrs, Volume=	3,003 cf	
Outflow	=	0.77 cfs @	12.13 hrs, Volume=	3,003 cf, Att	en= 0%, Lag= 0.0 min
Primary	=	0.77 cfs @	12.13 hrs, Volume=	3,003 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.27' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary		12.0" Round Culvert L= 20.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.70' / 56.60' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.77 cfs @ 12.13 hrs HW=57.27' (Free Discharge) **1=Culvert** (Barrel Controls 0.77 cfs @ 2.43 fps)

Summary for Pond 2: CB-C2

Inflow Area	=	29,769 sf,	, 53.77% Impervious,	Inflow Depth > 1.54"	for 2 Year event
Inflow =	=	0.98 cfs @	12.13 hrs, Volume=	3,820 cf	
Outflow =	=	0.98 cfs @	12.13 hrs, Volume=	3,820 cf, Atte	en= 0%, Lag= 0.0 min
Primary =	=	0.98 cfs @	12.13 hrs, Volume=	3,820 cf	-

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.32' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.70'	12.0" Round Culvert L= 9.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.70' / 56.60' S= 0.0111 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.98 cfs @ 12.13 hrs HW=57.32' (Free Discharge) ☐ 1=Culvert (Barrel Controls 0.98 cfs @ 2.73 fps)

Summary for Pond C: POND C BR

Inflow Area =	52,998 sf, 53.94% Impervious,	Inflow Depth > 1.54" for 2 Year event
Inflow =	1.75 cfs @ 12.13 hrs, Volume=	6,823 cf
Outflow =	1.52 cfs @ 12.19 hrs, Volume=	5,276 cf, Atten= 13%, Lag= 3.5 min
Discarded =	0.03 cfs @ 12.19 hrs, Volume=	2,165 cf
Primary =	1.49 cfs @ 12.19 hrs, Volume=	3,111 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 56.60' @ 12.19 hrs Surf.Area= 2,815 sf Storage= 2,109 cf

Plug-Flow detention time= 137.1 min calculated for 5,274 cf (77% of inflow) Center-of-Mass det. time= 56.3 min (815.9 - 759.5)

Volume	Invert	Avail.Stora	age Storage I	Description	
#1	55.75'	3,31	1 cf STORM	WATER WETL	AND (Prismatic)Listed below (Recalc)
Elevatio (fee 55.7 56.0 57.0	25 00	rf.Area (sq-ft) 2,182 2,363 3,123	Inc.Store (cubic-feet) 0 568 2,743	Cum.Store (cubic-feet) 0 568 3,311	
Device	Routing	Invert	Outlet Devices	i	
#1 #2	Discarded Primary	55.75' 56.45'	Head (feet) 0. 2.50 3.00	.0' breadth Br 20 0.40 0.60) 2.69 2.72 2.	Surface area oad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00 75 2.85 2.98 3.08 3.20 3.28 3.31
Discarded OutFlow Max=0.03 cfs @ 12.19 hrs HW=56.60' (Free Discharge)					

Primary OutFlow Max=1.49 cfs @ 12.19 hrs HW=56.60' (Free Discharge) ←2=Broad-Crested Rectangular Weir (Weir Controls 1.49 cfs @ 1.02 fps)

Summary for Pond DMHC1: DMH-C1

Inflow Area	=	52,998 sf,	53.94% Impervious,	Inflow Depth > 1.	.54" for 2 Year event
Inflow =	=	1.75 cfs @	12.13 hrs, Volume=	6,823 cf	
Outflow =	=	1.75 cfs @	12.13 hrs, Volume=	6,823 cf,	Atten= 0%, Lag= 0.0 min
Primary =	=	1.75 cfs @	12.13 hrs, Volume=	6,823 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.37' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.65'	18.0" Round Culvert L= 9.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.65' / 56.52' S= 0.0144 '/' Cc= 0.900

n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.75 cfs @ 12.13 hrs HW=57.37' (Free Discharge) -1=Culvert (Barrel Controls 1.75 cfs @ 3.06 fps)

Summary for Pond WQUC: WQU-C

Inflow Area	a =	52,998 sf	, 53.94% Impervious,	Inflow Depth > 1.54"	for 2 Year event
Inflow	=	1.75 cfs @	12.13 hrs, Volume=	6,823 cf	
Outflow	=	1.75 cfs @	12.13 hrs, Volume=	6,823 cf, Atte	en= 0%, Lag= 0.0 min
Primary	=	1.75 cfs @	12.13 hrs, Volume=	6,823 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.22' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.52'	18.0" Round Culvert L= 114.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $56.52' / 55.95'$ S= $0.0050'/$ ' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.75 cfs @ 12.13 hrs HW=57.22' (Free Discharge) -1=Culvert (Barrel Controls 1.75 cfs @ 3.16 fps)

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Summary for Subcatchment C1: PROP 1C-1

Runoff = 1.18 cfs @ 12.13 hrs, Volume= 4,800 cf, Depth> 2.48"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

_	A	rea (sf)	CN	Description		
		9,184	98	Paved park	ing, HSG A	N
		3,397	98	Roofs, HSC	θĂ	
_		10,648	39	>75% Gras	s cover, Go	bod, HSG A
		23,229	71	Weighted A	verage	
		10,648	39	45.84% Pe	rvious Area	
		12,581	98	54.16% Im	pervious Ar	ea
	Та	Longth	Clan		Conosity	Description
	Tc (min)	Length (feet)	Slop (ft/ft		Capacity (cfs)	Description
-	8.2	50	0.020	/ (/	(013)	Shoot Flow
	0.2	50	0.020	0 0.10		Sheet Flow, Grass: Dense n= 0.240 P2= 3.20"
	1.4	170	0.010	0 2.03		Shallow Concentrated Flow,
	1.4	170	0.010	2.00		Paved $Kv = 20.3$ fps
-	0.6	220	Total			· · · · · · · · · · · · · · · · · · ·

9.6 220 Total

Summary for Subcatchment C2: PROP 1C-2

Runoff = 1.50 cfs @ 12.13 hrs, Volume= 6,110 cf, Depth> 2.46"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

A	rea (sf)	CN	Description		
	10,915	98	Paved park	ing, HSG A	N
	5,092	98	Roofs, HSC	βA	
	13,762	39	>75% Gras	s cover, Go	bod, HSG A
	29,769	71	Weighted A	verage	
	13,762	39	46.23% Pe	vious Area	l
	16,007	98	53.77% Imp	pervious Ar	ea
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.2	50	0.0200	0.10		Sheet Flow,
					Grass: Dense n= 0.240 P2= 3.20"
1.5	180	0.0100	2.03		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
9.7	230	Total			

Summary for Reach 1C: DA-1C

Inflow Area	a =	52,998 sf,	53.94% Impervious,	Inflow Depth = 1.55"	for 10 Year event
Inflow	=	2.46 cfs @	12.17 hrs, Volume=	6,844 cf	
Outflow	=	2.46 cfs @	12.17 hrs, Volume=	6,844 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Pond 1: CB-C1

Inflow Area	a =	23,229 sf, 54.16% Impervious, Inflow Depth > 2.48" for 10 Year event
Inflow	=	1.18 cfs @ 12.13 hrs, Volume= 4,800 cf
Outflow	=	1.18 cfs @ 12.13 hrs, Volume= 4,800 cf, Atten= 0%, Lag= 0.0 min
Primary	=	1.18 cfs @ 12.13 hrs, Volume= 4,800 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.43' @ 12.13 hrs

#1 Primary 56.70' 12.0" Round Culvert L= 20.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.70' / 56.60' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior	

Primary OutFlow Max=1.18 cfs @ 12.13 hrs HW=57.43' (Free Discharge) **1=Culvert** (Barrel Controls 1.18 cfs @ 2.70 fps)

Summary for Pond 2: CB-C2

Inflow Area	=	29,769 sf,	53.77% Impervious,	Inflow Depth > 2	2.46" for 10 Year event
Inflow :	=	1.50 cfs @	12.13 hrs, Volume=	6,110 cf	
Outflow :	=	1.50 cfs @	12.13 hrs, Volume=	6,110 cf,	Atten= 0%, Lag= 0.0 min
Primary :	=	1.50 cfs @	12.13 hrs, Volume=	6,110 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.51' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.70'	12.0" Round Culvert L= 9.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.70' / 56.60' S= 0.0111 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.50 cfs @ 12.13 hrs HW=57.51' (Free Discharge) -1=Culvert (Barrel Controls 1.50 cfs @ 3.01 fps)

Summary for Pond C: POND C BR

Inflow Area =	52,998 sf, 53.94% Impervious,	Inflow Depth > 2.47" for 10 Year event
Inflow =	2.68 cfs @ 12.13 hrs, Volume=	10,910 cf
Outflow =	2.49 cfs @ 12.17 hrs, Volume=	9,202 cf, Atten= 7%, Lag= 2.4 min
Discarded =	0.03 cfs @ 12.17 hrs, Volume=	2,358 cf
Primary =	2.46 cfs @ 12.17 hrs, Volume=	6,844 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 56.65' @ 12.17 hrs Surf.Area= 2,859 sf Storage= 2,272 cf

Plug-Flow detention time= 108.1 min calculated for 9,202 cf (84% of inflow) Center-of-Mass det. time= 39.6 min (798.6 - 759.1)

Volume	Invert	Avail.Stora	age Storage	Description			
#1	55.75'	3,31 <i>°</i>	1 cf STORM	WATER WETL	AND (Prismatic)Listed below (Recalc)		
Elevatio (fee 55.7	et) 75	2,182	Inc.Store (cubic-feet) 0	Cum.Store (cubic-feet) 0			
56.0		2,363	568	568			
57.0	0	3,123	2,743	3,311			
Device	Routing	Invert	Outlet Device:	5			
#1	Discarded	55.75'	0.520 in/hr Ex	diltration over	Surface area		
#2	Primary		Head (feet) 0 2.50 3.00	.20 0.40 0.60) 2.69 2.72 2.	oad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00 75 2.85 2.98 3.08 3.20 3.28 3.31		
Discarded OutFlow Max=0.03 cfs @ 12.17 hrs HW=56.65' (Free Discharge)							
Primary OutFlow Max=2.46 cfs @ 12.17 hrs HW=56.65' (Free Discharge)							

2=Broad-Crested Rectangular Weir (Weir Controls 2.46 cfs @ 1.21 fps)

Summary for Pond DMHC1: DMH-C1

Inflow Area =	52,998 sf, 53.94% Impervious,	Inflow Depth > 2.47" for 10 Year event
Inflow =	2.68 cfs @ 12.13 hrs, Volume=	10,910 cf
Outflow =	2.68 cfs @ 12.13 hrs, Volume=	10,910 cf, Atten= 0%, Lag= 0.0 min
Primary =	2.68 cfs @ 12.13 hrs, Volume=	10,910 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.58' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.65'	18.0" Round Culvert L= 9.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.65' / 56.52' S= 0.0144 '/' Cc= 0.900

n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=2.67 cfs @ 12.13 hrs HW=57.57' (Free Discharge) ☐ 1=Culvert (Barrel Controls 2.67 cfs @ 3.35 fps)

Summary for Pond WQUC: WQU-C

Inflow Are	a =	52,998 sf, 53.94% Impervious, Inflow Depth > 2.47" for 10 Year even	nt
Inflow	=	2.68 cfs @ 12.13 hrs, Volume= 10,910 cf	
Outflow	=	2.68 cfs @ 12.13 hrs, Volume= 10,910 cf, Atten= 0%, Lag= 0.0 m	nin
Primary	=	2.68 cfs @ 12.13 hrs, Volume= 10,910 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.42' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.52'	18.0" Round Culvert L= 114.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.52' / 55.95' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=2.67 cfs @ 12.13 hrs HW=57.42' (Free Discharge) **1=Culvert** (Barrel Controls 2.67 cfs @ 3.49 fps)

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Summary for Subcatchment C1: PROP 1C-1

Runoff = 2.30 cfs @ 12.13 hrs, Volume= 9,572 cf, Depth> 4.94"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

_	A	rea (sf)	CN	Description		
		9,184	98	Paved park	ing, HSG A	N
		3,397	98	Roofs, HSC	θĂ	
_		10,648	39	>75% Gras	s cover, Go	bod, HSG A
		23,229	71	Weighted A	verage	
		10,648	39	45.84% Per	rvious Area	l
		12,581	98	54.16% Imp	pervious Ar	ea
	Тс	Length	Slop	e Velocity	Capacity	Description
	(min)	(feet)	(ft/ft		(cfs)	Description
	8.2	50	0.020	0.10		Sheet Flow,
						Grass: Dense n= 0.240 P2= 3.20"
	1.4	170	0.010	0 2.03		Shallow Concentrated Flow,
_						Paved Kv= 20.3 fps
	06	220	Total			

9.6 220 Total

Summary for Subcatchment C2: PROP 1C-2

Runoff = 2.91 cfs @ 12.13 hrs, Volume= 12,201 cf, Depth> 4.92"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

A	rea (sf)	CN	Description		
	10,915	98	Paved park	ing, HSG A	N
	5,092	98	Roofs, HSO	βA	
	13,762	39	>75% Gras	s cover, Go	bod, HSG A
	29,769	71	Weighted A	verage	
	13,762	39	46.23% Pei	vious Area	
	16,007	98	53.77% Imp	pervious Ar	ea
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.2	50	0.0200	0.10		Sheet Flow,
					Grass: Dense n= 0.240 P2= 3.20"
1.5	180	0.0100	2.03		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
9.7	230	Total			

Summary for Reach 1C: DA-1C

Inflow Area	a =	52,998 sf,	53.94% Impervious,	Inflow Depth > 3.9	96" for 100 Year event
Inflow	=	4.91 cfs @	12.17 hrs, Volume=	17,487 cf	
Outflow	=	4.91 cfs @	12.17 hrs, Volume=	17,487 cf, A	Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Pond 1: CB-C1

Inflow Area	a =	23,229 sf, 54.16% Impervious, Inflow Depth > 4.94" for 100 Year event
Inflow	=	2.30 cfs @ 12.13 hrs, Volume= 9,572 cf
Outflow	=	2.30 cfs @ 12.13 hrs, Volume= 9,572 cf, Atten= 0%, Lag= 0.0 min
Primary	=	2.30 cfs @ 12.13 hrs, Volume= 9,572 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.84' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
<u>200100</u> #1	Primary		12.0" Round Culvert L= 20.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.70' / 56.60' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=2.29 cfs @ 12.13 hrs HW=57.84' (Free Discharge) **1=Culvert** (Barrel Controls 2.29 cfs @ 3.22 fps)

Summary for Pond 2: CB-C2

Inflow Area	a =	29,769 sf,	53.77% Impervious,	Inflow Depth > 4.92"	for 100 Year event
Inflow	=	2.91 cfs @	12.13 hrs, Volume=	12,201 cf	
Outflow	=	2.91 cfs @	12.13 hrs, Volume=	12,201 cf, Atter	n= 0%, Lag= 0.0 min
Primary	=	2.91 cfs @	12.13 hrs, Volume=	12,201 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.15' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.70'	12.0" Round Culvert L= 9.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.70' / 56.60' S= 0.0111 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=2.91 cfs @ 12.13 hrs HW=58.15' (Free Discharge) -1=Culvert (Inlet Controls 2.91 cfs @ 3.71 fps)

Summary for Pond C: POND C BR

Inflow Area =	52,998 sf, 53.94% Impervious,	Inflow Depth > 4.93" for 100 Year event
Inflow =	5.21 cfs @ 12.13 hrs, Volume=	21,773 cf
Outflow =	4.94 cfs @ 12.17 hrs, Volume=	20,034 cf, Atten= 5%, Lag= 2.1 min
Discarded =	0.04 cfs @ 12.17 hrs, Volume=	2,547 cf
Primary =	4.91 cfs @ 12.17 hrs, Volume=	17,487 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 56.77' @ 12.17 hrs Surf.Area= 2,948 sf Storage= 2,614 cf

Plug-Flow detention time= 76.8 min calculated for 20,033 cf (92% of inflow) Center-of-Mass det. time= 33.5 min (796.9 - 763.4)

Volume	Invert	Avail.Stora	age Storage	Description	
#1	55.75'	3,31	1 cf STORN	I WATER WETL	AND (Prismatic)Listed below (Recalc)
Elevatic (fee 55.7 56.0 57.0	/t) /5 00 00	2,182 2,363 3,123	Inc.Store (cubic-feet) 0 568 2,743	Cum.Store (cubic-feet) 0 568 3,311	
Device	Routing	Invert	Outlet Device	-	
#1 #2	Discarded Primary	56.45'	10.0' long x Head (feet) (2.50 3.00).20 0.40 0.60 h) 2.69 2.72 2.	Surface area oad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00 75 2.85 2.98 3.08 3.20 3.28 3.31
		Max=0.04 cfs		HW=56.77' (Fr	ree Discharge)

Primary OutFlow Max=4.90 cfs @ 12.17 hrs HW=56.77' (Free Discharge) ←2=Broad-Crested Rectangular Weir (Weir Controls 4.90 cfs @ 1.53 fps)

Summary for Pond DMHC1: DMH-C1

Inflow Area	a =	52,998 sf, 53.94% Impervious, Inflow Depth > 4.93" for 100 Year eve	ent
Inflow	=	5.21 cfs @ 12.13 hrs, Volume= 21,773 cf	
Outflow	=	5.21 cfs @ 12.13 hrs, Volume= 21,773 cf, Atten= 0%, Lag= 0.0 m	nin
Primary	=	5.21 cfs @ 12.13 hrs, Volume= 21,773 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.06' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.65'	18.0" Round Culvert L= 9.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.65' / 56.52' S= 0.0144 '/' Cc= 0.900

n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=5.20 cfs @ 12.13 hrs HW=58.06' (Free Discharge) ☐ 1=Culvert (Barrel Controls 5.20 cfs @ 3.91 fps)

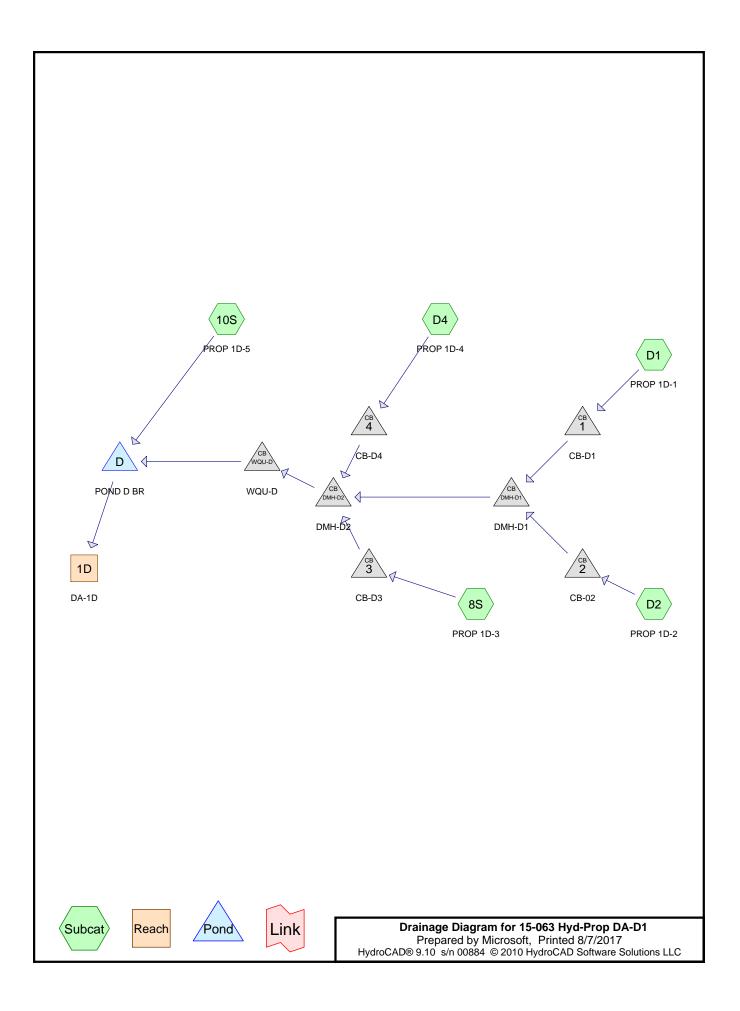
Summary for Pond WQUC: WQU-C

Inflow Are	a =	52,998 sf, 53.94% Impervious, Inflow Depth > 4.93" for 100 Year event	
Inflow	=	5.21 cfs @ 12.13 hrs, Volume= 21,773 cf	
Outflow	=	5.21 cfs @ 12.13 hrs, Volume= 21,773 cf, Atten= 0%, Lag= 0.0 min	1
Primary	=	5.21 cfs @ 12.13 hrs, Volume= 21,773 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.89' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.52'	18.0" Round Culvert L= 114.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.52' / 55.95' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=5.20 cfs @ 12.13 hrs HW=57.89' (Free Discharge) **1=Culvert** (Barrel Controls 5.20 cfs @ 4.05 fps)



Area Listing (all nodes)

CN	Description (subcatchment-numbers)
39	>75% Grass cover, Good, HSG A (8S, 10S, D1, D2, D4)
98	Paved parking, HSG A (8S, D1, D2, D4)
98	Roofs, HSG A (10S, D1, D4)
	39 98

Summary for Subcatchment 8S: PROP 1D-3

Runoff = 0.39 cfs @ 12.16 hrs, Volume= 1,644 cf, Depth> 0.32"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

A	rea (sf)	CN E	Description			
	6,892	98 F	Paved park	ing, HSG A		
	54,769	39 >	-75% Gras	s cover, Go	ood, HSG A	
	61,661	46 V	Veighted A	verage		
	54,769	39 8	38.82% Per	vious Area		
	6,892	98 1	1.18% Imp	pervious Ar	ea	
_						
Tc	Length	Slope	Velocity	Capacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
9.7	50	0.0130	0.09		Sheet Flow,	
					Grass: Dense n= 0.240 P2= 3.20"	
1.9	200	0.0130	1.71		Shallow Concentrated Flow,	
					Grassed Waterway Kv= 15.0 fps	
0.5	66	0.0100	2.03		Shallow Concentrated Flow,	
					Paved Kv= 20.3 fps	
12.1	316	Total				

Summary for Subcatchment 10S: PROP 1D-5

Runoff = 0.11 cfs @ 12.11 hrs, Volume= 400 cf, Depth> 0.26"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

Are	ea (sf)	CN I	Description		
	1,675	98	Roofs, HSG	βA	
1	7,130	39 :	>75% Gras	s cover, Go	ood, HSG A
1	8,805	44	Weighted A	verage	
1	7,130	39 9	91.09% Per	vious Area	
	1,675	98 8	8.91% Impe	ervious Area	а
Tc	Length	Slope		Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.2	50	0.0200	0.10		Sheet Flow,
					Grass: Dense n= 0.240 P2= 3.20"
0.2	70	0.1000	4.74		Shallow Concentrated Flow,
					Grassed Waterway Kv= 15.0 fps
8.4	120	Total			

Summary for Subcatchment D1: PROP 1D-1

Runoff = 0.88 cfs @ 12.14 hrs, Volume= 3,519 cf, Depth> 1.56"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

A	rea (sf)	CN	Description		
	9,083	98	Paved park	ing, HSG A	N
	5,664	98	Roofs, HSG	6 A	
	12,238	39 :	>75% Gras	s cover, Go	bod, HSG A
	26,985	71	Weighted A	verage	
	12,238	39 4	45.35% Pe	vious Area	
	14,747	98	54.65% Imp	pervious Ar	ea
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.2	50	0.0200	0.10		Sheet Flow,
					Grass: Dense n= 0.240 P2= 3.20"
2.5	300	0.0100	2.03		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
10.7	350	Total			

Summary for Subcatchment D2: PROP 1D-2

	Runoff	=	0.28 cfs @	12.15 hrs, Volume=	= 1,156 cf, Depth> 0.95"
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Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

A	Area (sf)	CN E	Description			
	4,844			ing, HSG A		
	9,786	39 >	75% Gras	s cover, Go	bod, HSG A	
	14,630	59 V	Veighted A	verage		
	9,786	39 6	6.89% Per	vious Area		
	4,844	98 3	3.11% Imp	pervious Ar	ea	
_		. .				
Tc	- 3	Slope	Velocity	Capacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
9.7	50	0.0130	0.09		Sheet Flow, SHHET	
					Grass: Dense n= 0.240 P2= 3.20"	
1.4	140	0.0130	1.71		Shallow Concentrated Flow,	
					Grassed Waterway Kv= 15.0 fps	
0.3	32	0.0100	2.03		Shallow Concentrated Flow,	
					Paved Kv= 20.3 fps	
11.4	222	Total				

Summary for Subcatchment D4: PROP 1D-4

Runoff = 1.23 cfs @ 12.12 hrs, Volume= 4,679 cf, Depth> 1.40"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

_	A	rea (sf)	CN	Description	า	
		13,972	98	Paved parl	king, HSG A	N
		5,630	98	Roofs, HS	GĂ	
_		20,432	39	>75% Gras	ss cover, Go	bod, HSG A
		40,034	68	Weighted /	Average	
		20,432	39	51.04% Pe	rvious Area	l de la constante de
		19,602	98	98 48.96% Imperv		ea
	То	Longth	Slop		Conocity	Description
	Tc (min)	Length (feet)	Slop (ft/f			Description
-	7.4	70	0.020			Sheet Flow,
		10	0.020	0.10		Grass: Short n= 0.150 P2= 3.20"
	1.4	172	0.010	0 2.03		Shallow Concentrated Flow,
						Paved Kv= 20.3 fps
-	0 0	242	Total			

8.8 242 Total

Summary for Reach 1D: DA-1D

Inflow Area	a =	162,115 sf,	29.46% Impervious,	Inflow Depth = 0.34"	for 2 Year event
Inflow	=	2.41 cfs @	12.20 hrs, Volume=	4,659 cf	
Outflow	=	2.41 cfs @	12.20 hrs, Volume=	4,659 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Pond 1: CB-D1

Inflow Area	a =	26,985 sf, 54.6	5% Impervious,	Inflow Depth > 1.5	56" for 2 Year event
Inflow	=	0.88 cfs @ 12.14	4 hrs, Volume=	3,519 cf	
Outflow	=	0.88 cfs @ 12.14	4 hrs, Volume=	3,519 cf, <i>i</i>	Atten= 0%, Lag= 0.0 min
Primary	=	0.88 cfs @ 12.14	4 hrs, Volume=	3,519 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.37' @ 12.14 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.77'	12.0" Round Culvert L= 6.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $57.77' / 57.71'$ S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.87 cfs @ 12.14 hrs HW=58.37' (Free Discharge) **1=Culvert** (Barrel Controls 0.87 cfs @ 2.54 fps)

Summary for Pond 2: CB-02

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.15' @ 12.15 hrs

Device	Routing	Invert	Outlet Devices
	Primary		12.0" Round Culvert L= 17.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.85' / 57.71' S= 0.0082 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.28 cfs @ 12.15 hrs HW=58.15' (Free Discharge) -1=Culvert (Barrel Controls 0.28 cfs @ 2.11 fps)

Summary for Pond 3: CB-D3

Inflow Area	a =	61,661 sf, 11.18	3% Impervious,	Inflow Depth > 0.3	32" for 2 Year event
Inflow	=	0.39 cfs @ 12.16	hrs, Volume=	1,644 cf	
Outflow	=	0.39 cfs @ 12.16	hrs, Volume=	1,644 cf, <i>1</i>	Atten= 0%, Lag= 0.0 min
Primary	=	0.39 cfs @ 12.16	hrs, Volume=	1,644 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 56.99' @ 12.16 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.60'	12.0" Round Culvert L= 17.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.60' / 56.51' S= 0.0053 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.39 cfs @ 12.16 hrs HW=56.99' (Free Discharge) -1=Culvert (Barrel Controls 0.39 cfs @ 2.07 fps)

Summary for Pond 4: CB-D4

Inflow Area	a =	40,034 sf, 48.96% Impervious, Inflow Depth > 1.40" for 2 Year	event
Inflow	=	1.23 cfs @ 12.12 hrs, Volume= 4,679 cf	
Outflow	=	1.23 cfs @ 12.12 hrs, Volume= 4,679 cf, Atten= 0%, Lag=	0.0 min
Primary	=	1.23 cfs @ 12.12 hrs, Volume= 4,679 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.31' @ 12.12 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.60'	12.0" Round Culvert
			L= 6.0' CPP, projecting, no headwall, Ke= 0.900

Inlet / Outlet Invert= 56.60' / 56.51' S= 0.0150' /' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.23 cfs @ 12.12 hrs HW=57.31' (Free Discharge) **1=Culvert** (Barrel Controls 1.23 cfs @ 2.88 fps)

Summary for Pond D: POND D BR

Inflow Area =	162,115 sf, 29.46% Impervious,	Inflow Depth > 0.84" for 2 Year event
Inflow =	2.86 cfs @ 12.13 hrs, Volume=	11,398 cf
Outflow =	2.47 cfs @ 12.20 hrs, Volume=	8,562 cf, Atten= 14%, Lag= 3.8 min
Discarded =	0.06 cfs @ 12.20 hrs, Volume=	3,903 cf
Primary =	2.41 cfs @ 12.20 hrs, Volume=	4,659 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 55.50' @ 12.20 hrs Surf.Area= 4,913 sf Storage= 3,657 cf

Plug-Flow detention time= 144.8 min calculated for 8,562 cf (75% of inflow) Center-of-Mass det. time= 59.8 min (819.8 - 759.9)

Volume	Invert	Avail.Stor	rage Storage	Description	
#1	54.70'	4,67	75 cf STORM	I WATER WETLAN	ND (Prismatic)Listed below (Recalc)
Elevatic (fee 54.7 55.7	et) 70	urf.Area (sq-ft) 4,273 5,077	Inc.Store (cubic-feet) 0 4,675	Cum.Store (cubic-feet) 0 4,675	
Device	Routing	Invert	Outlet Device	S	
#1 #2	Discarded Primary	54.70' 55.40'	30.0' long x Head (feet) (2.50 3.00	0.20 0.40 0.60 0.8 h) 2.69 2.72 2.75	urface area d-Crested Rectangular Weir 30 1.00 1.20 1.40 1.60 1.80 2.00 2.85 2.98 3.08 3.20 3.28 3.31

Discarded OutFlow Max=0.06 cfs @ 12.20 hrs HW=55.50' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.06 cfs)

Primary OutFlow Max=2.41 cfs @ 12.20 hrs HW=55.50' (Free Discharge) ←2=Broad-Crested Rectangular Weir (Weir Controls 2.41 cfs @ 0.83 fps)

Summary for Pond DMH-D1: DMH-D1

Inflow Area	a =	41,615 sf,	47.08% Impervious,	Inflow Depth > 1.35	5" for 2 Year event
Inflow	=	1.16 cfs @	12.14 hrs, Volume=	4,675 cf	
Outflow	=	1.16 cfs @	12.14 hrs, Volume=	4,675 cf, At	ten= 0%, Lag= 0.0 min
Primary	=	1.16 cfs @	12.14 hrs, Volume=	4,675 cf	-

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

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Peak Elev= 58.20' @ 12.14 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.61'	15.0" Round Culvert L= 189.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $57.61' / 56.65'$ S= 0.0051 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.15 cfs @ 12.14 hrs HW=58.20' (Free Discharge) 1=Culvert (Barrel Controls 1.15 cfs @ 2.98 fps)

Summary for Pond DMH-D2: DMH-D2

Inflow Area	=	143,310 sf	, 32.16% Impervious,	Inflow Depth > 0.9	2" for 2 Year event
Inflow	=	2.75 cfs @	12.13 hrs, Volume=	10,998 cf	
Outflow	=	2.75 cfs @	12.13 hrs, Volume=	10,998 cf, A	tten= 0%, Lag= 0.0 min
Primary	=	2.75 cfs @	12.13 hrs, Volume=	10,998 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.22' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.23'	18.0" Round Culvert L= 22.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.23' / 56.12' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=2.75 cfs @ 12.13 hrs HW=57.22' (Free Discharge) **1=Culvert** (Barrel Controls 2.75 cfs @ 3.16 fps)

Summary for Pond WQU-D: WQU-D

Inflow Area =	143,310 sf, 32.16% Impervious,	Inflow Depth > 0.92" for 2 Year event
Inflow =	2.75 cfs @ 12.13 hrs, Volume=	10,998 cf
Outflow =	2.75 cfs @ 12.13 hrs, Volume=	10,998 cf, Atten= 0%, Lag= 0.0 min
Primary =	2.75 cfs @ 12.13 hrs, Volume=	10,998 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.13' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.12'	18.0" Round Culvert L= 148.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $56.12' / 55.70'$ S= 0.0028 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=2.75 cfs @ 12.13 hrs HW=57.13' (Free Discharge) **1=Culvert** (Barrel Controls 2.75 cfs @ 3.07 fps)

Summary for Subcatchment 8S: PROP 1D-3

Runoff = 0.60 cfs @ 12.16 hrs, Volume= 3,209 cf, Depth> 0.62"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

 A	rea (sf)	CN [Description		
	6,892	98 F	Paved park	ing, HSG A	
	54,769	39 >	-75% Gras	s cover, Go	bod, HSG A
	61,661	46 \	Veighted A	verage	
	54,769	39 8	38.82% Per	vious Area	
	6,892	98 1	1.18% Imp	pervious Ar	ea
_					
Тс	Length	Slope		Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
9.7	50	0.0130	0.09		Sheet Flow,
					Grass: Dense n= 0.240 P2= 3.20"
1.9	200	0.0130	1.71		Shallow Concentrated Flow,
					Grassed Waterway Kv= 15.0 fps
0.5	66	0.0100	2.03		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
12.1	316	Total			

Summary for Subcatchment 10S: PROP 1D-5

Runoff = 0.16 cfs @ 12.11 hrs, Volume= 826 cf, Depth> 0.53"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

Area	a (sf)	CN	Description		
1	,675	98	Roofs, HSC	β A	
17	,130	39	>75% Gras	s cover, Go	ood, HSG A
18	,805	44	Weighted A	verage	
17	,130	39	91.09% Pei	vious Area	
1	,675	98	8.91% Impe	ervious Area	a
	ength	Slope		Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.2	50	0.0200	0.10		Sheet Flow,
					Grass: Dense n= 0.240 P2= 3.20"
0.2	70	0.1000	4.74		Shallow Concentrated Flow,
					Grassed Waterway Kv= 15.0 fps
8.4	120	Total			

Summary for Subcatchment D1: PROP 1D-1

Runoff = 1.34 cfs @ 12.14 hrs, Volume= 5,623 cf, Depth> 2.50"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

A	rea (sf)	CN [Description		
	9,083	98 F	Paved park	ing, HSG A	N
	5,664	98 F	Roofs, HSG	6 A	
	12,238	39 >	>75% Gras	s cover, Go	bod, HSG A
	26,985	71 \	Neighted A	verage	
	12,238	39 4	15.35% Pei	vious Area	
	14,747	98 5	54.65% Imp	pervious Ar	ea
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.2	50	0.0200	0.10		Sheet Flow,
					Grass: Dense n= 0.240 P2= 3.20"
2.5	300	0.0100	2.03		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
10.7	350	Total			

Summary for Subcatchment D2: PROP 1D-2

Runoff	=	0.43 cfs @	12.15 hrs.	Volume=	1,915 cf, Depth> 1.57"
Runon	_	0.70 013 @	12.101113,	volume_	

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

/	Area (sf)	CN E	Description			
	4,844			ing, HSG A		
	9,786	39 >	75% Gras	s cover, Go	ood, HSG A	
	14,630	59 V	Veighted A	verage		
	9,786	39 6	6.89% Per	vious Area		
	4,844	98 3	3.11% Imp	pervious Ar	ea	
_				•		
Tc		Slope	Velocity	Capacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
9.7	50	0.0130	0.09		Sheet Flow, SHHET	
					Grass: Dense n= 0.240 P2= 3.20"	
1.4	140	0.0130	1.71		Shallow Concentrated Flow,	
					Grassed Waterway Kv= 15.0 fps	
0.3	32	0.0100	2.03		Shallow Concentrated Flow,	
					Paved Kv= 20.3 fps	
11.4	222	Total				

Summary for Subcatchment D4: PROP 1D-4

Runoff = 1.88 cfs @ 12.12 hrs, Volume= 7,526 cf, Depth> 2.26"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

_	A	rea (sf)	CN	Description		
		13,972	98	Paved park	ing, HSG A	N
		5,630	98	Roofs, HSG	6 A	
		20,432	39	>75% Gras	s cover, Go	bod, HSG A
		40,034	68	Weighted A	verage	
		20,432	39	51.04% Per	rvious Area	
		19,602	98	48.96% Imp	pervious Ar	ea
	Тс	Length	Slop	e Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)	
	7.4	70	0.020	0.16		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.20"
	1.4	172	0.010	2.03		Shallow Concentrated Flow,
_						Paved Kv= 20.3 fps
	00	2/2	Total			

8.8 242 Total

Summary for Reach 1D: DA-1D

Inflow Area	a =	162,115 sf	, 29.46% Impervious,	Inflow Depth >	0.86"	for 10 Year event
Inflow	=	4.14 cfs @	12.16 hrs, Volume=	11,643 cf		
Outflow	=	4.14 cfs @	12.16 hrs, Volume=	11,643 cf	, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Pond 1: CB-D1

Inflow Area	ι =	26,985 sf,	54.65% Impervious,	Inflow Depth > 2.50"	for 10 Year event
Inflow	=	1.34 cfs @	12.14 hrs, Volume=	5,623 cf	
Outflow	=	1.34 cfs @	12.14 hrs, Volume=	5,623 cf, Atte	en= 0%, Lag= 0.0 min
Primary	=	1.34 cfs @	12.14 hrs, Volume=	5,623 cf	-

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.55' @ 12.14 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.77'	12.0" Round Culvert L= 6.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $57.77' / 57.71'$ S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.34 cfs @ 12.14 hrs HW=58.55' (Free Discharge) **1=Culvert** (Barrel Controls 1.34 cfs @ 2.81 fps)

Summary for Pond 2: CB-02

Inflow Area = 14,630 sf, 33.11% Impervious, Inflow Depth > 1.57" for 10 Year event 0.43 cfs @ 12.15 hrs. Volume= Inflow 1.915 cf = 0.43 cfs @ 12.15 hrs, Volume= Outflow 1,915 cf, Atten= 0%, Lag= 0.0 min = 0.43 cfs @ 12.15 hrs, Volume= Primary = 1,915 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.23' @ 12.15 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary		12.0" Round Culvert L= 17.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.85' / 57.71' S= 0.0082 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.43 cfs @ 12.15 hrs HW=58.23' (Free Discharge) **1=Culvert** (Barrel Controls 0.43 cfs @ 2.31 fps)

Summary for Pond 3: CB-D3

Inflow Area	a =	61,661 sf,	11.18% Impervious,	Inflow Depth > 0	.62" for 10 Year event
Inflow	=	0.60 cfs @	12.16 hrs, Volume=	3,209 cf	
Outflow	=	0.60 cfs @	12.16 hrs, Volume=	3,209 cf,	Atten= 0%, Lag= 0.0 min
Primary	=	0.60 cfs @	12.16 hrs, Volume=	3,209 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.09' @ 12.16 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.60'	12.0" Round Culvert L= 17.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.60' / 56.51' S= 0.0053 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.60 cfs @ 12.16 hrs HW=57.09' (Free Discharge) **1=Culvert** (Barrel Controls 0.60 cfs @ 2.29 fps)

Summary for Pond 4: CB-D4

Inflow Area	a =	40,034 sf, 48.96% Impervious, Inflow Depth > 2.26" for 10 Year event	
Inflow	=	1.88 cfs @ 12.12 hrs, Volume= 7,526 cf	
Outflow	=	1.88 cfs @ 12.12 hrs, Volume= 7,526 cf, Atten= 0%, Lag= 0.0 mi	n
Primary	=	1.88 cfs @ 12.12 hrs, Volume= 7,526 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.54' @ 12.12 hrs

Device	Routing	Invert	Outlet Devices		
#1	Primary	56.60'	2.0" Round Culvert		
			L= 6.0' CPP, projecting, no headwall, Ke= 0.900		

Inlet / Outlet Invert= 56.60' / 56.51' S= 0.0150'/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.88 cfs @ 12.12 hrs HW=57.54' (Free Discharge) **1=Culvert** (Barrel Controls 1.88 cfs @ 3.19 fps)

Summary for Pond D: POND D BR

Inflow Area =	162,115 sf, 29.46% Impervious,	Inflow Depth > 1.41" for 10 Year event
Inflow =	4.36 cfs @ 12.13 hrs, Volume=	19,098 cf
Outflow =	4.20 cfs @ 12.16 hrs, Volume=	15,906 cf, Atten= 4%, Lag= 1.8 min
Discarded =	0.06 cfs @ 12.16 hrs, Volume=	4,263 cf
Primary =	4.14 cfs @ 12.16 hrs, Volume=	11,643 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 55.54' @ 12.16 hrs Surf.Area= 4,947 sf Storage= 3,864 cf

Plug-Flow detention time= 112.9 min calculated for 15,906 cf (83% of inflow) Center-of-Mass det. time= 38.0 min (810.1 - 772.1)

Volume	Invert	Avail.Stor	rage Storage	e Description	
#1	54.70'	4,67	75 cf STORM	I WATER WETL	AND (Prismatic)Listed below (Recalc)
Elevatio (fee 54.7 55.7	et) 70	rf.Area (sq-ft) 4,273 5,077	Inc.Store (cubic-feet) 0 4,675	Cum.Store (cubic-feet) 0 4,675	
Device	Routing	Invert	Outlet Device	es	
#1 #2	Discarded Primary	54.70' 55.40'	30.0' long x Head (feet) (2.50 3.00	0.20 0.40 0.60 h) 2.69 2.72 2.	Surface areaoad-Crested Rectangular Weir0.801.001.201.401.601.802.00752.852.983.083.203.283.31

Discarded OutFlow Max=0.06 cfs @ 12.16 hrs HW=55.54' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.06 cfs)

Primary OutFlow Max=4.14 cfs @ 12.16 hrs HW=55.54' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 4.14 cfs @ 1.00 fps)

Summary for Pond DMH-D1: DMH-D1

Inflow Area	a =	41,615 sf, 47.08% Impervious, Inflow Depth > 2.17" for 10 Year event
Inflow	=	1.77 cfs @ 12.14 hrs, Volume= 7,538 cf
Outflow	=	1.77 cfs @ 12.14 hrs, Volume= 7,538 cf, Atten= 0%, Lag= 0.0 min
Primary	=	1.77 cfs @ 12.14 hrs, Volume= 7,538 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

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Peak Elev= 58.36' @ 12.14 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.61'	15.0" Round Culvert L= 189.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $57.61' / 56.65' S = 0.0051 '/' Cc= 0.900$ n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.76 cfs @ 12.14 hrs HW=58.36' (Free Discharge) 1=Culvert (Barrel Controls 1.76 cfs @ 3.31 fps)

Summary for Pond DMH-D2: DMH-D2

Inflow Area	a =	143,310 sf, 32.16% Impervious, Inflow	Depth > 1.53" for 10 Year event
Inflow	=	4.21 cfs @ 12.13 hrs, Volume=	18,272 cf
Outflow	=	4.21 cfs @ 12.13 hrs, Volume=	18,272 cf, Atten= 0%, Lag= 0.0 min
Primary	=	4.21 cfs @ 12.13 hrs, Volume=	18,272 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.51' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.23'	18.0" Round Culvert L= 22.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.23' / 56.12' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=4.20 cfs @ 12.13 hrs HW=57.51' (Free Discharge) **1=Culvert** (Barrel Controls 4.20 cfs @ 3.52 fps)

Summary for Pond WQU-D: WQU-D

Inflow Are	a =	143,310 sf, 32.16% Impervious, Inflow Depth > 1.53" for 10 Year event	
Inflow	=	4.21 cfs @ 12.13 hrs, Volume= 18,272 cf	
Outflow	=	4.21 cfs @ 12.13 hrs, Volume= 18,272 cf, Atten= 0%, Lag= 0.0 mi	n
Primary	=	4.21 cfs @ 12.13 hrs, Volume= 18,272 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.43' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.12'	18.0" Round Culvert L= 148.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $56.12' / 55.70'$ S= 0.0028 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=4.20 cfs @ 12.13 hrs HW=57.43′ (Free Discharge) ←1=Culvert (Barrel Controls 4.20 cfs @ 3.42 fps)

Summary for Subcatchment 8S: PROP 1D-3

Runoff = 2.06 cfs @ 12.19 hrs, Volume= 10,459 cf, Depth> 2.04"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

A	rea (sf)	CN E	Description			
	6,892	98 F	Paved park	ing, HSG A		
	54,769	39 >	-75% Gras	s cover, Go	ood, HSG A	
	61,661	46 V	Veighted A	verage		
	54,769	39 8	38.82% Per	vious Area		
	6,892	98 1	1.18% Imp	pervious Ar	ea	
_						
Tc	Length	Slope	Velocity	Capacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
9.7	50	0.0130	0.09		Sheet Flow,	
					Grass: Dense n= 0.240 P2= 3.20"	
1.9	200	0.0130	1.71		Shallow Concentrated Flow,	
					Grassed Waterway Kv= 15.0 fps	
0.5	66	0.0100	2.03		Shallow Concentrated Flow,	
					Paved Kv= 20.3 fps	
12.1	316	Total				

Summary for Subcatchment 10S: PROP 1D-5

Runoff = 0.65 cfs @ 12.14 hrs, Volume= 2,952 cf, Depth> 1.88"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

A	rea (sf)	CN [Description				
	1,675	98 Roofs, HSG A					
	17,130	39 >	-75% Gras	s cover, Go	bod, HSG A		
	18,805	44 \	Veighted A	verage			
17,130 39 91.09% Pervious Area				vious Area			
1,675 98 8.91% Impervious Area					a		
Тс	Length	Slope	Velocity	Capacity	Description		
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)			
8.2	50	0.0200	0.10		Sheet Flow,		
					Grass: Dense n= 0.240 P2= 3.20"		
0.2	70	0.1000	4.74		Shallow Concentrated Flow,		
					Grassed Waterway Kv= 15.0 fps		
8.4	120	Total					

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Summary for Subcatchment D1: PROP 1D-1

Runoff = 2.60 cfs @ 12.14 hrs, Volume= 11,192 cf, Depth> 4.98"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

A	rea (sf)	CN	Description					
	9,083	98	Paved park	ing, HSG A	N Contraction of the second seco			
	5,664	98 Roofs, HSG A						
	12,238	39 :	39 >75% Grass cover, Good, HSG A					
26,985 71 Weighted Average								
	12,238	39 4	45.35% Pe	vious Area				
	14,747 98 54.65% Impervious Are				ea			
Тс	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
8.2	50	0.0200	0.10		Sheet Flow,			
					Grass: Dense n= 0.240 P2= 3.20"			
2.5	300	0.0100	2.03		Shallow Concentrated Flow,			
					Paved Kv= 20.3 fps			
10.7	350	Total						

Summary for Subcatchment D2: PROP 1D-2

Runoff	_	0.94 cfs @	12 16 hrc	Volumo-	1 201 of Dopths 2 52"
RUHUH	=	0.94 015 @	12.101115,	volume=	4,291 cf, Depth> 3.52"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

A	Area (sf)	CN E	Description					
	4,844	98 Paved parking, HSG A						
	9,786	39 >	75% Gras	s cover, Go	bod, HSG A			
	14,630	59 V	Veighted A	verage				
	9,786	39 6						
	4,844	98 3	98 33.11% Impervious Area					
_		. .		- ·				
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
9.7	50	0.0130	0.09		Sheet Flow, SHHET			
					Grass: Dense n= 0.240 P2= 3.20"			
1.4	140	0.0130	1.71		Shallow Concentrated Flow,			
					Grassed Waterway Kv= 15.0 fps			
0.3	32	0.0100	2.03		Shallow Concentrated Flow,			
					Paved Kv= 20.3 fps			
11.4	222	Total						

Summary for Subcatchment D4: PROP 1D-4

Runoff = 3.74 cfs @ 12.12 hrs, Volume= 15,325 cf, Depth> 4.59"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

_	A	rea (sf)	CN	Description		
		13,972	98	Paved park	ing, HSG A	N
		5,630	98	Roofs, HSC	θĂ	
		20,432	39	>75% Gras	s cover, Go	bod, HSG A
		40,034	68	Weighted A	verage	
		20,432	39	51.04% Pe	rvious Area	l
		19,602	98	48.96% Imp	pervious Ar	ea
	Тс	Length	Slop	e Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft	t) (ft/sec)	(cfs)	
	7.4	70	0.020	0.16		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.20"
	1.4	172	0.010	0 2.03		Shallow Concentrated Flow,
_						Paved Kv= 20.3 fps
	0 0	242	Total			

8.8 242 Total

Summary for Reach 1D: DA-1D

Inflow Area	a =	162,115 sf,	29.46% Impervious,	Inflow Depth >	2.69"	for 100 Year event
Inflow	=	9.46 cfs @	12.17 hrs, Volume=	36,376 c	f	
Outflow	=	9.46 cfs @	12.17 hrs, Volume=	36,376 c	f, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Pond 1: CB-D1

Inflow Area	a =	26,985 sf, 54.65% Impervious, Inflow Depth > 4.98" for 100 Year eve	ent
Inflow	=	2.60 cfs @ 12.14 hrs, Volume= 11,192 cf	
Outflow	=	2.60 cfs @ 12.14 hrs, Volume= 11,192 cf, Atten= 0%, Lag= 0.0 m	nin
Primary	=	2.60 cfs @ 12.14 hrs, Volume= 11,192 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 59.03' @ 12.14 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.77'	12.0" Round Culvert L= 6.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.77' / 57.71' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=2.59 cfs @ 12.14 hrs HW=59.02' (Free Discharge) **1=Culvert** (Inlet Controls 2.59 cfs @ 3.30 fps)

Summary for Pond 2: CB-02

Inflow Area =14,630 sf, 33.11% Impervious, Inflow Depth > 3.52" for 100 Year eventInflow =0.94 cfs @12.16 hrs, Volume=4,291 cfOutflow =0.94 cfs @12.16 hrs, Volume=4,291 cfPrimary =0.94 cfs @12.16 hrs, Volume=4,291 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.45' @ 12.16 hrs

Device F	Routing	Invert	Outlet Devices
	Primary		12.0" Round Culvert L= 17.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.85' / 57.71' S= 0.0082 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.94 cfs @ 12.16 hrs HW=58.45' (Free Discharge) -1=Culvert (Barrel Controls 0.94 cfs @ 2.74 fps)

Summary for Pond 3: CB-D3

Inflow Area	a =	61,661 sf, 11.18% Impervious, Inflow Depth > 2.04" for 100 Year e	event
Inflow	=	2.06 cfs @ 12.19 hrs, Volume= 10,459 cf	
Outflow	=	2.06 cfs @ 12.19 hrs, Volume= 10,459 cf, Atten= 0%, Lag= 0.	0 min
Primary	=	2.06 cfs @ 12.19 hrs, Volume= 10,459 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.64' @ 12.19 hrs

Device	Routing	Invert	Outlet Devices
-	<u>U</u>	56.60'	12.0" Round Culvert L= 17.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.60' / 56.51' S= 0.0053 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=2.06 cfs @ 12.19 hrs HW=57.64' (Free Discharge)

Summary for Pond 4: CB-D4

Inflow Area	a =	40,034 sf, 48.96% Impervious, Inflow Depth > 4.59" for 100 Year event	
Inflow	=	3.74 cfs @ 12.12 hrs, Volume= 15,325 cf	
Outflow	=	3.74 cfs @ 12.12 hrs, Volume= 15,325 cf, Atten= 0%, Lag= 0.0 min	
Primary	=	3.74 cfs @ 12.12 hrs, Volume= 15,325 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.67' @ 12.12 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.60'	12.0" Round Culvert
			L= 6.0' CPP, projecting, no headwall, Ke= 0.900

Inlet / Outlet Invert= 56.60' / 56.51' S= 0.0150'/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=3.74 cfs @ 12.12 hrs HW=58.67' (Free Discharge) **1=Culvert** (Inlet Controls 3.74 cfs @ 4.76 fps)

Summary for Pond D: POND D BR

Inflow Area =	162,115 sf, 29.46% Impervious,	Inflow Depth > 3.27" for 100 Year event
Inflow =	9.75 cfs @ 12.14 hrs, Volume=	44,220 cf
Outflow =	9.53 cfs @ 12.17 hrs, Volume=	40,976 cf, Atten= 2%, Lag= 1.5 min
Discarded =	0.06 cfs @ 12.17 hrs, Volume=	4,599 cf
Primary =	9.46 cfs @ 12.17 hrs, Volume=	36,376 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 55.64' @ 12.17 hrs Surf.Area= 5,028 sf Storage= 4,368 cf

Plug-Flow detention time= 69.6 min calculated for 40,975 cf (93% of inflow) Center-of-Mass det. time= 29.2 min (818.9 - 789.7)

Volume	Invert	Avail.Sto	orage Storag	e Description	
#1	54.70'	4,6	75 cf STOR	M WATER WETLA	ND (Prismatic)Listed below (Recalc)
Elevatio		ırf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
54.7	-	4,273	0	0	
55.7	0	5,077	4,675	4,675	
Device	Routing	Invert	Outlet Devid	ces	
#1	Discarded	54.70'	0.520 in/hr	Exfiltration over S	urface area
#2	Primary	55.40'	Head (feet) 2.50 3.00	0.20 0.40 0.60 0 sh) 2.69 2.72 2.7	ad-Crested Rectangular Weir .80 1.00 1.20 1.40 1.60 1.80 2.00 5 2.85 2.98 3.08 3.20 3.28 3.31

Discarded OutFlow Max=0.06 cfs @ 12.17 hrs HW=55.64' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.06 cfs)

Primary OutFlow Max=9.46 cfs @ 12.17 hrs HW=55.64' (Free Discharge) **2=Broad-Crested Rectangular Weir** (Weir Controls 9.46 cfs @ 1.32 fps)

Summary for Pond DMH-D1: DMH-D1

Inflow Area	a =	41,615 sf, 47.08% Impervious, Inflow Depth > 4.46" for 100 Year ev	/ent
Inflow	=	3.53 cfs @ 12.15 hrs, Volume= 15,483 cf	
Outflow	=	3.53 cfs @ 12.15 hrs, Volume= 15,483 cf, Atten= 0%, Lag= 0.0	min
Primary	=	3.53 cfs @ 12.15 hrs, Volume= 15,483 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

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Peak Elev= 58.80' @ 12.15 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.61'	15.0" Round Culvert L= 189.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $57.61' / 56.65' \text{ S} = 0.0051 '/' \text{ Cc} = 0.900$ n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=3.53 cfs @ 12.15 hrs HW=58.80' (Free Discharge) 1=Culvert (Inlet Controls 3.53 cfs @ 2.93 fps)

Summary for Pond DMH-D2: DMH-D2

Inflow Area	=	143,310 sf	, 32.16% Impervious,	Inflow Depth > 3.4	6" for 100 Year event
Inflow =	=	9.11 cfs @	12.14 hrs, Volume=	41,268 cf	
Outflow =	=	9.11 cfs @	12.14 hrs, Volume=	41,268 cf, A	tten= 0%, Lag= 0.0 min
Primary =	=	9.11 cfs @	12.14 hrs, Volume=	41,268 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.82' @ 12.14 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.23'	18.0" Round Culvert L= 22.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.23' / 56.12' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=9.10 cfs @ 12.14 hrs HW=58.81' (Free Discharge) **1=Culvert** (Inlet Controls 9.10 cfs @ 5.15 fps)

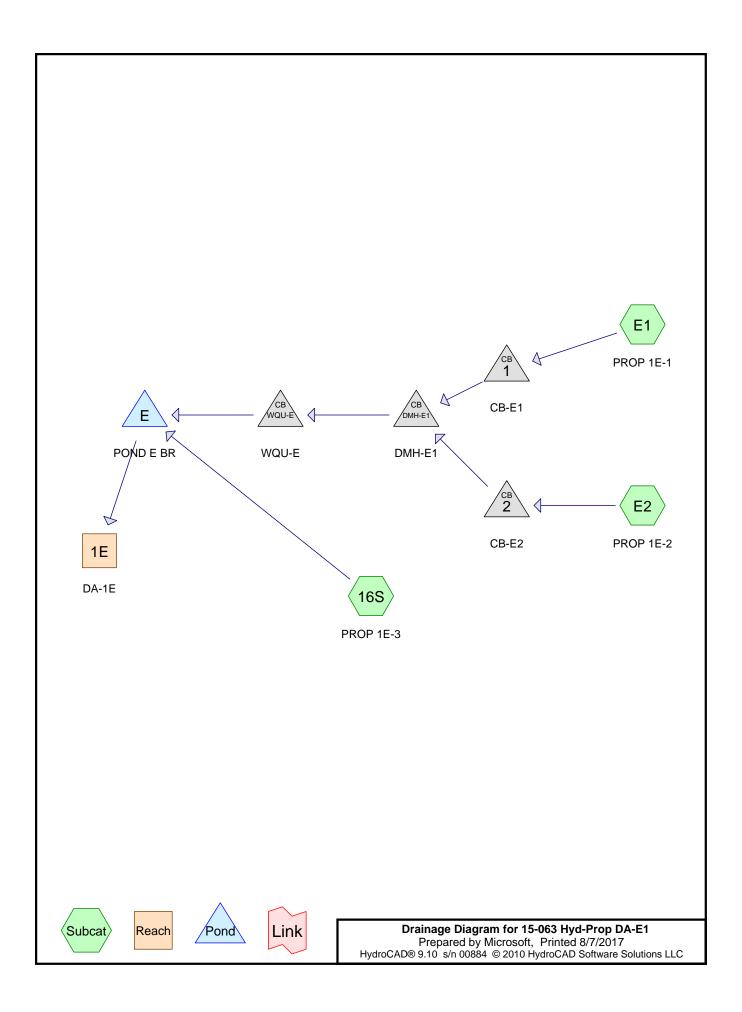
Summary for Pond WQU-D: WQU-D

Inflow Area	a =	143,310 sf, 32.16% Impervious, Inflow Depth > 3.46" for 100 Year ev	/ent
Inflow	=	9.11 cfs @ 12.14 hrs, Volume= 41,268 cf	
Outflow	=	0.11 cfs @ 12.14 hrs, Volume= 41,268 cf, Atten= 0%, Lag= 0.0	min
Primary	=	9.11 cfs @ 12.14 hrs, Volume= 41,268 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 59.10' @ 12.14 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.12'	18.0" Round Culvert L= 148.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $56.12' / 55.70'$ S= 0.0028 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=9.10 cfs @ 12.14 hrs HW=59.10' (Free Discharge) ←1=Culvert (Barrel Controls 9.10 cfs @ 5.15 fps)



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Area Listing (all nodes)

Area (sq-ft)	CN	Description (subcatchment-numbers)
17,130	39	>75% Grass cover, Good, HSG A (16S)
20,342	76	Gravel roads, HSG A (E1, E2)
12,988	98	Paved parking, HSG A (E1, E2)
8,369	98	Roofs, HSG A (16S, E1, E2)

Summary for Subcatchment 16S: PROP 1E-3

Runoff = 0.12 cfs @ 12.06 hrs, Volume= 400 cf, Depth> 0.26"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

_	A	rea (sf)	CN	Description					
		1,675	98	Roofs, HSC	βA				
		17,130	39	>75% Gras	s cover, Go	od, HSG A			
		18,805	44	Weighted A	verage				
		17,130	39	91.09% Pe	rvious Area				
		1,675	98	8.91% Impe	ervious Area	а			
	Тс	Length	Slop		Capacity	Description			
_	(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)				
	4.3	50	0.100	0 0.19		Sheet Flow,			
						Grass: Dense	n= 0.240	P2= 3.20"	

Summary for Subcatchment E1: PROP 1E-1

Runoff = 0.85 cfs @ 12.13 hrs, Volume= 3,228 cf, Depth> 1.99"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

A	rea (sf)	CN	Description		
	6,487	98	Paved park	ing, HSG A	N Contraction of the second seco
	3,422	98	Roofs, HSG	6 A	
	9,583	76	Gravel road	ls, HSG A	
	19,492	87	Weighted A	verage	
	9,583	76	49.16% Pe	rvious Area	
	9,909	98	50.84% Imp	pervious Ar	ea
Tc	Length	Slope	e Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.2	50	0.0200	0.10		Sheet Flow,
					Grass: Dense n= 0.240 P2= 3.20"
1.2	145	0.0100	2.03		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
9.4	195	Total			

Summary for Subcatchment E2: PROP 1E-2

Runoff = 0.87 cfs @ 12.13 hrs, Volume= 3,301 cf, Depth> 1.93"

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Type III 24-hr 2 Year Rainfall=3.10" Printed 8/7/2017 Page 4

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_	A	rea (sf)	CN	Description		
		6,501	98	Paved park	ing, HSG A	A line line line line line line line line
		3,272	98	Roofs, HSC	θĂ	
_		10,759	76	Gravel road	ls, HSG A	
		20,532	86	Weighted A	verage	
		10,759	76	52.40% Pei	vious Area	l de la constante de
		9,773	98	47.60% Imp	pervious Ar	ea
	_					– 1.4
	Tc	Length	Slope		Capacity	Description
_	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)	
	8.2	50	0.0200	0.10		Sheet Flow,
						Grass: Dense n= 0.240 P2= 3.20"
	1.1	140	0.0100) 2.03		Shallow Concentrated Flow,
_						Paved Kv= 20.3 fps
			-			

9.3 190 Total

Summary for Reach 1E: DA-1E

Inflow Are	a =	58,829 sf, 36.30% Impervious	Inflow Depth = 0.81"	for 2 Year event
Inflow	=	1.74 cfs @ 12.15 hrs, Volume=	3,995 cf	
Outflow	=	1.74 cfs @ 12.15 hrs, Volume=	3,995 cf, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Pond 1: CB-E1

Inflow Area =	19,492 sf, 50.84% Impervious,	Inflow Depth > 1.99" for 2 Year event
Inflow =	0.85 cfs @ 12.13 hrs, Volume=	3,228 cf
Outflow =	0.85 cfs @ 12.13 hrs, Volume=	3,228 cf, Atten= 0%, Lag= 0.0 min
Primary =	0.85 cfs @ 12.13 hrs, Volume=	3,228 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.08' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.50'	12.0" Round Culvert L= 14.5' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.50' / 57.40' S= 0.0069 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.85 cfs @ 12.13 hrs HW=58.08' (Free Discharge) —1=Culvert (Barrel Controls 0.85 cfs @ 2.56 fps)

Summary for Pond 2: CB-E2

Inflow Area =	20,532 sf, 47.60% Impervious,	Inflow Depth > 1.93" for 2 Year event
Inflow =	0.87 cfs @ 12.13 hrs, Volume=	3,301 cf
Outflow =	0.87 cfs @ 12.13 hrs, Volume=	3,301 cf, Atten= 0%, Lag= 0.0 min
Primary =	0.87 cfs @ 12.13 hrs, Volume=	3,301 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Peak Elev= 58.09' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.50'	12.0" Round Culvert L= 11.5' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.50' / 57.40' S= 0.0087 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.87 cfs @ 12.13 hrs HW=58.09' (Free Discharge) -1=Culvert (Barrel Controls 0.87 cfs @ 2.62 fps)

Summary for Pond DMH-E1: DMH-E1

Inflow Area	a =	40,024 sf	, 49.18% Impervious,	Inflow Depth > 1.9	96" for 2 Year event
Inflow	=	1.72 cfs @	12.13 hrs, Volume=	6,529 cf	
Outflow	=	1.72 cfs @	12.13 hrs, Volume=	6,529 cf, 7	Atten= 0%, Lag= 0.0 min
Primary	=	1.72 cfs @	12.13 hrs, Volume=	6,529 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.06' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.30'	18.0" Round Culvert L= 20.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.30' / 57.20' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.72 cfs @ 12.13 hrs HW=58.06' (Free Discharge) -1=Culvert (Barrel Controls 1.72 cfs @ 2.80 fps)

Summary for Pond E: POND E BR

Inflow Area =	58,829 sf, 36.30% Impervious,	Inflow Depth > 1.41" for 2 Year event
Inflow =	1.81 cfs @ 12.12 hrs, Volume=	6,929 cf
Outflow =	1.76 cfs @ 12.15 hrs, Volume=	5,636 cf, Atten= 2%, Lag= 1.4 min
Discarded =	0.03 cfs @ 12.15 hrs, Volume=	1,641 cf
Primary =	1.74 cfs @ 12.15 hrs, Volume=	3,995 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 56.55' @ 12.15 hrs Surf.Area= 2,090 sf Storage= 1,507 cf

Plug-Flow detention time= 109.1 min calculated for 5,633 cf (81% of inflow) Center-of-Mass det. time= 33.5 min (819.0 - 785.5)

Volume	Invert	Avail.Storage	e Storage	Description	
#1	55.75'	1,933 c	STORM	WATER WETLAN	ND (Prismatic)Listed below (Recalc)
Elevation (feet)			nc.Store bic-feet)	Cum.Store (cubic-feet)	
55.75 56.75		l,671 2,194	0 1,933	0 1.933	

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Device	Routing	Invert	Outlet Devices
#1	Discarded	55.75'	0.520 in/hr Exfiltration over Surface area
#2	Primary	56.45'	20.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32

Discarded OutFlow Max=0.03 cfs @ 12.15 hrs HW=56.55' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.03 cfs)

Primary OutFlow Max=1.74 cfs @ 12.15 hrs HW=56.55' (Free Discharge) **2=Broad-Crested Rectangular Weir** (Weir Controls 1.74 cfs @ 0.86 fps)

Summary for Pond WQU-E: WQU-E

Inflow Area	a =	40,024 sf, 49.18% Impervious, Inflow Depth > 1.96" for 2 Year event
Inflow	=	1.72 cfs @ 12.13 hrs, Volume= 6,529 cf
Outflow	=	1.72 cfs @ 12.13 hrs, Volume= 6,529 cf, Atten= 0%, Lag= 0.0 min
Primary	=	1.72 cfs @ 12.13 hrs, Volume= 6,529 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.78' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.10'	18.0" Round Culvert L= 130.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $57.10' / 56.40'$ S= 0.0054 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.72 cfs @ 12.13 hrs HW=57.78' (Free Discharge) -1=Culvert (Barrel Controls 1.72 cfs @ 3.24 fps) HydroCAD® 9.10 s/n 00884 © 2010 HydroCAD Software Solutions LLC

Summary for Subcatchment 16S: PROP 1E-3

Runoff = 0.19 cfs @ 12.06 hrs, Volume= 827 cf, Depth> 0.53"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

A	rea (sf)	CN	Description					
	1,675	98	Roofs, HSG	βA				
	17,130	39	>75% Gras	s cover, Go	od, HSG A			
	18,805	44	Weighted A	verage				
	17,130	39	91.09% Per	vious Area				
	1,675	98	8.91% Impe	ervious Area	а			
Тс	Longth	Slop	e Velocity	Capacity	Description			
(min)	Length (feet)	(ft/f		(cfs)	Description			
4.3	50	0.100	0 0.19		Sheet Flow,			
					Grass: Dense	n= 0.240	P2= 3.20"	

Summary for Subcatchment E1: PROP 1E-1

Runoff = 1.46 cfs @ 12.13 hrs, Volume= 5,507 cf, Depth> 3.39"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

A	rea (sf)	CN	Description		
	6,487	98	Paved park	ing, HSG A	N Contraction of the second
	3,422	98	Roofs, HSG	6 A	
	9,583	76	Gravel road	ls, HSG A	
	19,492	87	Weighted A	verage	
	9,583	76	49.16% Pei	rvious Area	
	9,909	98	50.84% Imp	pervious Ar	ea
Tc	Length	Slope	e Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.2	50	0.0200	0.10		Sheet Flow,
					Grass: Dense n= 0.240 P2= 3.20"
1.2	145	0.0100	2.03		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
9.4	195	Total			

Summary for Subcatchment E2: PROP 1E-2

Runoff = 1.51 cfs @ 12.13 hrs, Volume= 5,680 cf, Depth> 3.32"

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_	A	rea (sf)	CN	Description		
		6,501	98	Paved park	ing, HSG A	N
		3,272	98	Roofs, HSC	θĂ.	
		10,759	76	Gravel road	ls, HSG A	
		20,532	86	Weighted A	verage	
		10,759	76	52.40% Pei	rvious Area	
		9,773	98	47.60% Imp	pervious Ar	ea
	Тс	Length	Slope	e Velocity	Capacity	Description
	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)	
	8.2	50	0.0200	0.10		Sheet Flow,
						Grass: Dense n= 0.240 P2= 3.20"
	1.1	140	0.0100	2.03		Shallow Concentrated Flow,
						Paved Kv= 20.3 fps

9.3 190 Total

Summary for Reach 1E: DA-1E

Inflow Are	a =	58,829 sf, 36.30% Impervious,	Inflow Depth > 1.82"	for 10 Year event
Inflow	=	3.03 cfs @ 12.14 hrs, Volume=	8,926 cf	
Outflow	=	3.03 cfs @ 12.14 hrs, Volume=	8,926 cf, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Pond 1: CB-E1

Inflow Area	a =	19,492 sf	, 50.84% Impervious,	Inflow Depth > 3.39	for 10 Year event
Inflow	=	1.46 cfs @	12.13 hrs, Volume=	5,507 cf	
Outflow	=	1.46 cfs @	12.13 hrs, Volume=	5,507 cf, Att	ten= 0%, Lag= 0.0 min
Primary	=	1.46 cfs @	12.13 hrs, Volume=	5,507 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.31' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.50'	12.0" Round Culvert L= 14.5' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.50' / 57.40' S= 0.0069 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.46 cfs @ 12.13 hrs HW=58.31' (Free Discharge) **1=Culvert** (Barrel Controls 1.46 cfs @ 2.92 fps)

Summary for Pond 2: CB-E2

Inflow Area	=	20,532 sf,	47.60% Impervious,	Inflow Depth > 3.32"	for 10 Year event
Inflow =	=	1.51 cfs @	12.13 hrs, Volume=	5,680 cf	
Outflow =	=	1.51 cfs @	12.13 hrs, Volume=	5,680 cf, Atter	n= 0%, Lag= 0.0 min
Primary =	=	1.51 cfs @	12.13 hrs, Volume=	5,680 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

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Peak Elev= 58.32' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.50'	12.0" Round Culvert L= 11.5' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.50' / 57.40' S= 0.0087 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.51 cfs @ 12.13 hrs HW=58.32' (Free Discharge) **1=Culvert** (Barrel Controls 1.51 cfs @ 2.98 fps)

Summary for Pond DMH-E1: DMH-E1

Inflow Area	a =	40,024 sf	, 49.18% Impervious,	Inflow Depth > 3.3	5" for 10 Year event
Inflow	=	2.97 cfs @	12.13 hrs, Volume=	11,187 cf	
Outflow	=	2.97 cfs @	12.13 hrs, Volume=	11,187 cf, A	tten= 0%, Lag= 0.0 min
Primary	=	2.97 cfs @	12.13 hrs, Volume=	11,187 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.34' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.30'	18.0" Round Culvert L= 20.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.30' / 57.20' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=2.97 cfs @ 12.13 hrs HW=58.34' (Free Discharge) -1=Culvert (Barrel Controls 2.97 cfs @ 3.20 fps)

Summary for Pond E: POND E BR

Inflow Area =	58,829 sf, 36.30% Impervious,	Inflow Depth > 2.45" for 10 Year event
Inflow =	3.11 cfs @ 12.12 hrs, Volume=	12,014 cf
Outflow =	3.05 cfs @ 12.14 hrs, Volume=	10,711 cf, Atten= 2%, Lag= 1.2 min
Discarded =	0.03 cfs @ 12.14 hrs, Volume=	1,785 cf
Primary =	3.03 cfs @ 12.14 hrs, Volume=	8,926 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 56.60' @ 12.14 hrs Surf.Area= 2,114 sf Storage= 1,603 cf

Plug-Flow detention time= 81.2 min calculated for 10,711 cf (89% of inflow) Center-of-Mass det. time= 27.9 min (811.4 - 783.5)

Volume	Invert	Avail.Storag	ge Storage	Description	
#1	55.75'	1,933	cf STORM	WATER WETLA	ND (Prismatic)Listed below (Recalc)
Elevation (feet)			Inc.Store ubic-feet)	Cum.Store (cubic-feet)	
55.75 56.75		l,671 2,194	0 1,933	0 1,933	

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Device	Routing	Invert	Outlet Devices
#1 #2	Discarded Primary		0.520 in/hr Exfiltration over Surface area 20.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 <td< td=""></td<>
			Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32

Discarded OutFlow Max=0.03 cfs @ 12.14 hrs HW=56.60' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.03 cfs)

Primary OutFlow Max=3.02 cfs @ 12.14 hrs HW=56.60' (Free Discharge) **2=Broad-Crested Rectangular Weir** (Weir Controls 3.02 cfs @ 1.03 fps)

Summary for Pond WQU-E: WQU-E

Inflow Area =	=	40,024 sf	, 49.18% Impervious	Inflow Depth > 3.35"	for 10 Year event
Inflow =	=	2.97 cfs @	12.13 hrs, Volume=	11,187 cf	
Outflow =	=	2.97 cfs @	12.13 hrs, Volume=	11,187 cf, Atte	en= 0%, Lag= 0.0 min
Primary =	=	2.97 cfs @	12.13 hrs, Volume=	11,187 cf	-

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.03' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.10'	18.0" Round Culvert L= 130.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.10' / 56.40' S= 0.0054 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=2.97 cfs @ 12.13 hrs HW=58.03' (Free Discharge) -1=Culvert (Barrel Controls 2.97 cfs @ 3.68 fps)

Summary for Subcatchment 16S: PROP 1E-3

Runoff = 0.75 cfs @ 12.08 hrs, Volume= 2,956 cf, Depth> 1.89"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

A	Area (sf)	CN	Description					
	1,675	98	Roofs, HSG	βA				
	17,130	39	>75% Grass	s cover, Go	od, HSG A			
	18,805	44	Weighted A	verage				
	17,130	39	91.09% Per	vious Area				
	1,675	98	8.91% Impe	ervious Area	а			
Tc (min)	Length (feet)	Slop (ft/f		Capacity (cfs)	Description			
4.3	50	0.100	0 0.19		Sheet Flow, Grass: Dense	n= 0.240	P2= 3.20"	

Summary for Subcatchment E1: PROP 1E-1

Runoff = 2.90 cfs @ 12.13 hrs, Volume= 10,974 cf, Depth> 6.76"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

A	rea (sf)	CN	Description		
	6,487	98	Paved park	ing, HSG A	N Contraction of the second seco
	3,422	98	Roofs, HSG	6 A	
	9,583	76	Gravel road	ls, HSG A	
	19,492	87	Weighted A	verage	
	9,583	76	49.16% Pe	rvious Area	
	9,909	98	50.84% Imp	pervious Ar	ea
Tc	Length	Slope	e Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.2	50	0.0200	0.10		Sheet Flow,
					Grass: Dense n= 0.240 P2= 3.20"
1.2	145	0.0100	2.03		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
9.4	195	Total			

Summary for Subcatchment E2: PROP 1E-2

Runoff = 3.04 cfs @ 12.13 hrs, Volume= 11,415 cf, Depth> 6.67"

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Type III 24-hr 100 Year Rainfall=8.30" Printed 8/7/2017 HydroCAD® 9.10 s/n 00884 © 2010 HydroCAD Software Solutions LLC Page 12

6,501 98 Paved parking, HSG A 3,272 98 Roofs, HSG A 10,759 76 Gravel roads, HSG A 20,532 86 Weighted Average 10,759 76 52.40% Pervious Area 9,773 98 47.60% Impervious Area 9,773 98 47.60% Impervious Area 0,759 76 52.40% Pervious Area 9,773 98 47.60% Impervious Area 0,759 8.2 50 0.0200 0.10 Sheet Flow, Grass: Dense n= 0.240 P2= 3.20" 1.1 140 0.0100 2.03 Shallow Concentrated Flow, Paved Ky= 20.3 fps Flow,	 А	rea (sf)	CN	Description		
10,759 76 Gravel roads, HSG A 20,532 86 Weighted Average 10,759 76 52.40% Pervious Area 9,773 98 47.60% Impervious Area Tc Length Slope Velocity Capacity (min) (feet) (ft/ft) (ft/sec) (cfs) 8.2 50 0.0200 0.10 Sheet Flow, Grass: Dense n= 0.240 P2= 3.20" 1.1 140 0.0100 2.03 Shallow Concentrated Flow,		6,501	98	Paved park	ing, HSG A	\
20,532 86 Weighted Average 10,759 76 52.40% Pervious Area 9,773 98 47.60% Impervious Area Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs) 8.2 50 0.0200 0.10 Sheet Flow, Grass: Dense n= 0.240 P2= 3.20" 1.1 140 0.0100 2.03 Shallow Concentrated Flow,		3,272	98	Roofs, HSC	βĂ	
10,759 76 52.40% Pervious Area 9,773 98 47.60% Impervious Area Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs) 8.2 50 0.0200 0.10 Sheet Flow, Grass: Dense n= 0.240 P2= 3.20" 1.1 140 0.0100 2.03 Shallow Concentrated Flow,		10,759	76	Gravel roac	ls, HSG A	
9,7739847.60% Impervious AreaTcLengthSlopeVelocityCapacityDescription(min)(feet)(ft/ft)(ft/sec)(cfs)8.2500.02000.10Sheet Flow, Grass: Dense n= 0.240 P2= 3.20"1.11400.01002.03Shallow Concentrated Flow,		20,532	86	Weighted A	verage	
TcLengthSlopeVelocityCapacity (cfs)Description(min)(feet)(ft/ft)(ft/sec)(cfs)8.2500.02000.10Sheet Flow, Grass: Dense n= 0.240 P2= 3.20"1.11400.01002.03Shallow Concentrated Flow,		10,759	76	52.40% Pei	vious Area	
(min) (feet) (ft/ft) (ft/sec) (cfs) 8.2 50 0.0200 0.10 Sheet Flow, Grass: Dense n= 0.240 P2= 3.20" 1.1 140 0.0100 2.03 Shallow Concentrated Flow,		9,773	98	47.60% Imp	pervious Ar	ea
(min) (feet) (ft/ft) (ft/sec) (cfs) 8.2 50 0.0200 0.10 Sheet Flow, Grass: Dense n= 0.240 P2= 3.20" 1.1 140 0.0100 2.03 Shallow Concentrated Flow,	_		-		- ·	
8.2 50 0.0200 0.10 Sheet Flow, Grass: Dense n= 0.240 P2= 3.20" 1.1 140 0.0100 2.03 Shallow Concentrated Flow,		0				Description
1.11400.01002.03Grass: Densen= 0.240P2= 3.20"Shallow Concentrated Flow,	 (min)	(feet)	(ft/ft	(ft/sec)	(cfs)	
1.1 140 0.0100 2.03 Shallow Concentrated Flow,	8.2	50	0.0200	0.10		Sheet Flow,
·						Grass: Dense n= 0.240 P2= 3.20"
Paved Ky= 20.3 fps	1.1	140	0.0100	2.03		Shallow Concentrated Flow,
						Paved Kv= 20.3 fps

9.3 190 Total

Summary for Reach 1E: DA-1E

Inflow Are	a =	58,829 sf, 36.30% Imperviou	s, Inflow Depth > 4.51"	for 100 Year event
Inflow	=	6.48 cfs @ 12.14 hrs, Volume	= 22,103 cf	
Outflow	=	6.48 cfs @ 12.14 hrs, Volume	= 22,103 cf, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Pond 1: CB-E1

Inflow Area =	19,492 sf, 50.84% Imperviou	us, Inflow Depth > 6.76" for 100 Year event
Inflow =	2.90 cfs @ 12.13 hrs, Volume	e= 10,974 cf
Outflow =	2.90 cfs @ 12.13 hrs, Volume	e= 10,974 cf, Atten= 0%, Lag= 0.0 min
Primary =	2.90 cfs @ 12.13 hrs, Volume	e= 10,974 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.94' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
	Primary	57.50'	12.0" Round Culvert L= 14.5' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.50' / 57.40' S= 0.0069 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=2.90 cfs @ 12.13 hrs HW=58.94' (Free Discharge) **1=Culvert** (Inlet Controls 2.90 cfs @ 3.69 fps)

Summary for Pond 2: CB-E2

Inflow Area =	20,532 sf, 47.60% Impervious,	Inflow Depth > 6.67" for 100 Year event
Inflow =	3.04 cfs @ 12.13 hrs, Volume=	11,415 cf
Outflow =	3.04 cfs @ 12.13 hrs, Volume=	11,415 cf, Atten= 0%, Lag= 0.0 min
Primary =	3.04 cfs @ 12.13 hrs, Volume=	11,415 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

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Peak Elev= 59.03' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices	
	Primary	57.50'	12.0" Round Culvert L= 11.5' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.50' / 57.40' S= 0.0087 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior	

Primary OutFlow Max=3.03 cfs @ 12.13 hrs HW=59.03' (Free Discharge) **1=Culvert** (Inlet Controls 3.03 cfs @ 3.86 fps)

Summary for Pond DMH-E1: DMH-E1

Inflow Area	=	40,024 sf	, 49.18% Impervious,	Inflow Depth > 6.71"	for 100 Year event
Inflow :	=	5.93 cfs @	12.13 hrs, Volume=	22,389 cf	
Outflow :	=	5.93 cfs @	12.13 hrs, Volume=	22,389 cf, Atter	= 0%, Lag= 0.0 min
Primary :	=	5.93 cfs @	12.13 hrs, Volume=	22,389 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.92' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices	
#1	Primary	57.30'	18.0" Round Culvert L= 20.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.30' / 57.20' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior	

Primary OutFlow Max=5.93 cfs @ 12.13 hrs HW=58.92' (Free Discharge) -1=Culvert (Barrel Controls 5.93 cfs @ 3.86 fps)

Summary for Pond E: POND E BR

Inflow Area =	58,829 sf, 36.30% Impervious,	Inflow Depth > 5.17" for 100 Year event
Inflow =	6.58 cfs @ 12.12 hrs, Volume=	25,345 cf
Outflow =	6.51 cfs @ 12.14 hrs, Volume=	24,026 cf, Atten= 1%, Lag= 0.9 min
Discarded =	0.03 cfs @ 12.14 hrs, Volume=	1,923 cf
Primary =	6.48 cfs @ 12.14 hrs, Volume=	22,103 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 56.69' @ 12.14 hrs Surf.Area= 2,164 sf Storage= 1,809 cf

Plug-Flow detention time= 51.1 min calculated for 24,026 cf (95% of inflow) Center-of-Mass det. time= 21.4 min (801.4 - 779.9)

Volume	Invert	Avail.Stor	age Storage	Description	
#1	55.75'	1,93	3 cf STORM	STORM WATER WETLAND (Prismatic)Listed below (Re	
Elevation (feet)		.Area sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
55.75 56.75		1,671 2,194	0 1,933	0 1,933	

Device	Routing	Invert	Outlet Devices
#1	Discarded	55.75'	0.520 in/hr Exfiltration over Surface area
#2	Primary	56.45'	20.0' long x 1.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00

Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32

Discarded OutFlow Max=0.03 cfs @ 12.14 hrs HW=56.69' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.03 cfs)

Primary OutFlow Max=6.47 cfs @ 12.14 hrs HW=56.69' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 6.47 cfs @ 1.33 fps)

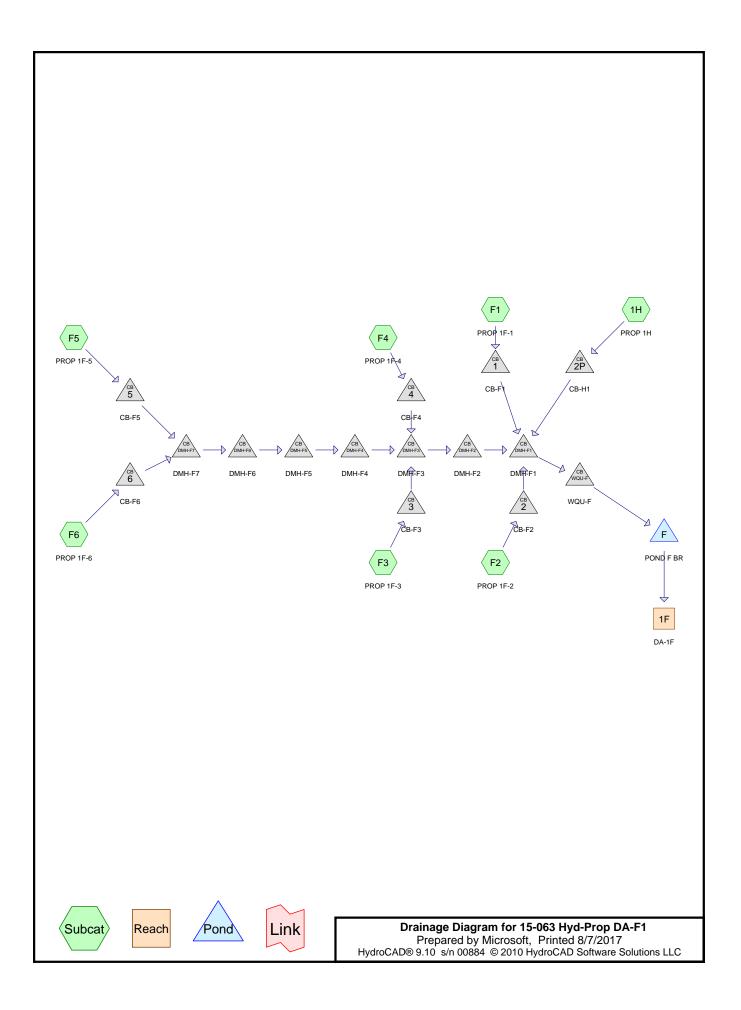
Summary for Pond WQU-E: WQU-E

Inflow Are	a =	40,024 sf, 49.18% Impervious, Inflow Depth > 6.71" for 100 Year event
Inflow	=	5.93 cfs @ 12.13 hrs, Volume= 22,389 cf
Outflow	=	5.93 cfs @ 12.13 hrs, Volume= 22,389 cf, Atten= 0%, Lag= 0.0 min
Primary	=	5.93 cfs @ 12.13 hrs, Volume= 22,389 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.63' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices	
#1	Primary	57.10'	18.0" Round Culvert L= 130.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $57.10' / 56.40'$ S= 0.0054 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior	

Primary OutFlow Max=5.93 cfs @ 12.13 hrs HW=58.63' (Free Discharge) **1=Culvert** (Inlet Controls 5.93 cfs @ 3.35 fps)



Area Listing (all nodes)

Area (sq-ft)	CN	Description (subcatchment-numbers)	
79,755	30	Meadow, non-grazed, HSG A (1H)	
115,754	39	>75% Grass cover, Good, HSG A (1H, F1, F2, F4, F5, F6)	
30,381	98	Paved parking, HSG A (F1, F2, F3, F4, F5, F6)	
20,742	98	Roofs, HSG A (1H, F1, F2)	

Summary for Subcatchment 1H: PROP 1H

Runoff = 0.53 cfs @ 12.28 hrs, Volume= 2,748 cf, Depth> 0.21"

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Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

_	A	rea (sf)	CN	Description				
		11,533	98	98 Roofs, HSG A				
		68,069	39	>75% Gras	s cover, Go	bod, HSG A		
_		79,755	30	Meadow, no	on-grazed,	HSG A		
159,357 39 Weighted Average					verage			
	147,824 34 92.76% Pervious Area				vious Area			
	11,533 98 7.24% Impervious Area			7.24% Impe	ervious Are	a		
	_		-		- ·			
	Tc	Length	Slope		Capacity	Description		
_	(min)	(feet)	(ft/ft) (ft/sec)	(cfs)			
	6.6	50	0.0100	0.13		Sheet Flow,		
						Range n= 0.130 P2= 3.20"		
	14.9	600	0.0020	0.67		Shallow Concentrated Flow,		
						Grassed Waterway Kv= 15.0 fps		
_	21.5	650	Total					

21.5 650 Total

Summary for Subcatchment F1: PROP 1F-1

Runoff = 0.93 cfs @ 12.13 hrs, Volume= 3,623 cf, Depth> 1.10"

A	rea (sf)	CN	Description				
	9,051	98	Paved park	ing, HSG A	N		
	6,129	98	Roofs, HSO	βA			
	24,232	39	>75% Gras	s cover, Go	bod, HSG A		
	39,412	62	62 Weighted Average				
	24,232	39	61.48% Pei	vious Area			
	15,180	98	38.52% Imp	pervious Ar	ea		
Тс	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	· · · · · · · · · · · · · · · · · · ·		
8.2	50	0.0200	0.10		Sheet Flow,		
					Grass: Dense n= 0.240 P2= 3.20"		
1.4	170	0.0100	2.03		Shallow Concentrated Flow,		
					Paved Kv= 20.3 fps		
9.6	220	Total					

Summary for Subcatchment F2: PROP 1F-2

Runoff = 0.71 cfs @ 12.13 hrs, Volume= 2,746 cf, Depth> 1.62"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

_	A	rea (sf)	CN	N Description					
		8,426	98	Paved park	Paved parking, HSG A				
		3,080	98	Roofs, HSC	θĂ				
_		8,820	39	>75% Gras	s cover, Go	bod, HSG A			
		20,326	72	Weighted A	verage				
		8,820	39	43.39% Pe	rvious Area	l			
		11,506	98	56.61% Im	pervious Ar	ea			
	Tc	Length	Slop		Capacity	Description			
_	(min)	(feet)	(ft/ft	t) (ft/sec)	(cfs)				
	8.2	50	0.020	0 0.10		Sheet Flow,			
						Grass: Dense n= 0.240 P2= 3.20"			
	1.2	150	0.010	0 2.03		Shallow Concentrated Flow,			
_						Paved Kv= 20.3 fps			
	0.1	200	Total						

9.4 200 Total

Summary for Subcatchment F3: PROP 1F-3

Runoff = 0.26 cfs @ 12.03 hrs, Volume= 786 cf, Depth> 2.87"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

Α	rea (sf)	CN	Description		
	3,290	98	Paved park	ing, HSG A	N Contraction of the second seco
	3,290	98	100.00% In	npervious A	vrea
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description
0.7	50	0.0200	1.20	· · · ·	Sheet Flow,
1.4	170	0.0100	2.03	Smooth surfaces n= 0.011 P2= 3.20" Shallow Concentrated Flow, Paved Kv= 20.3 fps	
0.4	220	Tatal			

2.1 220 Total

Summary for Subcatchment F4: PROP 1F-4

Runoff = 0.21 cfs @ 12.07 hrs, Volume= 696 cf, Depth> 0.66"

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Type III 24-hr 2 Year Rainfall=3.10" Printed 8/7/2017 Page 5

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A	rea (sf)	CN E	Description					
	2,914	98 F	98 Paved parking, HSG A					
	9,663	39 >	75% Gras	s cover, Go	ood, HSG A			
	12,577	53 V	Veighted A	verage				
	9,663	39 7	6.83% Per	vious Area				
	2,914	98 2	3.17% Imp	pervious Are	ea			
_		<u>.</u>		•				
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
4.5	50	0.2500	0.19		Sheet Flow,			
					Woods: Light underbrush n= 0.400 P2= 3.20"			
0.2	30	0.2000	2.24		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
0.2	70	0.0800	5.74		Shallow Concentrated Flow,			
					Paved Kv= 20.3 fps			
4.9	150	Total						

Summary for Subcatchment F5: PROP 1F-5

Runoff = 0.25 cfs @ 12.06 hrs, Volume= 800 cf, Depth> 1.41"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 2 Year Rainfall=3.10"

A	rea (sf)	CN E	Description					
	3,350	98 F	98 Paved parking, HSG A					
	3,450	39 >	75% Gras	s cover, Go	bod, HSG A	_		
	6,800	68 V	68 Weighted Average					
	3,450	39 5	39 50.74% Pervious Area					
	3,350	98 4	9.26% Imp	pervious Ar	ea			
_								
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		_		
3.0	50	0.2500	0.28		Sheet Flow,			
					Grass: Dense n= 0.240 P2= 3.20"			
1.0	170	0.0200	2.87		Shallow Concentrated Flow,			
					Paved Kv= 20.3 fps	_		
4.0	220	Total						

Summary for Subcatchment F6: PROP 1F-6

Runoff = 0.27 cfs @ 12.02 hrs, Volume= 800 cf, Depth> 1.97"

15-063 Hyd-Prop DA-F1

Type III 24-hr 2 Year Rainfall=3.10" Printed 8/7/2017 Page 6

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	A	rea (sf)	CN	Description					
		3,350	98	98 Paved parking, HSG A					
		1,520	39	>75% Gras	s cover, Go	bod, HSG A			
		4,870	80	80 Weighted Average					
		1,520	39	5 F					
		3,350	98	98 68.79% Impervious Area					
	Тс	Length	Slop		Capacity	Description			
-	(min)	(feet)	(ft/ft	t) (ft/sec)	(cfs)				
	0.7	50	0.020	0 1.20		Sheet Flow,			
						Smooth surfaces n= 0.011 P2= 3.20"			
	0.8	140	0.020	0 2.87		Shallow Concentrated Flow,			
_						Paved Kv= 20.3 fps			
	1 E	100	Total						

1.5 190 Total

Summary for Reach 1F: DA-1F

Inflow Are	a =	246,632 sf, 20.73% Impervious	, Inflow Depth = 0.30 "	for 2 Year event
Inflow	=	2.51 cfs @ 12.14 hrs, Volume=	6,257 cf	
Outflow	=	2.51 cfs @ 12.14 hrs, Volume=	6,257 cf, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Pond 1: CB-F1

Inflow Area	a =	39,412 sf, 38.52% Impervious, Inflow Depth > 1.10" for 2 Year e	vent
Inflow	=	0.93 cfs @ 12.13 hrs, Volume= 3,623 cf	
Outflow	=	0.93 cfs @ 12.13 hrs, Volume= 3,623 cf, Atten= 0%, Lag= (0.0 min
Primary	=	0.93 cfs @ 12.13 hrs, Volume= 3,623 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.62' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.00'	12.0" Round Culvert
			L= 16.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.00' / 56.90' S= 0.0063 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.93 cfs @ 12.13 hrs HW=57.62' (Free Discharge) -1=Culvert (Barrel Controls 0.93 cfs @ 2.60 fps)

Summary for Pond 2: CB-F2

Inflow Are	a =	20,326 sf, 56.61% Impervious, Inflow Depth > 1.62" for 2 Year event	
Inflow	=	0.71 cfs @ 12.13 hrs, Volume= 2,746 cf	
Outflow	=	0.71 cfs @ 12.13 hrs, Volume= 2,746 cf, Atten= 0%, Lag= 0.0 n	nin
Primary	=	0.71 cfs @ 12.13 hrs, Volume= 2,746 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Peak Elev= 57.52' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.00'	12.0" Round Culvert L= 12.5' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.00' / 56.90' S= 0.0080 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.71 cfs @ 12.13 hrs HW=57.52' (Free Discharge) 1=Culvert (Barrel Controls 0.71 cfs @ 2.49 fps)

Summary for Pond 2P: CB-H1

Inflow Area =	159,357 sf	, 7.24% Impervious,	Inflow Depth > 0.21" for 2 Year	· event
Inflow =	0.53 cfs @	12.28 hrs, Volume=	2,748 cf	
Outflow =	0.53 cfs @	12.28 hrs, Volume=	2,748 cf, Atten= 0%, Lag	= 0.0 min
Primary =	0.53 cfs @	12.28 hrs, Volume=	2,748 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.96' @ 12.28 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.50'	10.0" Round Culvert L= 115.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $57.50' / 56.90'$ S= 0.0052 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.53 cfs @ 12.28 hrs HW=57.96' (Free Discharge) ☐ 1=Culvert (Barrel Controls 0.53 cfs @ 2.49 fps)

Summary for Pond 3: CB-F3

Inflow Area	a =	3,290 sf,100	0.00% Impervious	, Inflow Depth >	2.87"	for 2 Year event
Inflow	=	0.26 cfs @ 12.	.03 hrs, Volume=	786 0	of	
Outflow	=	0.26 cfs @ 12.	.03 hrs, Volume=	786 c	of, Atter	n= 0%, Lag= 0.0 min
Primary	=	0.26 cfs @ 12.	.03 hrs, Volume=	786 c	of	-

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 59.99' @ 12.03 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	59.70'	12.0" Round Culvert L= 10.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 59.70' / 59.60' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.26 cfs @ 12.03 hrs HW=59.99' (Free Discharge) -1=Culvert (Barrel Controls 0.26 cfs @ 2.05 fps)

Summary for Pond 4: CB-F4

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 59.96' @ 12.07 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	59.70'	12.0" Round Culvert L= 9.7' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 59.70' / 59.60' S= 0.0103 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.21 cfs @ 12.07 hrs HW=59.96' (Free Discharge) **1=Culvert** (Barrel Controls 0.21 cfs @ 1.97 fps)

Summary for Pond 5: CB-F5

Inflow Are	a =	6,800 sf,	49.26% Impervious,	Inflow Depth > 1.41	for 2 Year event
Inflow	=	0.25 cfs @	12.06 hrs, Volume=	800 cf	
Outflow	=	0.25 cfs @	12.06 hrs, Volume=	800 cf, Att	en= 0%, Lag= 0.0 min
Primary	=	0.25 cfs @	12.06 hrs, Volume=	800 cf	-

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 67.98' @ 12.06 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	67.70'	12.0" Round Culvert L= 14.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 67.70' / 67.43' S= 0.0193 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.25 cfs @ 12.06 hrs HW=67.98' (Free Discharge)

Summary for Pond 6: CB-F6

Inflow Area	a =	4,870 sf,	68.79% Impervious,	Inflow Depth > 1.97"	for 2 Year event
Inflow	=	0.27 cfs @	12.02 hrs, Volume=	800 cf	
Outflow	=	0.27 cfs @	12.02 hrs, Volume=	800 cf, Atte	n= 0%, Lag= 0.0 min
Primary	=	0.27 cfs @	12.02 hrs, Volume=	800 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 67.99' @ 12.02 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	67.70'	12.0" Round Culvert
			L= 14.0' CPP, projecting, no headwall, Ke= 0.900

Inlet / Outlet Invert= 67.70' / 67.43' = 0.0193'' = Cc = 0.900n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.27 cfs @ 12.02 hrs HW=67.99' (Free Discharge)

Summary for Pond DMH-F1: DMH-F1

Inflow Area =	246,632 sf	, 20.73% Impervious,	Inflow Depth > 0.59"	for 2 Year event
Inflow =	2.64 cfs @	12.10 hrs, Volume=	12,200 cf	
Outflow =	2.64 cfs @	12.10 hrs, Volume=	12,200 cf, Atten=	= 0%, Lag= 0.0 min
Primary =	2.64 cfs @	12.10 hrs, Volume=	12,200 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.70' @ 12.10 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.80'	18.0" Round Culvert L= 20.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.80' / 56.60' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=2.64 cfs @ 12.10 hrs HW=57.70' (Free Discharge) **1=Culvert** (Barrel Controls 2.64 cfs @ 3.44 fps)

Summary for Pond DMH-F2: DMH-F2

Inflow Area =	=	27,537 sf	, 46.86% Impervious,	Inflow Depth > 1.34"	for 2 Year event
Inflow =	=	0.95 cfs @	12.04 hrs, Volume=	3,083 cf	
Outflow =	=	0.95 cfs @	12.04 hrs, Volume=	3,083 cf, Atte	en= 0%, Lag= 0.0 min
Primary =	=	0.95 cfs @	12.04 hrs, Volume=	3,083 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.12' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.60'	15.0" Round Culvert L= 56.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.60' / 56.90' S= 0.0125 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.94 cfs @ 12.04 hrs HW=58.12' (Free Discharge) **1=Culvert** (Inlet Controls 0.94 cfs @ 1.94 fps)

Summary for Pond DMH-F3: DMH-F3

Inflow Area =	= 27,537	sf, 46.86% Impervious	, Inflow Depth > 1.34	for 2 Year event
Inflow =	0.95 cfs @	2 12.04 hrs, Volume=	3,083 cf	
Outflow =	0.95 cfs @	2 12.04 hrs, Volume=	3,083 cf, Att	ten= 0%, Lag= 0.0 min
Primary =	0.95 cfs @	2 12.04 hrs, Volume=	3,083 cf	-

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 60.02' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	59.50'	15.0" Round Culvert L= 152.5' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 59.50' / 57.70' S= 0.0118 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.94 cfs @ 12.04 hrs HW=60.02' (Free Discharge) -1=Culvert (Inlet Controls 0.94 cfs @ 1.94 fps)

Summary for Pond DMH-F4: DMH-F4

Inflow Area	=	11,670 sf	, 57.41% Impervious,	Inflow Depth > 1.65"	for 2 Year event
Inflow	=	0.50 cfs @	12.03 hrs, Volume=	1,601 cf	
Outflow	=	0.50 cfs @	12.03 hrs, Volume=	1,601 cf, Atte	en= 0%, Lag= 0.0 min
Primary	=	0.50 cfs @	12.03 hrs, Volume=	1,601 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 64.52' @ 12.03 hrs

Device	Routing	Invert	Outlet Devices	
-	Primary		12.0" Round Culvert L= 91.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 64.12' / 59.60' S= 0.0497 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior	

Primary OutFlow Max=0.50 cfs @ 12.03 hrs HW=64.52' (Free Discharge) -1=Culvert (Inlet Controls 0.50 cfs @ 1.70 fps)

Summary for Pond DMH-F5: DMH-F5

Inflow Area	ι =	11,670 sf	, 57.41% Impervious,	Inflow Depth > 1.65"	for 2 Year event
Inflow	=	0.50 cfs @	12.03 hrs, Volume=	1,601 cf	
Outflow	=	0.50 cfs @	12.03 hrs, Volume=	1,601 cf, Atte	n= 0%, Lag= 0.0 min
Primary	=	0.50 cfs @	12.03 hrs, Volume=	1,601 cf	-

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 65.53' @ 12.03 hrs

Device	Routing	Invert	Outlet Devices	
#1	Primary	65.13'	12.0" Round Culvert L= 91.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 65.13' / 64.22' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior	

Primary OutFlow Max=0.50 cfs @ 12.03 hrs HW=65.53' (Free Discharge) -1=Culvert (Inlet Controls 0.50 cfs @ 1.70 fps)

Summary for Pond DMH-F6: DMH-F6

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 66.96' @ 12.03 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	66.56'	12.0" Round Culvert L= 133.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 66.56' / 65.23' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.50 cfs @ 12.03 hrs HW=66.96' (Free Discharge)

Summary for Pond DMH-F7: DMH-F7

Inflow Area	a =	11,670 sf	, 57.41% Impervious,	Inflow Depth > 1.65"	for 2 Year event
Inflow	=	0.50 cfs @	12.03 hrs, Volume=	1,601 cf	
Outflow	=	0.50 cfs @	12.03 hrs, Volume=	1,601 cf, Atte	en= 0%, Lag= 0.0 min
Primary	=	0.50 cfs @	12.03 hrs, Volume=	1,601 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 67.73' @ 12.03 hrs

Device	Routing	Invert	Outlet Devices	
#1	Primary	67.33'	12.0" Round Culvert L= 67.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 67.33' / 66.67' S= 0.0099 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior	

Primary OutFlow Max=0.50 cfs @ 12.03 hrs HW=67.73' (Free Discharge)

Summary for Pond F: POND F BR

Inflow Area =	246,632 sf, 20.73% Impervious,	Inflow Depth > 0.59" for 2 Year event
Inflow =	2.64 cfs @ 12.10 hrs, Volume=	12,200 cf
Outflow =	2.56 cfs @ 12.14 hrs, Volume=	9,655 cf, Atten= 3%, Lag= 2.2 min
Discarded =	0.05 cfs @ 12.14 hrs, Volume=	3,397 cf
Primary =	2.51 cfs @ 12.14 hrs, Volume=	6,257 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 56.05' @ 12.14 hrs Surf.Area= 4,175 sf Storage= 3,097 cf

Plug-Flow detention time= 121.9 min calculated for 9,650 cf (79% of inflow) Center-of-Mass det. time= 44.7 min (805.0 - 760.3)

<u>Volume</u> #1	Invert 55.25'	Avail.Sto 3,94		Description WATER WETL	AND (Prismatic)Listed below (Recalc)
Elevatio	••••	ırf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
55.2 56.2		3,557 4,328	0 3,943	0 3,943	
Device	Routing	Invert	Outlet Devices	i	
#1 #2	Discarded Primary	55.25' 55.95'	Head (feet) 0. 2.50 3.00	.0' breadth Br 20 0.40 0.60) 2.69 2.72 2.	Surface area oad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00 75 2.85 2.98 3.08 3.20 3.28 3.31

Discarded OutFlow Max=0.05 cfs @ 12.14 hrs HW=56.05' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.05 cfs)

Primary OutFlow Max=2.51 cfs @ 12.14 hrs HW=56.05' (Free Discharge) **2=Broad-Crested Rectangular Weir** (Weir Controls 2.51 cfs @ 0.86 fps)

Summary for Pond WQU-F: WQU-F

Inflow Area	a =	246,632 sf, 20.73% Impervious, Inflow Depth > 0.59" for 2 Year ev	/ent
Inflow	=	2.64 cfs @ 12.10 hrs, Volume= 12,200 cf	
Outflow	=	2.64 cfs @ 12.10 hrs, Volume= 12,200 cf, Atten= 0%, Lag= 0).0 min
Primary	=	2.64 cfs @ 12.10 hrs, Volume= 12,200 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.29' @ 12.10 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.50'	24.0" Round Culvert
			L= 120.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 56.50' / 55.90' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=2.64 cfs @ 12.10 hrs HW=57.29' (Free Discharge) **1=Culvert** (Barrel Controls 2.64 cfs @ 3.40 fps)

Summary for Subcatchment 1H: PROP 1H

Runoff = 0.81 cfs @ 12.28 hrs, Volume= 4,671 cf, Depth> 0.35"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

_	A	rea (sf)	CN	Description			
		11,533	98 Roofs, HSG A				
		68,069	39	>75% Gras	s cover, Go	bod, HSG A	
		79,755	30	Meadow, no	on-grazed,	HSG A	
	159,357 39 Weighted Average			Weighted A	verage		
	147,824 34 92.76% Pervious Area			92.76% Pei	vious Area		
	11,533 98 7.24% Impervious Are			7.24% Impe	ervious Are	a	
_	Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description	
	6.6	50	0.0100	0.13		Sheet Flow,	
_	14.9	600	0.0020	0.67		Range n= 0.130 P2= 3.20" Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps	
	21 5	650	Total				

21.5 650 Total

Summary for Subcatchment F1: PROP 1F-1

Runoff = 1.42 cfs @ 12.13 hrs, Volume= 5,927 cf, Depth> 1.80"

A	rea (sf)	CN I	Description		
	9,051	98	Paved park	ing, HSG A	N Contraction of the second seco
	6,129	98	Roofs, HSC	βA	
	24,232	39 :	>75% Gras	s cover, Go	bod, HSG A
	39,412	62	Weighted A	verage	
	24,232	39 (61.48% Pe	rvious Area	
	15,180	98 3	38.52% Imp	pervious Ar	ea
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.2	50	0.0200	0.10		Sheet Flow,
					Grass: Dense n= 0.240 P2= 3.20"
1.4	170	0.0100	2.03		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
9.6	220	Total			

Summary for Subcatchment F2: PROP 1F-2

Runoff = 1.09 cfs @ 12.13 hrs, Volume= 4,379 cf, Depth> 2.59"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

_	A	rea (sf)	CN	Description					
		8,426	98	Paved park	ing, HSG A	N			
		3,080	98	Roofs, HSC	θĂ				
_		8,820	39	>75% Gras	s cover, Go	bod, HSG A			
		20,326	72	72 Weighted Average					
		8,820	39	39 43.39% Pervious Area					
		11,506	98	56.61% Im	pervious Ar	ea			
	Tc	Length	Slop		Capacity	Description			
_	(min)	(feet)	(ft/ft	t) (ft/sec)	(cfs)				
	8.2	50	0.020	0 0.10		Sheet Flow,			
						Grass: Dense n= 0.240 P2= 3.20"			
	1.2	150	0.010	0 2.03		Shallow Concentrated Flow,			
_						Paved Kv= 20.3 fps			
	0.1	200	Total						

9.4 200 Total

Summary for Subcatchment F3: PROP 1F-3

Runoff = 0.40 cfs @ 12.03 hrs, Volume= 1,223 cf, Depth> 4.46"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

_	A	rea (sf)	CN	Description					
		3,290	98	Paved park	ing, HSG A	N Contraction of the second seco			
		3,290	98	98 100.00% Impervious Area					
	Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description			
-	0.7	50	0.0200	1.20		Sheet Flow,			
	1.4	170	0.0100	2.03		Smooth surfaces n= 0.011 P2= 3.20" Shallow Concentrated Flow, Paved Kv= 20.3 fps			
	0.4	220	Total						

2.1 220 Total

Summary for Subcatchment F4: PROP 1F-4

Runoff = 0.32 cfs @ 12.07 hrs, Volume= 1,198 cf, Depth> 1.14"

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Type III 24-hr 10 Year Rainfall=4.70" Printed 8/7/2017 C Page 15

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Α	rea (sf)	CN E	Description		
	2,914	98 F	aved park	ing, HSG A	N Contraction of the second
	9,663	39 >	75% Gras	s cover, Go	bod, HSG A
	12,577	53 V	Veighted A	verage	
	9,663	39 7	6.83% Per	vious Area	
	2,914	98 2	3.17% Imp	pervious Ar	ea
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
4.5	50	0.2500	0.19		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.20"
0.2	30	0.2000	2.24		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.2	70	0.0800	5.74		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
4.9	150	Total			

Summary for Subcatchment F5: PROP 1F-5

Runoff = 0.38 cfs @ 12.06 hrs, Volume= 1,287 cf, Depth> 2.27"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 10 Year Rainfall=4.70"

	Α	rea (sf)	CN [Description					
		3,350	98 F	Paved park	ing, HSG A	N Contraction of the second			
		3,450	39 >	-75% Gras	s cover, Go	bod, HSG A			
		6,800	68 V	Veighted A	verage				
		3,450	39 5	39 50.74% Pervious Area					
		3,350	98 4	3 49.26% Impervious Area					
	Тс	Length	Slope	Velocity	Capacity	Description			
(n	nin)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	3.0	50	0.2500	0.28		Sheet Flow,			
						Grass: Dense n= 0.240 P2= 3.20"			
	1.0	170	0.0200	2.87		Shallow Concentrated Flow,			
						Paved Kv= 20.3 fps			
	4.0	220	Total						

Summary for Subcatchment F6: PROP 1F-6

Runoff = 0.41 cfs @ 12.02 hrs, Volume= 1,264 cf, Depth> 3.11"

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Type III 24-hr 10 Year Rainfall=4.70" Printed 8/7/2017 C Page 16

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_	A	rea (sf)	ı (sf)	CN D	escription				
		3,350	,350	98 P	aved park	ing, HSG A			
_		1,520	,520	39 >	75% Gras	s cover, Go	bod, HSG A		
		4,870	,870	80 V	Weighted Average				
		1,520	,520	39 3	39 31.21% Pervious Area				
		3,350	,350	98 6	68.79% Impervious Area				
	Tc (min)	Length (feet)	0	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
	0.7	50	50	0.0200	1.20		Sheet Flow,		
	0.8	140	140	0.0200	2.87		Smooth surfaces n= 0.011 P2= 3.20" Shallow Concentrated Flow, Paved Kv= 20.3 fps		
	4 5	400	400	T . (.)					

1.5 190 Total

Summary for Reach 1F: DA-1F

Inflow Are	a =	246,632 sf, 20.73% Impervious, Inflow Depth > 0.	66" for 10 Year event
Inflow	=	3.90 cfs @ 12.13 hrs, Volume= 13,584 cf	
Outflow	=	3.90 cfs @ 12.13 hrs, Volume= 13,584 cf,	Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Pond 1: CB-F1

Inflow Area =	39,412 sf, 38.52% Impervious,	Inflow Depth > 1.80" for 10 Year event
Inflow =	1.42 cfs @ 12.13 hrs, Volume=	5,927 cf
Outflow =	1.42 cfs @ 12.13 hrs, Volume=	5,927 cf, Atten= 0%, Lag= 0.0 min
Primary =	1.42 cfs @ 12.13 hrs, Volume=	5,927 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.80' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.00'	12.0" Round Culvert L= 16.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.00' / 56.90' S= 0.0063 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.42 cfs @ 12.13 hrs HW=57.80' (Free Discharge) **1=Culvert** (Barrel Controls 1.42 cfs @ 2.88 fps)

Summary for Pond 2: CB-F2

Inflow Area	a =	20,326 sf, 56.61% Impervious, Inflow Depth > 2.59" for 10 Year eve	ent
Inflow	=	1.09 cfs @ 12.13 hrs, Volume= 4,379 cf	
Outflow	=	1.09 cfs @ 12.13 hrs, Volume= 4,379 cf, Atten= 0%, Lag= 0.0	min
Primary	=	1.09 cfs @ 12.13 hrs, Volume= 4,379 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

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Peak Elev= 57.67' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.00'	12.0" Round Culvert L= 12.5' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.00' / 56.90' S= 0.0080 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.08 cfs @ 12.13 hrs HW=57.67' (Free Discharge) 1=Culvert (Barrel Controls 1.08 cfs @ 2.74 fps)

Summary for Pond 2P: CB-H1

Inflow Area :	=	159,357 sf,	7.24% Impervious,	Inflow Depth > 0.35"	for 10 Year event
Inflow =	=	0.81 cfs @	12.28 hrs, Volume=	4,671 cf	
Outflow =	=	0.81 cfs @	12.28 hrs, Volume=	4,671 cf, Atte	n= 0%, Lag= 0.0 min
Primary =	=	0.81 cfs @	12.28 hrs, Volume=	4,671 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.09' @ 12.28 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.50'	10.0" Round Culvert L= 115.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $57.50' / 56.90'$ S= 0.0052 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.81 cfs @ 12.28 hrs HW=58.09' (Free Discharge) **1=Culvert** (Barrel Controls 0.81 cfs @ 2.76 fps)

Summary for Pond 3: CB-F3

Inflow Area	a =	3,290 sf,10	00.00% Impervious	Inflow Depth > 4	4.46" for 10 \	Year event
Inflow	=	0.40 cfs @ 1	2.03 hrs, Volume=	1,223 cf		
Outflow	=	0.40 cfs @ 1	2.03 hrs, Volume=	1,223 cf,	Atten= 0%, L	.ag= 0.0 min
Primary	=	0.40 cfs @ 1	2.03 hrs, Volume=	1,223 cf		-

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 60.07' @ 12.03 hrs

Device R	Routing	Invert	Outlet Devices
	<u> </u>		12.0" Round Culvert L= 10.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 59.70' / 59.60' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.40 cfs @ 12.03 hrs HW=60.07' (Free Discharge) ←1=Culvert (Barrel Controls 0.40 cfs @ 2.24 fps)

Summary for Pond 4: CB-F4

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 60.03' @ 12.07 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	59.70'	12.0" Round Culvert L= 9.7' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 59.70' / 59.60' S= 0.0103 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.32 cfs @ 12.07 hrs HW=60.03' (Free Discharge) -1=Culvert (Barrel Controls 0.32 cfs @ 2.15 fps)

Summary for Pond 5: CB-F5

Inflow Are	a =	6,800 sf,	49.26% Impervious,	Inflow Depth > 2.27"	for 10 Year event
Inflow	=	0.38 cfs @	12.06 hrs, Volume=	1,287 cf	
Outflow	=	0.38 cfs @	12.06 hrs, Volume=	1,287 cf, Atte	n= 0%, Lag= 0.0 min
Primary	=	0.38 cfs @	12.06 hrs, Volume=	1,287 cf	-

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 68.04' @ 12.06 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	67.70'	12.0" Round Culvert L= 14.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 67.70' / 67.43' S= 0.0193 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.38 cfs @ 12.06 hrs HW=68.04' (Free Discharge)

Summary for Pond 6: CB-F6

Inflow Area	a =	4,870 sf, 68.79% Impervious, Inflow Depth > 3.11" for 10 Year e	event
Inflow	=	0.41 cfs @ 12.02 hrs, Volume= 1,264 cf	
Outflow	=	0.41 cfs @ 12.02 hrs, Volume= 1,264 cf, Atten= 0%, Lag= 0).0 min
Primary	=	0.41 cfs @ 12.02 hrs, Volume= 1,264 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 68.06' @ 12.02 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	67.70'	12.0" Round Culvert
			L= 14.0' CPP, projecting, no headwall, Ke= 0.900

Inlet / Outlet Invert= 67.70' / 67.43' S= 0.0193'' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.41 cfs @ 12.02 hrs HW=68.06' (Free Discharge) **1=Culvert** (Inlet Controls 0.41 cfs @ 1.62 fps)

Summary for Pond DMH-F1: DMH-F1

Inflow Area	a =	246,632 sf	, 20.73% Impervious,	Inflow Depth > 0.97"	for 10 Year event
Inflow	=	4.03 cfs @	12.10 hrs, Volume=	19,950 cf	
Outflow	=	4.03 cfs @	12.10 hrs, Volume=	19,950 cf, Atte	en= 0%, Lag= 0.0 min
Primary	=	4.03 cfs @	12.10 hrs, Volume=	19,950 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.97' @ 12.10 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.80'	18.0" Round Culvert L= 20.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.80' / 56.60' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=4.03 cfs @ 12.10 hrs HW=57.97' (Free Discharge) **1=Culvert** (Barrel Controls 4.03 cfs @ 3.77 fps)

Summary for Pond DMH-F2: DMH-F2

Inflow Area =	=	27,537 sf,	, 46.86% Impervious,	Inflow Depth > 2.17	for 10 Year event
Inflow =	:	1.44 cfs @	12.04 hrs, Volume=	4,973 cf	
Outflow =	:	1.44 cfs @	12.04 hrs, Volume=	4,973 cf, Atte	en= 0%, Lag= 0.0 min
Primary =	:	1.44 cfs @	12.04 hrs, Volume=	4,973 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.26' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices
-	Primary		15.0" Round Culvert L= 56.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.60' / 56.90' S= 0.0125 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.44 cfs @ 12.04 hrs HW=58.26' (Free Discharge) **1=Culvert** (Inlet Controls 1.44 cfs @ 2.19 fps)

Summary for Pond DMH-F3: DMH-F3

Inflow Area =	27,537 sf	, 46.86% Impervious,	Inflow Depth > 2.17"	for 10 Year event
Inflow =	1.44 cfs @	12.04 hrs, Volume=	4,973 cf	
Outflow =	1.44 cfs @	12.04 hrs, Volume=	4,973 cf, Atte	n= 0%, Lag= 0.0 min
Primary =	1.44 cfs @	12.04 hrs, Volume=	4,973 cf	-

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Type III 24-hr 10 Year Rainfall=4.70" Printed 8/7/2017 C Page 20

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Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 60.16' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	59.50'	15.0" Round Culvert L= 152.5' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $59.50' / 57.70'$ S= 0.0118 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.44 cfs @ 12.04 hrs HW=60.16' (Free Discharge) -1=Culvert (Inlet Controls 1.44 cfs @ 2.19 fps)

Summary for Pond DMH-F4: DMH-F4

Inflow Area	=	11,670 sf,	57.41% Impervious,	Inflow Depth > 2.62"	for 10 Year event
Inflow	=	0.76 cfs @ 1	12.03 hrs, Volume=	2,551 cf	
Outflow	=	0.76 cfs @	12.03 hrs, Volume=	2,551 cf, Atte	en= 0%, Lag= 0.0 min
Primary	=	0.76 cfs @ 1	12.03 hrs, Volume=	2,551 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 64.62' @ 12.03 hrs

#1 Primary 64.12' 12.0" Round Culvert L= 91.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 64.12' / 59.60' S= 0.0497 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior	

Primary OutFlow Max=0.76 cfs @ 12.03 hrs HW=64.62' (Free Discharge) **1=Culvert** (Inlet Controls 0.76 cfs @ 1.91 fps)

Summary for Pond DMH-F5: DMH-F5

Inflow Area	a =	11,670 sf, 57.41% Imperviou	us, Inflow Depth > 2.62" for 10	Year event
Inflow	=	0.76 cfs @ 12.03 hrs, Volume	e= 2,551 cf	
Outflow	=	0.76 cfs @ 12.03 hrs, Volume	e= 2,551 cf, Atten= 0%,	Lag= 0.0 min
Primary	=	0.76 cfs @ 12.03 hrs, Volume	e= 2,551 cf	-

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 65.63' @ 12.03 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	65.13'	12.0" Round Culvert L= 91.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 65.13' / 64.22' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.76 cfs @ 12.03 hrs HW=65.63' (Free Discharge) -1=Culvert (Inlet Controls 0.76 cfs @ 1.91 fps)

Summary for Pond DMH-F6: DMH-F6

Inflow Area =11,670 sf, 57.41% Impervious, Inflow Depth > 2.62" for 10 Year eventInflow =0.76 cfs @ 12.03 hrs, Volume=2,551 cfOutflow =0.76 cfs @ 12.03 hrs, Volume=2,551 cf, Atten= 0%, Lag= 0.0 minPrimary =0.76 cfs @ 12.03 hrs, Volume=2,551 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 67.06' @ 12.03 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	66.56'	12.0" Round Culvert L= 133.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 66.56' / 65.23' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.76 cfs @ 12.03 hrs HW=67.06' (Free Discharge)

Summary for Pond DMH-F7: DMH-F7

Inflow Area	a =	11,670 sf	, 57.41% Impervious,	Inflow Depth > 2.62"	for 10 Year event
Inflow	=	0.76 cfs @	12.03 hrs, Volume=	2,551 cf	
Outflow	=	0.76 cfs @	12.03 hrs, Volume=	2,551 cf, Atte	n= 0%, Lag= 0.0 min
Primary	=	0.76 cfs @	12.03 hrs, Volume=	2,551 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 67.83' @ 12.03 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	67.33'	12.0" Round Culvert L= 67.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 67.33' / 66.67' S= 0.0099 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.76 cfs @ 12.03 hrs HW=67.83' (Free Discharge)

Summary for Pond F: POND F BR

Inflow Area =	246,632 sf, 20.73% Impervious,	Inflow Depth > 0.97" for 10 Year event
Inflow =	4.03 cfs @ 12.10 hrs, Volume=	19,950 cf
Outflow =	3.95 cfs @ 12.13 hrs, Volume=	17,261 cf, Atten= 2%, Lag= 1.8 min
Discarded =	0.05 cfs @ 12.13 hrs, Volume=	3,677 cf
Primary =	3.90 cfs @ 12.13 hrs, Volume=	13,584 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 56.09' @ 12.13 hrs Surf.Area= 4,201 sf Storage= 3,241 cf

Plug-Flow detention time= 101.6 min calculated for 17,254 cf (86% of inflow) Center-of-Mass det. time= 36.7 min (805.3 - 768.6) Prepared by Microsoft HydroCAD® 9.10 s/n 00884 © 2010 HydroCAD Software Solutions LLC

Volume	Invert	Avail.Sto	rage Storage I	Description	
#1	55.25'	3,94	43 cf STORM	WATER WETL	_AND (Prismatic)Listed below (Recalc)
Elevatio	•••	rf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
55.2 56.2		3,557 4,328	0 3,943	0 3,943	
Device	Routing	Invert	Outlet Devices	i	
#1 #2	Discarded Primary	55.25' 55.95'	Head (feet) 0. 2.50 3.00	.0' breadth Br 20 0.40 0.60) 2.69 2.72 2	Surface area road-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00 .75 2.85 2.98 3.08 3.20 3.28 3.31

Discarded OutFlow Max=0.05 cfs @ 12.13 hrs HW=56.09' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.05 cfs)

Primary OutFlow Max=3.89 cfs @ 12.13 hrs HW=56.09' (Free Discharge) **2=Broad-Crested Rectangular Weir** (Weir Controls 3.89 cfs @ 0.99 fps)

Summary for Pond WQU-F: WQU-F

Inflow Area	a =	246,632 sf, 20.73% Impervious, Inflow Depth > 0.97" for 10 Year	event
Inflow	=	4.03 cfs @ 12.10 hrs, Volume= 19,950 cf	
Outflow	=	4.03 cfs @ 12.10 hrs, Volume= 19,950 cf, Atten= 0%, Lag= (0.0 min
Primary	=	4.03 cfs @ 12.10 hrs, Volume= 19,950 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 57.50' @ 12.10 hrs

Device	Routing	Invert	Outlet Devices
<u></u> #1	Primary		24.0" Round Culvert L= 120.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.50' / 55.90' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=4.03 cfs @ 12.10 hrs HW=57.50' (Free Discharge) -1=Culvert (Barrel Controls 4.03 cfs @ 3.76 fps)

Summary for Subcatchment 1H: PROP 1H

Runoff = 2.26 cfs @ 12.38 hrs, Volume= 17,713 cf, Depth> 1.33"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

_	A	rea (sf)	CN	Description							
		11,533	98	N8 Roofs, HSG A							
		68,069	39	>75% Gras	s cover, Go	bod, HSG A					
_		79,755	30	Meadow, no	on-grazed,	HSG A					
	1	59,357	39	Weighted A	verage						
	1	47,824	34	92.76% Per	vious Area						
	11,533 98 7.24% Impervious Area					а					
_	Tc (min)	Length (feet)	Slop (ft/fl		Capacity (cfs)	Description					
	6.6	50	0.010	0.13		Sheet Flow,					
_	14.9	600	0.002	0 0.67		Range n= 0.130 P2= 3.20" Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps					
	21 5	650	Total								

21.5 650 Total

Summary for Subcatchment F1: PROP 1F-1

Runoff = 2.99 cfs @ 12.13 hrs, Volume= 12,764 cf, Depth> 3.89"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

A	rea (sf)	CN	Description		
	9,051	98	Paved park	ing, HSG A	N
	6,129	98	Roofs, HSG	βA	
	24,232	39 :	>75% Gras	s cover, Go	bod, HSG A
	39,412	62	Neighted A	verage	
	24,232	39 (51.48% Pei	vious Area	l
	15,180	98 3	38.52% Imp	pervious Ar	ea
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.2	50	0.0200	0.10		Sheet Flow,
					Grass: Dense n= 0.240 P2= 3.20"
1.4	170	0.0100	2.03		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
9.6	220	Total			

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Summary for Subcatchment F2: PROP 1F-2

Runoff = 2.09 cfs @ 12.13 hrs, Volume= 8,656 cf, Depth> 5.11"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

_	A	rea (sf)	CN	Description	l							
_		8,426	98	Paved park	Paved parking, HSG A							
		3,080	98	Roofs, HSC	ΞĂ							
_		8,820	39	>75% Gras	s cover, Go	bod, HSG A						
		20,326	72	Weighted A	verage							
		8,820	39	43.39% Pe	rvious Area	l						
		11,506	98	56.61% Impervious Area								
	Та	Longth	Clan		Conocity	Description						
	Tc (min)	Length	Slop		Capacity	Description						
-	(min)	(feet)	(ft/f1	/ / /	(cfs)							
	8.2	50	0.020	0 0.10		Sheet Flow,						
						Grass: Dense n= 0.240 P2= 3.20"						
	1.2	150	0.010	0 2.03		Shallow Concentrated Flow,						
_						Paved Kv= 20.3 fps						
	Q /	200	Total									

9.4 200 Total

Summary for Subcatchment F3: PROP 1F-3

Runoff = 0.71 cfs @ 12.03 hrs, Volume= 2,208 cf, Depth> 8.05"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

_	A	rea (sf)	CN	Description					
		3,290	98	Paved park	ing, HSG A	N			
_		3,290	98	100.00% Impervious Area					
	Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description			
-	0.7	50	0.0200		(0.0)	Sheet Flow,			
	1.4	170	0.0100) 2.03		Smooth surfaces n= 0.011 P2= 3.20" Shallow Concentrated Flow, Paved Kv= 20.3 fps			
_	0.4	000	Tatal			-			

2.1 220 Total

Summary for Subcatchment F4: PROP 1F-4

Runoff = 0.79 cfs @ 12.08 hrs, Volume= 2,988 cf, Depth> 2.85"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30" 15-063 Hyd-Prop DA-F1

Type III 24-hr 100 Year Rainfall=8.30" Printed 8/7/2017 LC Page 25

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A	rea (sf)	CN D	escription							
	2,914	98 P	98 Paved parking, HSG A							
	9,663	39 >	75% Gras	s cover, Go	ood, HSG A					
	12,577	53 V	Veighted A	verage						
	9,663	39 7	6.83% Per	vious Area						
	2,914	98 2	3.17% lmp	ervious Are	ea					
-		0		• •						
Тс	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
4.5	50	0.2500	0.19		Sheet Flow,					
					Woods: Light underbrush n= 0.400 P2= 3.20"					
0.2	30	0.2000	2.24		Shallow Concentrated Flow,					
					Woodland Kv= 5.0 fps					
0.2	70	0.0800	5.74		Shallow Concentrated Flow,					
					Paved Kv= 20.3 fps					
4.9	150	Total								

Summary for Subcatchment F5: PROP 1F-5

Runoff = 0.75 cfs @ 12.06 hrs, Volume= 2,616 cf, Depth> 4.62"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30"

A	rea (sf)	CN E	Description			_				
	3,350	98 F	Paved parking, HSG A							
	3,450	39 >	75% Gras	s cover, Go	bod, HSG A	_				
	6,800	68 V	Veighted A	verage						
	3,450	39 5	0.74% Per	vious Area						
	3,350	98 4	49.26% Impervious Area							
_										
Tc	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		_				
3.0	50	0.2500	0.28		Sheet Flow,					
					Grass: Dense n= 0.240 P2= 3.20"					
1.0	170	0.0200	2.87		Shallow Concentrated Flow,					
					Paved Kv= 20.3 fps	_				
4.0	220	Total								

Summary for Subcatchment F6: PROP 1F-6

Runoff = 0.78 cfs @ 12.02 hrs, Volume= 2,411 cf, Depth> 5.94"

Runoff by SCS TR-20 method, UH=SCS, Split Pervious/Imperv., Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Type III 24-hr 100 Year Rainfall=8.30" 15-063 Hyd-Prop DA-F1

Type III 24-hr 100 Year Rainfall=8.30" Printed 8/7/2017 LC Page 26

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_	A	rea (sf)	CN	Description							
		3,350	98	Paved parking, HSG A							
_		1,520	39	>75% Gras	s cover, Go	bod, HSG A					
		4,870	80	80 Weighted Average							
		1,520	39	31.21% Pe	rvious Area						
		3,350	98	98 68.79% Impervious Area							
	Тс	Length			Capacity	Description					
_	(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)						
	0.7	50	0.020	0 1.20		Sheet Flow,					
						Smooth surfaces n= 0.011 P2= 3.20"					
	0.8	140	0.020	0 2.87		Shallow Concentrated Flow,					
_						Paved Kv= 20.3 fps					
	4 -	400	T								

1.5 190 Total

Summary for Reach 1F: DA-1F

Inflow Are	a =	246,632 sf, 20.73% Impervious	Inflow Depth > 2.08"	for 100 Year event
Inflow	=	7.94 cfs @ 12.14 hrs, Volume=	42,685 cf	
Outflow	=	7.94 cfs @ 12.14 hrs, Volume=	42,685 cf, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

Summary for Pond 1: CB-F1

Inflow Area =	39,412 sf, 38.52% Impervious,	Inflow Depth > 3.89" for 100 Year event
Inflow =	2.99 cfs @ 12.13 hrs, Volume=	12,764 cf
Outflow =	2.99 cfs @ 12.13 hrs, Volume=	12,764 cf, Atten= 0%, Lag= 0.0 min
Primary =	2.99 cfs @ 12.13 hrs, Volume=	12,764 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.50' @ 12.13 hrs

#1 Primary 57.00' 12.0" Round Culvert L= 16.0' CPP, projecting, no headwall, Ke= 0.900	Device	Routing	Invert	Outlet Devices
n = 0.013 Corrugated PE, smooth interior		U		12.0" Round Culvert L= 16.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.00' / 56.90' S= 0.0063 '/' Cc= 0.900

Primary OutFlow Max=2.98 cfs @ 12.13 hrs HW=58.50' (Free Discharge) -1=Culvert (Inlet Controls 2.98 cfs @ 3.80 fps)

Summary for Pond 2: CB-F2

Inflow Area =	20,326 sf, 56.61% Impervious,	Inflow Depth > 5.11" for 100 Year event
Inflow =	2.09 cfs @ 12.13 hrs, Volume=	8,656 cf
Outflow =	2.09 cfs @ 12.13 hrs, Volume=	8,656 cf, Atten= 0%, Lag= 0.0 min
Primary =	2.09 cfs @ 12.13 hrs, Volume=	8,656 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs

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Peak Elev= 58.03' @ 12.13 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary		12.0" Round Culvert L= 12.5' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.00' / 56.90' S= 0.0080 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=2.09 cfs @ 12.13 hrs HW=58.03' (Free Discharge) 1=Culvert (Barrel Controls 2.09 cfs @ 3.23 fps)

Summary for Pond 2P: CB-H1

Inflow Area =	159,357 sf, 7.24% Impe	ervious, Inflow Depth > 1.33"	for 100 Year event
Inflow =	2.26 cfs @ 12.38 hrs, Vo	lume= 17,713 cf	
Outflow =	2.26 cfs @ 12.38 hrs, Vo	lume= 17,713 cf, Atte	n= 0%, Lag= 0.0 min
Primary =	2.26 cfs @ 12.38 hrs, Vo	lume= 17,713 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 59.46' @ 12.38 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	57.50'	10.0" Round Culvert L= 115.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= $57.50' / 56.90'$ S= 0.0052 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=2.26 cfs @ 12.38 hrs HW=59.46' (Free Discharge) ☐ 1=Culvert (Barrel Controls 2.26 cfs @ 4.14 fps)

Summary for Pond 3: CB-F3

Inflow Area	a =	3,290 sf,100.00% Impervious, Inflow Depth > 8.05" for 100 Year event
Inflow	=	0.71 cfs @ 12.03 hrs, Volume= 2,208 cf
Outflow	=	0.71 cfs @ 12.03 hrs, Volume= 2,208 cf, Atten= 0%, Lag= 0.0 min
Primary	=	0.71 cfs @ 12.03 hrs, Volume= 2,208 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 60.21' @ 12.03 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary		12.0" Round Culvert L= 10.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 59.70' / 59.60' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.71 cfs @ 12.03 hrs HW=60.21' (Free Discharge) **1=Culvert** (Barrel Controls 0.71 cfs @ 2.53 fps)

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Summary for Pond 4: CB-F4

Inflow Area = $12,577 ext{ sf}, 23.17\%$ Impervious, Inflow Depth > 2.85" for 100 Year eventInflow = $0.79 ext{ cfs} @ 12.08 ext{ hrs}, Volume=$ $2,988 ext{ cf}$ Outflow = $0.79 ext{ cfs} @ 12.08 ext{ hrs}, Volume=$ $2,988 ext{ cf}, ext{ Atten= 0\%, Lag= 0.0 min}$ Primary = $0.79 ext{ cfs} @ 12.08 ext{ hrs}, Volume=$ $2,988 ext{ cf}$

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 60.25' @ 12.08 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	59.70'	12.0" Round Culvert L= 9.7' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 59.70' / 59.60' S= 0.0103 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.79 cfs @ 12.08 hrs HW=60.25' (Free Discharge) -1=Culvert (Barrel Controls 0.79 cfs @ 2.60 fps)

Summary for Pond 5: CB-F5

Inflow Area	a =	6,800 sf	, 49.26% Impervious,	Inflow Depth > 4.62	for 100 Year event
Inflow	=	0.75 cfs @	12.06 hrs, Volume=	2,616 cf	
Outflow	=	0.75 cfs @	12.06 hrs, Volume=	2,616 cf, Att	en= 0%, Lag= 0.0 min
Primary	=	0.75 cfs @	12.06 hrs, Volume=	2,616 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 68.20' @ 12.06 hrs

Device	Routing	Invert	Outlet Devices
-	Primary		12.0" Round Culvert L= 14.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 67.70' / 67.43' S= 0.0193 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior
			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,

Primary OutFlow Max=0.75 cfs @ 12.06 hrs HW=68.20' (Free Discharge) -1=Culvert (Inlet Controls 0.75 cfs @ 1.91 fps)

Summary for Pond 6: CB-F6

Inflow Area	a =	4,870 sf, 68.79% Impervious, Inflow Depth > 5.94" for 100 Year event
Inflow	=	0.78 cfs @ 12.02 hrs, Volume= 2,411 cf
Outflow	=	0.78 cfs @ 12.02 hrs, Volume= 2,411 cf, Atten= 0%, Lag= 0.0 min
Primary	=	0.78 cfs @ 12.02 hrs, Volume= 2,411 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 68.21' @ 12.02 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	67.70'	12.0" Round Culvert
			L= 14.0' CPP, projecting, no headwall, Ke= 0.900

Inlet / Outlet Invert= 67.70' / 67.43' S= 0.0193'' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=0.77 cfs @ 12.02 hrs HW=68.21' (Free Discharge)

Summary for Pond DMH-F1: DMH-F1

Inflow Area	I =	246,632 sf, 20.73% Impervious, Inflow Depth > 2.40" for 100 Year e	event
Inflow	=	8.09 cfs @ 12.11 hrs, Volume= 49,356 cf	
Outflow	=	8.09 cfs @ 12.11 hrs, Volume= 49,356 cf, Atten= 0%, Lag= 0.0	0 min
Primary	=	8.09 cfs @ 12.11 hrs, Volume= 49,356 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 59.00' @ 12.11 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	56.80'	18.0" Round Culvert L= 20.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.80' / 56.60' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=8.09 cfs @ 12.11 hrs HW=59.00' (Free Discharge) -1=Culvert (Inlet Controls 8.09 cfs @ 4.58 fps)

Summary for Pond DMH-F2: DMH-F2

Inflow Area =	=	27,537 sf,	46.86% Impervious	Inflow Depth > 4.4	45" for 100 Year event
Inflow =	2	.84 cfs @	12.04 hrs, Volume=	10,222 cf	
Outflow =	2	.84 cfs @	12.04 hrs, Volume=	10,222 cf, /	Atten= 0%, Lag= 0.0 min
Primary =	2	.84 cfs @	12.04 hrs, Volume=	10,222 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.60' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices
<u></u> #1	Primary		15.0" Round Culvert L= 56.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 57.60' / 56.90' S= 0.0125 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=2.84 cfs @ 12.04 hrs HW=58.60' (Free Discharge) **1=Culvert** (Inlet Controls 2.84 cfs @ 2.69 fps)

Summary for Pond DMH-F3: DMH-F3

Inflow Area =	27,537 sf, 46.86% Impervious,	Inflow Depth > 4.45" for 100 Year event
Inflow =	2.84 cfs @ 12.04 hrs, Volume=	10,222 cf
Outflow =	2.84 cfs @ 12.04 hrs, Volume=	10,222 cf, Atten= 0%, Lag= 0.0 min
Primary =	2.84 cfs @ 12.04 hrs, Volume=	10,222 cf

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Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 60.50' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	59.50'	15.0" Round Culvert L= 152.5' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 59.50' / 57.70' S= 0.0118 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=2.84 cfs @ 12.04 hrs HW=60.50' (Free Discharge) -1=Culvert (Inlet Controls 2.84 cfs @ 2.69 fps)

Summary for Pond DMH-F4: DMH-F4

Inflow Area	a =	11,670 sf, 57.41% Impervious, Inflow Depth > 5.17" for 100 Year event
Inflow	=	1.45 cfs @ 12.04 hrs, Volume= 5,027 cf
Outflow	=	1.45 cfs @ 12.04 hrs, Volume= 5,027 cf, Atten= 0%, Lag= 0.0 min
Primary	=	1.45 cfs @ 12.04 hrs, Volume= 5,027 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 64.86' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices
-	Primary	64.12'	12.0" Round Culvert L= 91.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 64.12' / 59.60' S= 0.0497 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.45 cfs @ 12.04 hrs HW=64.86' (Free Discharge) **1=Culvert** (Inlet Controls 1.45 cfs @ 2.32 fps)

Summary for Pond DMH-F5: DMH-F5

Inflow Area	a =	11,670 sf, 57.41% l	mpervious,	Inflow Depth >	5.17"	for 100 Year event
Inflow	=	1.45 cfs @ 12.04 hrs,	Volume=	5,027 c	f	
Outflow	=	1.45 cfs @ 12.04 hrs,	Volume=	5,027 c	f, Atter	n= 0%, Lag= 0.0 min
Primary	=	1.45 cfs @ 12.04 hrs,	Volume=	5,027 c	f	-

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 65.87' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	65.13'	12.0" Round Culvert L= 91.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 65.13' / 64.22' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.45 cfs @ 12.04 hrs HW=65.87' (Free Discharge) **1=Culvert** (Inlet Controls 1.45 cfs @ 2.32 fps)

Summary for Pond DMH-F6: DMH-F6

Inflow Area =11,670 sf, 57.41% Impervious, Inflow Depth > 5.17" for 100 Year eventInflow =1.45 cfs @ 12.04 hrs, Volume=5,027 cfOutflow =1.45 cfs @ 12.04 hrs, Volume=5,027 cf, Atten= 0%, Lag= 0.0 minPrimary =1.45 cfs @ 12.04 hrs, Volume=5,027 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 67.30' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	66.56'	12.0" Round Culvert L= 133.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 66.56' / 65.23' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.45 cfs @ 12.04 hrs HW=67.30' (Free Discharge) **1=Culvert** (Inlet Controls 1.45 cfs @ 2.32 fps)

Summary for Pond DMH-F7: DMH-F7

Inflow Are	a =	11,670 sf, 57.41% Impervious, Inflow Depth > 5.17" for 100 Year ever	nt
Inflow	=	1.45 cfs @ 12.04 hrs, Volume= 5,027 cf	
Outflow	=	1.45 cfs @ 12.04 hrs, Volume= 5,027 cf, Atten= 0%, Lag= 0.0 mi	in
Primary	=	1.45 cfs @ 12.04 hrs, Volume= 5,027 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 68.07' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	67.33'	12.0" Round Culvert L= 67.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 67.33' / 66.67' S= 0.0099 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=1.45 cfs @ 12.04 hrs HW=68.07' (Free Discharge)

Summary for Pond F: POND F BR

Inflow Area =	246,632 sf, 20.73% Impervious,	Inflow Depth > 2.40" for 100 Year event
Inflow =	8.09 cfs @ 12.11 hrs, Volume=	49,356 cf
Outflow =	7.99 cfs @ 12.14 hrs, Volume=	46,613 cf, Atten= 1%, Lag= 1.6 min
Discarded =	0.05 cfs @ 12.14 hrs, Volume=	3,928 cf
Primary =	7.94 cfs @ 12.14 hrs, Volume=	42,685 cf

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 56.17' @ 12.14 hrs Surf.Area= 4,265 sf Storage= 3,590 cf

Plug-Flow detention time= 57.5 min calculated for 46,593 cf (94% of inflow) Center-of-Mass det. time= 25.9 min (828.3 - 802.4) 15-063 Hyd-Prop DA-F1

Type III 24-hr 100 Year Rainfall=8.30" Printed 8/7/2017 LC Page 32

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Volume	Invert	Avail.Stor	age Storage I	Description	
#1	55.25'	3,94	3 cf STORM	WATER WETL	_AND (Prismatic)Listed below (Recalc)
Elevatio	•••	rf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
55.2 56.2	-	3,557 4,328	0 3,943	0 3,943	
Device	Routing	Invert	Outlet Devices		
#1 #2	Discarded Primary	55.25' 55.95'	Head (feet) 0.2 2.50 3.00	.0' breadth Br 20 0.40 0.60 2.69 2.72 2	Surface area road-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00 .75 2.85 2.98 3.08 3.20 3.28 3.31

Discarded OutFlow Max=0.05 cfs @ 12.14 hrs HW=56.17' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.05 cfs)

Primary OutFlow Max=7.94 cfs @ 12.14 hrs HW=56.17' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 7.94 cfs @ 1.26 fps)

Summary for Pond WQU-F: WQU-F

Inflow Area	=	246,632 sf	, 20.73% Impervious,	Inflow Depth > 2.40)" for 100 Year event
Inflow	=	8.09 cfs @	12.11 hrs, Volume=	49,356 cf	
Outflow	=	8.09 cfs @	12.11 hrs, Volume=	49,356 cf, At	ten= 0%, Lag= 0.0 min
Primary	=	8.09 cfs @	12.11 hrs, Volume=	49,356 cf	

Routing by Stor-Ind method, Time Span= 1.00-24.00 hrs, dt= 0.01 hrs Peak Elev= 58.01' @ 12.11 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary		24.0" Round Culvert L= 120.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 56.50' / 55.90' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior

Primary OutFlow Max=8.09 cfs @ 12.11 hrs HW=58.01' (Free Discharge) -1=Culvert (Barrel Controls 8.09 cfs @ 4.40 fps)

Appendix C

Operation & Maintenance Plan

STORMWATER MANAGEMENT OPERATION AND MAINTENANCE PLAN

Port Place Newburyport, Massachusetts

The following Stormwater Management Operation and Maintenance (O&M) Plan has been prepared to operate and maintain the stormwater management system for the proposed development by Evergreen Commons LLC.

Owner/Operator: Evergreen Commons, LLC will be responsible for the operation and maintenance of the stormwater management system and erosion control measures until the roadways are completed and accepted by the City at which time the City of Newburyport will be responsible for the operation and maintenance of the Catch Basins, Drain Manholes and piping within the roadway. Evergreen Commons LLC or the Homeowners Associations will maintain the swirl particle separators, biorentention areas and the constructed stormwater wetland.

Inspection and Maintenance – Construction Phase

Erosion and Sediment Controls

All construction erosion control measures shall be installed in accordance to the project plan and specifications. Control measures shall be inspected at least once per week and immediately after each rain event of 0.5 inches or greater. A maintenance inspection report will be made after each inspection. The Contractor's site superintendent shall be responsible for inspections, maintenance and repair activities, as well as, for filling out the inspection reports. Any necessary repairs needed to the erosion control barriers shall be made immediately to keep them in good working order. If there are any signs of undercutting or impounding of water behind the barrier, a temporary check dam should replace the section of barrier.

Stabilization of any swales, ditches and ponds is required prior to directing any flow to them. Construction stormwater shall be diverted away from all infiltration facilities, and sediment control barriers shall be installed around the facilities to filter any potential sheet flow. See Erosion Control Notes in the Project plans and specifications for construction phase stabilization methods and vegetative practices. All measures will be maintained in good working order; if a repair is necessary, it will be initiated within 24 hours of report. Remove any built up sediment found inside measures and dispose of properly. Refer to the project plans and specifications for installation details for the following construction erosion and sediment controls.

Stabilized Construction Entrance -

- The entrance shall be maintained in a condition which will prevent tracking or flowing of sediment onto public rights-of-way. This will require periodic top dressing with additional stone or additional length as conditions demand and repair and/or cleanout of any measures used to trap sediment.
- All sediment spilled, washed, dropped or tracked onto public rights-of-way must be removed immediately.

Catch Basins and Particle Separators -

• Install erosion control measures in these structures as described on the Site Plans.

- Structures shall be inspected at least once a week and immediately after every rain storm. Remove any accumulated sediment and dispose off site properly.
- Measures shall remain in place until after permanent stabilization of grassed areas has been achieved and road paving has been completed.

Bioretention Areas & Constructed Stormwater Wetland

- Install erosion control barrier around perimeter of rain gardens, and maintain to prevent any tracking of sediments into area.
- Contractor to implement measures to divert any runoff from storms away from rain garden areas during construction and planting phases.
- Erosion control measures to remain in place until surrounding grassed areas have been stabilized.
- Remove any accumulated sediment from perimeter of erosion control barriers.
- For the Pocket Wetlands, aggressively provide erosion controls during the standing and planting periods. Stabilize the vegetation in all areas above the normal pool elevation during the standing period (typically by hydroseeding).

Construction Phase Dewatering – Pumped Filter Bags

Dewater the constructed pocket wetlands at least three days prior to planting, because a dry wetland is easier to plant than a wet one.

Filter Bags may be used to filter water pumped from disturbed areas prior to discharging into any surrounding resource areas. They may also be used to filter water pumped from the sediment storage areas of sediment basins.

Filter bags shall be installed according to the detail shown on the Site Plans.

Filter bags shall be made from non-woven geotextile material sewn with high-strength, double stitched "J" type seams. They shall be capable of trapping particles larger than 150 microns.

Filter bags shall be replaced when they become $\frac{1}{2}$ full. Spare bags shall be kept available for replacement of those that have failed or are filled.

Bags shall be located in well-vegetated (grassy) area, and discharge onto stable, erosion resistant areas. Where this is not possible, a geotextile flow path shall be provided. Bags shall not be placed on slopes greater than 5%.

The pump discharge hose shall be inserted into the bags in the manner specified by the manufacturer and securely clamped.

The pumping rate shall be no greater than 750 gpm or ¹/₂ the maximum specified manufacturer, whichever is less. Pump intake hoses should be floating and screened.

Filter bags shall be inspected daily. If any problem is detected, pumping shall cease immediately and not resume until the problem is corrected.

Long Term Inspection and Maintenance

During the phased construction, the stormwater management system shall be maintained on a routine basis not less than once per month. Upon acceptance of the roadways recommended maintenance performed by the Town of Wilmington as recommended below. Refer to the Grading & Drainage Plans, for drainage structure locations. Inspection and maintenance shall be performed as follows:

- 1. <u>Street Sweeping</u> Completed every spring after last snowfall. Removed sediment will be disposed off site by a qualified waste disposal contractor in accordance with state and federal regulations.
- 3. <u>Particle Separators</u> See attached maintenance procedures for Hydroworks proprietary particle separators. All sediments removed must be disposed of in accordance with all applicable local and state regulations.
- 3. <u>Snow Removal and Storage</u>: During the winter months, snow shall be plowed from the roadway and not stored or piled in or near the stormwater basins.
- 4. <u>Bioretention Areas</u> Inspect the biortention areas, and repair any eroded areas and remove trash on a monthly basis year round. Prune and remove any dead vegetation each spring and fall. Replace any dead vegetation and mulch the area each spring. If the soil media fails and infiltration no longer occurs, the entire media and all vegetation must be replaced in either late spring or early summer with similar plantings. Soil media and plants must be in accordance with Massachusetts DEP Stormwater Handbook guidelines.
- 5. <u>Constructed Stormwater Wetlands</u>- In the first three years after construction, inspect the wetlands twice a year during both the growing and non-growing seasons. During these inspections, record and map the following information:
 - The types and distribution of the dominant wetland plants
 - The presence and distribution of planted wetland species
 - The presence and distribution of invasive wetland species (must be removed)
 - Indications that other species are replacing the planted wetland species
 - Percentage of standing water that is unvegetated (excluding the deep water cells)
 - The maximum elevation and the vegetative condition in this zone
 - Stability of the original depth zones and the micro-topographic features

- Accumulation of sediment in the forebay and micropool; and survival rate of plants (cells with dead plants must be replanted)

6. <u>Sediment Forebay</u>- Sediment forebays are to be cleaned at least once per year.

Stormwater System Inspection Report

General Information				
Location: Port Place, Newburyport MA				
Date of Inspection	Start/End Time			
Inspector's Name(s)				
Inspector's Title(s)				
Inspector's Contact Information				
Purpose of Inspection				
Weather In	formation			
Has it rained since the last inspection? □Yes □No				
Weather at time of this inspection?				

Site-Specific Stormwater Devices

	Description	Installed and Operating Properly?	Corrective Action Needed	Date for Corrective Action/Responsible Person
1		□Yes □No		
2		□Yes □No		
3		□Yes □No		
4		□Yes □No		
5		□Yes □No		
6		□Yes □No		
7		□Yes □No		
8		□Yes □No		
9		□Yes □No		

	Description	Installed and Operating Properly?	Corrective Action Needed	Date for Corrective Action/Responsible Person
10		□Yes □No		
11		□Yes □No		
12		□Yes □No		
13		□Yes □No		
14		□Yes □No		
15		□Yes □No		

	Description		Corrective Action	Date for Corrective Action/Responsible Person
1	Are all slopes properly stabilized?	□Yes □No		
2	Are natural resource areas (e.g., streams, wetlands, etc.) being subjected to erosion?	□Yes □No		
3	Are discharge points free of sediment deposits?	□Yes □No		

Certification Statement:

"I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations."

Print name: _____

Signature: _____

Date:



Hydroworks[®] Hydroguard

Operations & Maintenance Manual

Version 1.5

Introduction

The Hydroguard is a state of the art hydrodynamic separator. Hydrodynamic separators remove solids, debris and lighter than water (oil, trash, floating debris) pollutants from stormwater. Hydrodynamic separators and other water quality measures are mandated by regulatory agencies (Town/City, State, Federal Government) to protect storm water quality from pollution generated by urban development (traffic, people) as part of new development permitting requirements.

As storm water treatment structures fill up with pollutants they become less and less effective in removing new pollution. Therefore it is important that storm water treatment structures be maintained on a regular basis to ensure that they are operating at optimum performance. The Hydroguard is no different in this regard and this manual has been assembled to provide the owner/operator with the necessary information to inspect and coordinate maintenance of their Hydroguard.

Hydroworks[®] HG Operation

The Hydroworks HG separator is unique since it treats both high and low flows in one device, but maintains separate flow paths for low and high flows. Accordingly, high flows do not scour out the fines that are settled in the low flow path since they are treated in a separate area of the device as shown in Figure 1.

The HG separator consists of three chambers:

- 1. an inner chamber that treats low or normal flows
- 2. a middle chamber that treats high flows
- 3. an outlet chamber where water is discharged to the downstream storm system

Under normal or low flows, water enters the middle chamber and is conveyed into the inner chamber by momentum. Since the inner chamber is offset to one side of the structure the water strikes the wall of the inner chamber at a tangent creating a vortex within the inner chamber. The vortex motion forces solids and floatables to the middle of the inner chamber. The water spirals down the inner chamber to the outlet of the inner chamber which is located below the inlet of the inner chamber and adjacent to the wall of the structure but above the floor of the structure. Floatables are trapped since the outlet of the inner chamber is submerged. The design maximizes the retention of settled solids since solids are forced to the center of the inner chamber by the vortex motion of water while the outlet of the inner chamber draws water from the wall of the inner chamber.

The water leaving the inner chamber continues into the middle chamber, again at a tangent to the wall of the structure. The water is then conveyed through an outlet baffle wall (high and low baffle). This enhances the collection of any floatables or solids not removed by the inner chamber. Water flowing through the baffles then enters the outlet chamber and is discharged into the downstream storm drain.

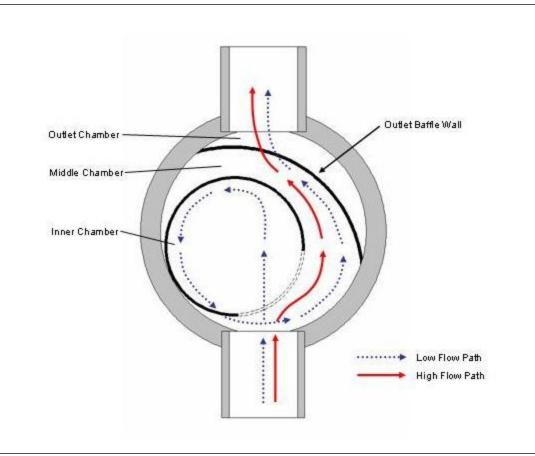


Figure 1. Hydroworks HG Operation – Plan View

During high flows, the flow rate entering the inner chamber is restricted by the size of the inlet opening to the inner chamber. This restriction of flow rate into the inner chamber prevents scour and re-suspension of solids from the inner chamber during periods of high flow. This is important since fines, which are typically considered highly polluted, are conveyed during low/normal flows.

The excess flow is conveyed directly into the middle chamber where it receives treatment for floatables and solids via the baffle system. This treatment of the higher flow rates is important since trash and heavier solids are typically conveyed during periods of higher flow rates. The Hydroworks HG separator is revolutionary since it incorporates low and high flow treatment in one device while maintaining separate low and high flow paths to prevent the scour and re-suspension of fines.

Figure 2 is a profile view of the HG separator showing the flow patterns for low and high flows.

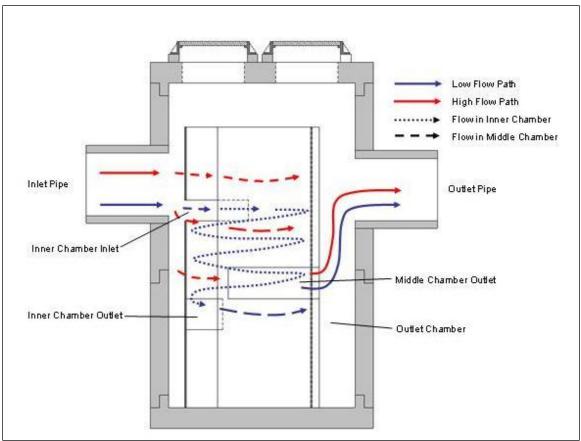
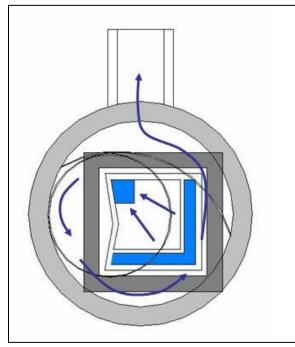


Figure 2. Hydroworks HG Operation – Profile View

The HG 4i is an inlet version of the HG 4 separator. There is a catch-basin grate on top of the HG 4i. Water flows directly into the inner chamber of the HG 4i through the catch-basin grate on top of the structure. The grate is oversized to allow maintenance of the entire structure. A funnel that sits underneath the grate on the top cap of the concrete itself directs the water into the inner chamber during normal flows and the middle chamber during high flows. Figures 3 and 4 show the flow paths for the HG 4i separator.

The inlet funnel is sloped towards the corner inlet and hence the wall of the inner chamber. Water moves in a circular direction in the inner chamber since water enters tangentially along the wall of the inner chamber due to the sloping funnel.

Water continues moving in a circular motion (vortex) through the rest of the structure (through the middle chamber and baffle wall) until it is discharged from the separator.



During periods of peak flow the water will back up from the corner inlet and overflow into two side overflow troughs which discharge directly into the middle chamber. These overflow troughs are covered from the surface such that water cannot directly fall through them (i.e. water must back up to enter the overflow troughs).

Accordingly this funnel provides the same separate flow paths for low and high flow as the other Hydroguard separators.

The whole funnel is removed for inspection and cleaning providing.

Figure 3. Hydroworks HG 4i Normal Flow Path

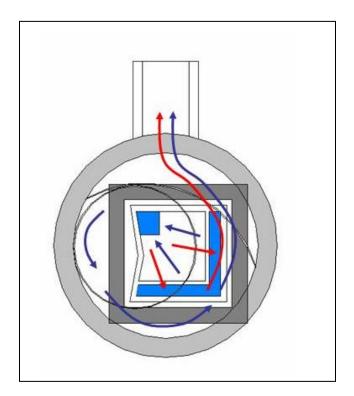


Figure 4. Hydroworks HG 4i Peak Flow Path

Inspection

Procedure

Although all parts of the Hydroguard should be inspected, inspection and maintenance should focus on the inner and middle chambers since this is where the pollutants (floatable and sinking) will accumulate.

Floatables

A visual inspection can be conducted for floatables by removing the covers and looking down into the separator. Multiple covers are provided on Hydroworks HG units to access all areas of the separator (The HG 4 may have a single larger 32" (800mm) cover due to the lack of space for multiple 24" (600mm) covers). Separators with an inlet grate (HG4i or custom separator) will have a plastic funnel located under the grate or on the top cap of the concrete that must be removed through the frame prior to inspection or maintenance. If you are missing a funnel please contact Hydroworks at the numbers provided at the end of this document.

TSS/Sediment

Inspection for TSS build-up can be conducted using a Sludge Judge®, Core Pro®, AccuSludge® or equivalent sampling device that allows the measurement of the depth of TSS/sediment in the unit. These devices typically have a ball valve at the bottom of the tube that allows water and TSS to flow into the tube when lowering the tube into the unit. Once the unit touches the bottom of the device, it is quickly pulled upward such that the water and TSS in the tube forces the ball valve closed allowing the user to see a full core of water/TSS in the unit. The unit should be inspected for TSS through each of the access covers. Several readings (2 or 3) should be made at each access cover to ensure that an accurate TSS depth measurement is recorded.

Frequency

Construction Period

The HG separator should be inspected every two weeks and after every large storm (over 0.5" (12.5 mm) of rain) during the construction period.

Post-Construction Period

The Hydroworks HG separator should be inspected once per year for normal stabilized sites (grassed or paved areas). If the unit is subject to oil spills or runoff from unstabilized (storage piles, exposed soils) areas the HG separator should be inspected more frequently (4 times per year). The initial annual inspection will indicate the required future frequency of maintenance if the unit was maintained after the construction period.

Reporting

Reports should be prepared as part of each inspection and include the following information:

- 1. Date of inspection
- 2. GPS coordinates of Hydroworks unit
- 3. Time since last rainfall
- 4. Date of last inspection
- 5. Installation deficiencies (missing parts, incorrect installation of parts)
- 6. Structural deficiencies (concrete cracks, broken parts)
- 7. Operational deficiencies (leaks, blockages)
- 8. Presence of oil sheen or depth of oil layer
- 9. Estimate of depth/volume of floatables (trash, leaves) captured
- 10. Sediment depth measured
- 11. Recommendations for any repairs and/or maintenance for the unit
- 12. Estimation of time before maintenance is required if not required at time of inspection

A sample inspection checklist is provided at the end of this manual.

Maintenance

Procedure

The Hydroworks HG unit is typically maintained using a vacuum truck. There are numerous companies that can maintain the HG separator. Maintenance with a vacuum truck involves removing all of the water and sediment together. The water is then separated from the sediment on the truck or at the disposal facility.

In instances where a vacuum truck is not available other maintenance methods (i.e. clamshell bucket) can be used, but they will be less effective. If a clamshell bucket is used the water must be decanted prior to cleaning since the sediment is under water and typically fine in nature. Disposal of the water will depend on local requirements. Disposal options for the decanted water may include:

- 1. Discharge into a nearby sanitary sewer manhole
- 2. Discharge into a nearby LID practice (grassed swale, bioretention)
- 3. Discharge through a filter bag into a downstream storm drain connection

The local municipality should be consulted for the allowable disposal options for both water and sediments prior to any maintenance operation. Once the water is decanted the sediment can be removed with the clamshell bucket.

Disposal of the contents of the separator depend on local requirements. Maintenance of a Hydroworks HG unit will typically take 1 to 2 hours based on a vacuum truck and longer for other cleaning methods (i.e. clamshell bucket).

Frequency

Construction Period

A HG separator can fill with construction sediment quickly during the construction period. The Hydroguard must be maintained during the construction period when the depth of TSS/sediment reaches 30" (750 mm). It must also be maintained during the construction period if there is an appreciable depth of oil in the unit (more than a sheen) or if floatables other than oil cover over 50% of the open water surface on the inlet side of the outlet baffle wall.

The HG separator should be maintained at the end of the construction period, prior to operation for the post-construction period.

Post-Construction Period

The Hydroguard was independently tested by Alden Research Laboratory in 2008. A HG6 was tested for scour with initial sediment loads of 4.6 ft³ and 9.3 ft³. The results from these tests were almost identical. Therefore, the 9.3 ft³ sediment load was used as 50% of the maximum sediment depth for maintenance in the calculation of the maintenance interval for the HG6 separator based on the NJDEP maintenance equation.

Maintenance Interval (months) = 3.565 x (Sediment Storage) / (MTFR x TSS Removal)

Maintenance Interval (HG6) = 3.565 x 9.3 / (1.81x 0.60) = 30 months

All values (flow, sediment storage) can be scaled by the surface area making the sediment depths and maintenance intervals equal for all separators.

The separator was loaded with the sediment in the inner chamber and middle chamber with the majority of sediment (80%) located in the inner chamber. The inner chamber for area represents approximately 44% of the separator surface area. The inner chamber is 4 ft (1200 mm) in diameter in the HG6. Therefore the 50% sediment depth for the HG6 in the inner chamber would be:

9.3 $ft^3 \ge 0.80 / (3.14 \ge 4 ft^2) \ge 12 in/ft = 7.1 inches (175 mm)$

Accordingly the 100% sediment volume would represent 14.2" (350 mm) of sediment depth in the inner chamber.

The HG separator must be maintained if there is an appreciable depth of oil in the unit (more than a sheen) or if floatables other than oil cover over 50% of the open water surface on the inlet side of the outlet baffle wall. It should also be maintained once the accumulated TSS/sediment depths are greater than 14" (350 mm) in the inner chamber. For typical stabilized post-construction sites (parking lots, streets) it is anticipated that maintenance will be required annually or once every two years. More frequent or less frequent maintenance will be required depending on individual site conditions (traffic use, stabilization, storage piles, etc.). The long term maintenance frequency can be established based on the maintenance requirements during the first several years of operation if site conditions do not change.



HYDROGUARD INSPECTION SHEET

Date Date of Last Inspection			
Site City State Owner			
GPS Coordinates			
Date of last rainfall			
Site Characteristics Soil erosion evident Exposed material storage on Large exposure to leaf litter (High traffic (vehicle) area		Yes	No
Hydroguard Incorrect access orientation Obstructions in the inlet or or Missing internal components Improperly installed internal of Improperly installed inlet or of Internal component damage Floating debris in the separa Large debris visible in the se Concrete cracks/deficiencies Exposed rebar Water seepage (water level no Water level depth below	components outlet pipes (cracked, broken, loose pieces) tor (oil, leaves, trash) parator ot at outlet pipe invert)	Yes	
Floating debris coverage <	0.5" (13mm)	>0.5" 13mm) > 25% surface area > 14" (350mm)	□* □* □*

- * Maintenance required
- ** Repairs required
- *** Further investigation is required

Please call Hydroworks at 888-290-7900 or email us at support@hydroworks.com if you have any questions regarding the Inspection Checklist. Please fax a copy of the completed checklist to Hydroworks at 888-783-7271 for our records.

Other Comments:		



Hydroworks[®] Hydroguard

One Year Limited Warranty

Hydroworks, LLC warrants, to the purchaser and subsequent owner(s) during the warranty period subject to the terms and conditions hereof, the Hydroworks Hydroguard to be free from defects in material and workmanship under normal use and service, when properly installed, used, inspected and maintained in accordance with Hydroworks written instructions, for the period of the warranty. The standard warranty period is 1 year.

The warranty period begins once the separator has been manufactured and is available for delivery. Any components determined to be defective, either by failure or by inspection, in material and workmanship will be repaired, replaced or remanufactured at Hydroworks' option provided, however, that by doing so Hydroworks, LLC will not be obligated to replace an entire insert or concrete section, or the complete unit. This warranty does not cover shipping charges, damages, labor, any costs incurred to obtain access to the unit, any costs to repair/replace any surface treatment/cover after repair/replacement, or other charges that may occur due to product failure, repair or replacement.

This warranty does not apply to any material that has been disassembled or modified without prior approval of Hydroworks, LLC, that has been subjected to misuse, misapplication, neglect, alteration, accident or act of God, or that has not been installed, inspected, operated or maintained in accordance with Hydroworks, LLC instructions and is in lieu of all other warranties expressed or implied. Hydroworks, LLC does not authorize any representative or other person to expand or otherwise modify this limited warranty.

The owner shall provide Hydroworks, LLC with written notice of any alleged defect in material or workmanship including a detailed description of the alleged defect upon discovery of the defect. Hydroworks, LLC should be contacted at 136 Central Ave., Clark, NJ 07066 or any other address as supplied by Hydroworks, LLC. (888-290-7900).

This limited warranty is exclusive. There are no other warranties, express or implied, or merchantability or fitness for a particular purpose and none shall be created whether under the uniform commercial code, custom or usage in the industry or the course of dealings between the parties. Hydroworks, LLC will replace any goods that are defective under this warranty as the sole and exclusive remedy for breach of this warranty.

Subject to the foregoing, all conditions, warranties, terms, undertakings or liabilities (including liability as to negligence), expressed or implied, and howsoever arising, as to the condition, suitability, fitness, safety, or title to the Hydroworks Hydroguard are hereby negated and excluded and Hydroworks, LLC gives and makes no such representation, warranty or undertaking except as expressly set forth herein. Under no circumstances shall Hydroworks, LLC be liable to the Purchaser or to any third party for product liability claims; claims arising from the design, shipment, or installation of the Hydroguard, or the cost of other goods or services related to the purchase and installation of the Hydroguard. For this Limited Warranty to apply, the Hydroguard must be installed in accordance with all site conditions required by state and local codes; all other applicable laws; and Hydroworks' written installation instructions.

Hydroworks, LLC expressly disclaims liability for special, consequential or incidental damages (even if it has been advised of the possibility of the same) or breach of expressed or implied warranty. Hydroworks, LLC shall not be liable for penalties or liquidated damages, including loss of production and profits; labor and materials; overhead costs; or other loss or expense incurred by the purchaser or any third party. Specifically excluded from limited warranty coverage are damages to the Hydroguard arising from ordinary wear and tear; alteration, accident, misuse, abuse or neglect; improper maintenance, failure of the product due to improper installation of the concrete sections or improper sizing; or any other event not caused by Hydroworks, LLC. This limited warranty represents Hydroworks' sole liability to the purchaser for claims related to the Hydroguard, whether the claim is based upon contract, tort, or other legal basis.

Appendix D

Figure 1,2 & 3 – ILSF, Pre & Post Development Drainage Areas



S LLC	Ś	5,936	354,249 SF				
COMMONS, LLC 1 OF	PLAN OF LAND 18 BOYD DRIVE NEWBURYPORT, MASSACHUSETTS PREPARED FOR PREPARED FOR PREPARED FOR		Well No. Ground Elev GW Elev on 5/08/17 GW Elev on 5/19/17 GW Elev on 6/23/17 GW Elev on 7/07/17 3 55.10 49.10 49.80 50.60 50.60 50.60 6 56.80 49.60 50.10 50.90 50.80 50.80	TEST PIT ESHGW DATA TP-5 48.5 TP-6 51.8 TP-9 54.7 TP-11 51.8 TP-13 52.0 AVG. 51.9	* AVERAGE ESHGW BASED UPON TEST PITS IN AND ADJACENT TO THE ILSF AREA (TP'S 5,6,7,8,9,10.11.13) AVERAGE ESHGW ELEVATION = 51.92 USE ELEVATION 52 FOR BOTTOM OF ILSF CALCULATION.	ILSF VOLUME REPORT - 7" RAINFALL Volume Report Comparing Gridi: E:/evergreen/ILSF 8-4.grd Reference elevation: 54.70 Average FILL Depth: 1.84 FIL Depth: 2.70 FIL volume: 451,271.8 C.F., 16,713.77 C.Y. ILSF VOLUME REPORT - 8.3" RAINFALL Volume Report Comparing Gridi: E:/evergreen/ILSF 8-4.grd Reference elevation: 55.20 Area in FILL 289,569.5 S.F., 6.66 Acres Average FIL Depth: 2.02 FIL Depth: 3.20 FIL volume: 584,792.6 C.F., 21,658.98 C.Y.	And State Plane



IS LLC				
	NEWBURYPORT, MASSACHUSETTS	DRAIN AREA 1 (ILSF)= 1,523,843 SF IMPERV. (ROOF/PAVEMENTS)= 40,723 SF WOODS = 137,550 SF LAWN = 1,123,138 SF ILSF AREA= 222,432 SF	DRAIN AREA 3 (BOYD DR)= 38,572 SF IMPERV. (ROOF/PAVEMENTS)= 29,987 SF LAWN = 8,585	MAS STE PLAN
SHEET NO. 1 OF 1	PROJECT NO. 2015–063 DATE: <u>MAY 22, 2017</u>			



	NEWBURYPORT, MASSACHUSETTS		IMPERV. (PAVEMENTS)= 13,972 SF LAWN = 3, IMPERV. (BLDGS.) =5,630 SF DRAIN ARE/ LAWN = 20,432 SF IMPERV. (P/	DRAIN AREA 1D-3 61,661= SF IMPERV. (BIDGS.) = 0,892 SF IMPERV. (BLDGS.) = 0 SF LAWN = 9 IMPERV. (BLDGS.) = 0 SF LAWN = 54,769 SF DRAIN AREA 1D-4 40,034= SF IMPERV. (P/ DRAIN AREA 1D-4 40,034= SF IMPERV. (BIDFRV. (BIDFRV. (B/ IMPERV. (B/ IMPERV. (B/	DRAIN AREA 1D-2 14,630= SF IMPERV. (BLOGS.) = 4,844 SF IMPERV. (BLDGS.) = 0 SF LAWN = 0 SF IMPERV. (BLDGS.) = 0 SF DRAIN AREA DRAIN AREA LAWN = 9,786 SF IMPERV. (PAVERAL) IMPERV. (PAVERAL)	110 SF D-1 26,985= SF D-1 26,985= SF EMENTS)= 9,083 SF SS.) =5,664 SF 38 SF	DRAIN AREA 1D (ILSF) 162,115= SF IMPERV. (P 8= SF IMPERV. (PAVEMENTS)= 20,099 SF IMPERV. (B 099 SF IMPERV. (BLDGS.) =8,489SF DRAIN ARE.	REA 1B-5 40,419= SF IMPERV. (P. (PAVEMENTS)= 0 SF IMPERV. (B. (BLDGS.) = 5,003 SF LAWN = 4 35,416 SF DRAIN ARE.	REA 1B-3 25,005= SF DRAIN AREA 1E-3 (PAVEMENTS)= 9,392 SF IMPERV. (PAVEME (BLDGS.) =4,208 SF IMPERV. (PAVEME 11,405 SF IMPERV. (BLDGS.) 11,405 SF IMPERV. (BLDGS.) REA 1B-4 32,646= SF IMPERV. (BLDGS.) (PAVEMENTS)= 5,484SF IMPERV. (BLDGS.) (BLDGS.) =0 SF DRAIN ARE 27,162 SF DRAIN ARE	BLDGS.) =10,696 SF IMPERV. (BLDGS. 38,501 SF LAWN = 9,583 (EV) REA 1B-1 8,603= SF DRAIN AREA 1E-1 (PAVEMENTS)= 3,006 SF IMPERV. (PAVEME (BLDGS.) =1,096 SF IMPERV. (PAVEME (BLDGS.) =1,096 SF IMPERV. (BLDGS.) 4,501 SF IMPERV. (BLDGS.) 4,501 SF IMPERV. (BLDGS.) (BLDGS.) =1,096 SF IMPERV. (BLDGS.) (BLDGS.) =1,096 SF IMPERV. (BLDGS.) (BLDGS.) =0 SF IMPERV. (BLDGS.) (BLDGS.) =0 SF IMPERV. (BLDGS.) (SF IMPERV. (BLDGS.)
MENT,	VE PROJEC 2015- ACHUSETTS DATE: MAY 2	IMPERV. (BLDGS.) =0 SF			$\epsilon \sim \epsilon$	IMPERV. (PAVEME IMPERV. (BLDGS.) LAWN = 8,820 SI DRAIN AREA 1F-3 IMPERV. (PAVEME	IMPERV. (PAVEMENTS)= 9,051 SF IMPERV. (BLDGS.) =6,129 SF LAWN = 24,232 SF DRAIN AREA 1F-2 20.326= SF	トてて	DRAIN AREA 1E-3 18,805= SF IMPERV. (PAVEMENTS)= 0 SF IMPERV. (BLDGS.) =1,675 SF LAWN = 17,130 SF DRAIN AREA 1F (ILSF) 87,275= SF	トート